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<p>Interest has arisen in the last few years to develop analytical models of the undersea acoustic environment which are suitable for use on digital computers. To realistically represent the sound-field structure which exists in the ocean, one must consider the variation of sound speed in two dimensions: depth and range. A computer program, TRIMAIN, was written in Fortran IV in which the sound-speed field for a given region is divided into triangular segments of the range-and-depth plane. In each segment the sound-speed field, in terms of <math>(1/c)^2</math>, is defined by a linear function of range and depth. The ray paths for this field become parabolic</p>			

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19. (Cont'd)

Caustics  
Spreading loss  
Inhomogeneous media  
Multiple profiles  
Linear segmented bottom  
Calcomp plotting  
Computer applications

20. (Cont'd)

trajectories in each triangular segment. All the rays are advanced to a given range at one time, and an interpolation in depth is performed to arrive at the intensity values. Four types of intensity calculations are available: a completely random phase summation, a completely coherent phase summation, a statistical influence over depth, and an average over a convergence zone. Additional output options are ray depth distributions, ray printplots, and Calcomp ray plots, including plots of input sound speeds and of bathymetric profiles.

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## HORIZONTAL-GRADIENT ACOUSTICAL RAY-TRACE PROGRAM TRIMAIN

### INTRODUCTION

The growth in computer capability over the last 15 years coupled with interest in underwater acoustics has prompted the creation of several computer programs for acoustical ray tracing. For short-range calculation, for which the sound-speed profile can be considered to be the same throughout the given domain and the bottom topography can be considered flat, computation time is conserved by using a single profile program which takes advantage of the periodic form of the ray trajectories, such as the program RTRACE [1]. For long-range acoustical ray tracing, for which the bottom profile as well as the horizontal velocity structure is quite varied, a more general program [2-4] is required. One example of this is the program TRIMAIN, the principal features of which are as follows:

- Acoustic velocity gradients in the sound speed field are accounted for by reading in sound-speed profiles as a function of range and depth. Sound-speed profiles may be introduced at any point in range, and there is no limit to the number which may be used, although each new profile slows the program. A maximum of 50 input and internally generated points are allowed per profile. The sound-speed profiles are assumed to be piecewise linear functions of depth and range. An excellent source of sound-speed-profile data is the NODC tapes [5].
- A variable bottom may be read in as a piecewise linear function of depth, with a maximum of 250 points as the end points of the linear pieces.
- The range-and-depth plane is divided into triangular regions whose vertexes are all initially at ranges equal to the ranges of the endpoints of the linear bottom segments.
- The rays are assumed to be parabolic in each triangle, and it is their intersections with the triangle boundaries that are calculated.
- All the rays are advanced at one time to a given range, rather than tracing one ray at a time all the way to the end of the track.
- Four types of intensity calculation are available: type I random phase summation, type I coherent phase summation, type II (average over depth), and type III (average over convergence zone). Unmodified ray theory is used throughout. (Caustics will be discussed later.)
- The volume attenuation in the medium is assumed to follow a modified Marsh-Schulkin formula.
- Bottom-loss values (in dB), may be entered as a function of grazing angle, one value per degree, or the Marine Geophysical Survey (MGS) bottom-loss values may be used by specifying the class and the range to which that value is to be used.
- A bottom-phase-shift table may be entered for coherent phase calculation if known; it is read in as a value in radians, one value per degree.

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- The sea surface is represented as a flat, specularly reflecting boundary with a constant user-specified reflection coefficient and a constant phase shift of  $180^\circ$ .
- A source beam pattern may be read in at 1-degree intervals.

Several output options are available:

- A printplot of intensity vs range,
- A printout of intensity vs range values,
- A printplot of the ray trajectories vs range,
- A Calcomp plot of ray trajectories vs range,
- Ray depth distribution at specified ranges,
- A Calcomp plot of the input sound-speed profiles,
- A printplot of the input, or of the input and interpolated, sound-speed profiles,
- An eigenray printout if intensity calculations are performed,
- Punched cards for intensity values or eigenrays.

Up to ten output control cards may be specified.

The calculated results from TRIMAIN have been compared with experimental results, (Appendix B), and good agreement exists between the two.

The time required to run the program depends on a number of factors, such as the number of rays, the number of range increments, and the output requested. A sample case using 81 rays, 200 range increments, one receiver, and two profiles took 7 minutes and 48 seconds.

The core requirement for the program and system routines is 43,503 decimal locations. Also, some sort of deferred printout equipment is required, such as a drum, or the data may be written on tapes and the tapes printed.

The original development [6] of this computer code was due to Mr. Edward L. Wright, who is now at Harvard Observatory, Cambridge, Massachusetts. The author has added a number of features which were not in the original program and has revised certain sections. The function of each subroutine will be outlined in this report for the convenience of those individuals who might be interested in modifying the program.

## BASIC EQUATIONS

The basic differential equations which are solved in TRIMAIN for ray position and time are:

$$n(\vec{r}) = \frac{1}{c(\vec{r})}, \quad (1)$$

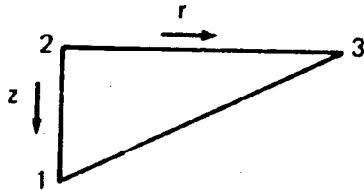
$$(d/ds)T = n(\vec{r}), \quad (2)$$

$$(d/ds)[n(\vec{r})(d/ds)\vec{r}] = \vec{\nabla}n(\vec{r}). \quad (3)$$

Eq. (1) states that the index of refraction as a function of range is equal to the reciprocal of the sound speed as a function of range. Eq. (2) is the equation for the ray time, where  $T$  is time and  $ds$  is arc length. Eq. (3) is the Lagrangian equation, where  $\vec{\nabla}$  is the Lagrangian; it gives the ray path and accounts for the refraction.

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We will now develop an equation for velocity fit. If we have the triangle



where depth is in the  $2 \rightarrow 1$  or  $z$  direction and range is in the  $2 \rightarrow 3$  or  $r$  direction, then the following equations hold:

$$\frac{1}{c_2^2} - \frac{1}{c_1^2} = G_r(r_3 - r_1) + G_z(z_3 - z_1), \quad (4)$$

$$\frac{1}{c_2^2} - \frac{1}{c_1^2} = G_r(r_2 - r_1) + G_z(z_2 - z_1), \quad (5)$$

$$\frac{1}{c^2} = \frac{1}{c_1^2} + G_r(r - r_1) + G_z(z - z_1), \quad (6)$$

where  $G_r$  is the gradient in the  $r$  direction and  $G_z$  is the gradient in the  $z$  direction. Eq. (6) gives the reciprocal of the sound speed squared at a range  $r$  and depth  $z$  in the triangle. We will specialize to the case  $r_2 = r_1$ , because we will always be getting vertical profiles.

## TRIMAIN INPUT

Following will be a list describing the data deck of the program TRIMAIN, and for illustration the sample data deck shown in Fig. 1 will be referred to. The Roman numbers itemizing the list are the card group numbers at the right in Fig. 1.

- I. *Title (columns 1-80).* In the restarting case, the word RESTART is placed in columns 1-7. If a dump is desired if program runs out of time again, DUMP is placed in columns 9-12.
- II. *Source Parameters*

<u>Variable</u>	<u>Columns</u>	<u>Remarks or Meaning</u>
Source depth	1-8	In meters. (In Fig. 1 the source depth is 500 meters.)
Frequency	9-13	In kilohertz (0.05 kHz in Fig. 1)

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THE TITLE FOR THE PROBLEM									
THIS IS CARD GROUP NUMBER									
5.00	0.050	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
15.0	0	7.5	0	1	0	1	0	1	0
15.0	0	15.0	0	2.5	1	0	1	0	0
75.0	0	-15.0	0	1	0	0	1	0	0
457.0	6	0	0	0	0	0	0	0	0
0.0	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	0.10
0.0	0	7	0	8	0	9	0	10	0
4.0	5.0	6.0	7.0	8.0	9.0	10.0	11.0	12.0	13.0
1.00	0	100.0	0	100.0	0	100.0	0	100.0	0
5.0	0	100.0	0	100.0	0	100.0	0	100.0	0
1.0	0	100.0	0	100.0	0	100.0	0	100.0	0
0.0	0	100.0	0	100.0	0	100.0	0	100.0	0
0.0	0	100.0	0	100.0	0	100.0	0	100.0	0
50.0	0	100.0	0	100.0	0	100.0	0	100.0	0
43.0	0	45.0	0	45.7	0	43.0	0	43.0	0
5.1	0	4.2	0	0	4.0	0	3.8	0	3.6
0.0	0	FIRST PROFILE AT RANGE 0.0 KM	0	0	0	0	0	0	0
0.0	0	15.31	0	2.0	0	15.32	0	5.0	0
2.00	0	15.16	0	3.00	0	15.13	0	4.00	0
0.00	0	14.97	0	1.250	0	15.01	0	1.500	0
3.00	0	15.35	0	4.000	0	15.53	0	7.000	0
0.107	6	SECOND PROFILE AT RANGE 1.07 KM	0	0	0	0	0	0	0
0.0	0	1.527	0	2.0	0	1.527	0	5.0	0
2.00	0	1.516	0	3.00	0	1.513	0	4.00	0
1.00	0	1.497	0	1.250	0	1.501	0	1.501	0
3.00	0	1.535	0	4.000	0	1.553	0	7.000	0
0.135	4	THIRD PROFILE AT RANGE 1.354 KM	0	0	0	0	0	0	0
0.0	0	1.485	0	1.20	0	1.484	0	5.0	0
2.00	0	1.487	5	3.0	0	1.490	0	1.500	0
1.00	0	1.501	0	1.250	0	1.505	0	1.505	0
3.00	0	1.536	0	4.000	0	1.554	0	7.000	0
END	OF	FILE	CARD	1	0	1	0	2.000	0
END	OF	FILE	CARD	1	0	1	0	15.19	0

Fig. 1 — Sample data deck of the program TRIMAIN

<u>Variable</u>	<u>Columns</u>	<u>Remarks or Meaning</u>
Attenuation switch	14	0 (as in Fig. 1) means no volume attenuation; nonzero means $\alpha = 0.0003025/f^2 + 44f^2/(4100 + f^2)$ dB/km, where $f$ is the frequency in kilohertz.
Source level	15-19	Level in decibels (0.0 in Fig. 1)
Beam pattern switch (to be referred to later as ITBP)	20	0 (as in Fig. 1) means no beam pattern; nonzero means the beam pattern will be read in later.
Down tilt	21-25	Tilt of the beam-pattern axis in degrees (0.0 in Fig. 1).
Surface loss	26-30	Surface loss in decibels (0.0 in Fig. 1).
Bottom-loss switch	31	1 means an infinite bottom loss, so that no table will be read in; 0 (as in Fig. 1) means a loss table will be read in later.
Bottom-phase switch (ISCP)	32	1 means a bottom-phase-shift table will be read in; 0 (as in Fig. 1) means no table will be read in.
Curved earth (receiver)	33	1 (as in Fig. 1) means a curved earth correction for the receiver; 0 means no curve.
Curved bottom points	34	1 (as in Fig. 1) means a curved earth correction for the bottom; 0 means no curve.
Plot (Calcomp) profiles	35	2 means input and interpolated profiles are plotted; 1 (as in Fig. 1) means only input profiles are plotted; 0 means no plot.
Printplot profiles	36	1 means printplot-input profiles; 0 means no plot; 2 (as in Fig. 1) means printplot-input and interpolated profiles.
Calcomp plot profiles in kilometers or nautical miles	37	1 means plot nm; 0 (as in Fig. 1) means km.
Plot length	38-45	Calcomp plot length in inches (24.0 inches in Fig. 1).

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<u>Variable</u>	<u>Columns</u>	<u>Remarks or Meaning</u>
Bottom-reflection termination (NBRS)	46-50	Maximum number of bottom hits allowed before a ray is terminated; if blank (as in Fig. 1) or 0, 2500 will be used.
Surface-reflection termination (NSRS)	51-55	Maximum number of surface hits allowed before a ray is terminated; if blank (as in Fig. 1) or 0, 2500 will be used.
Loss termination (ALIM)	56-65	Maximum loss allowed before a ray is terminated; the input value is a positive number in dB, such as 200.0; if blank (as in Fig. 1) or 0, a value of 300.0 will be used.
Multiple replacement option IA	66	If IA is blank (as in Fig. 1) or 0 and ITBP = 0, angle cards are read from the card reader; if IA is blank or 0 and ITBP = 1, angle fan cards and beam-pattern cards are read from the card reader. If IA = 1 and ITBP = 0, the last set of fan cards for which multiple replacement option LA (in column 71) is 1 will be used, and if ITBP = 1 a new beam pattern will then be read in. If IA = 2, which requires that ITBP = 1, the old beam pattern will be used and a new set of angles will be read. If IA = 3, the old angle set and beam-pattern set is used.
Multiple replacement option IB	67	If IB is blank or 0, bottom-loss cards are read from the card reader, and if ISCP = 1, phase-shift cards are read. Bottom classes 0 through 5 are assumed to have a zero phase shift, so phase-shift cards are not read for these classes. If IB = 1, the old bottom-loss set is used, and a new bottom-phase-shift set is read in if ISCP = 1. If IB = 2, a new bottom-loss set will be read in, and if ISCP = 1, the old bottom-phase-shift set will be used. If IB = 3 and ISCP = 1, the old bottom-phase-shift and bottom loss will be used.

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<u>Variable</u>	<u>Columns</u>	<u>Remarks or Meaning</u>
Multiple replacement option IP	68	If IP is blank or 0, a new set of output control cards will be read in; if IP = 1, the old set will be used.
Multiple replacement option ID	69	If ID is blank or 0, a new bottom track will be read, if ID = 1, the old bottom track will be used.
Multiple replacement option IS	70	If IS is blank or 0, a new set of sound-speed profiles will be read; if IS = 1, the old set will be read.
Multiple replacement option LA	71	If LA = 1, the current deck will be used later; if LA is blank or 0, no portion of this deck will be used later. Thus in the following pages the discussion of the various input sections are subject to the provisions of this section.
Restart Option	73-76	If restart capability is desired, the word DUMP is placed in columns 73-76.

**III. Ray Initialization Cards****A. Fan Cards**

<u>Variable</u>	<u>Columns</u>	<u>Remarks</u>
Up-angle limit	1-10	In degrees; the sign convention is + for up and - for down. (In Fig. 1 there are three fan cards, each on a separate line; the three up-angle limits are 15° down, 15° up, and 75° up.)
Down-angle limit (DAL)	11-20	DAL = -DAL for input. (In Fig. 1 the three down-angle limits that pair with the up-angle limits are 75° down, 15° down, and 15° up.)
Angular step	21-30	The step input is always positive. (In Fig. 1 the step is 1° from 75° down to 15° down, 1/4° from 15° down to 15° up, and 1° from 15° up to 75° up.)

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<u>Variable</u>	<u>Columns</u>	<u>Remarks</u>
Continuation Switch	31-35	0 means this is the last fan card; 1 means more cards follow.
Source Level	36-40	Decibels added for this fan to the source level in columns 15-19 on card II. This is left blank (as in Fig. 1) if no additional beam pattern on the transmitter is desired.
Phase	41-45	Phase in radians for this fan.

## B. Beam Pattern Cards

If the beam pattern switch on card II (column 20) was nonzero, the beam pattern is read in, 20 values to a card, which is four columns per value, in decibels below the axial value. The first value is on axis, the next 1° off, etc. A blank or zero after the axial value ends the reading; the last nonzero value is extended to all higher angles.

## IV. Bottom-Loss Cards

Cards are read with a variable (referred to as RUNTIL) in columns 1-8 in kilometers (in an F8.4 format) and IClass in columns 9-10 (I2 format). RUNTIL is the last range for IClass. (In the Fig. 1 example 457.0 6 means class 6 until 457 km (assuming another RUNTIL after this which is 0.0). The last RUNTIL must be negative or zero. The associated class will be used for the rest of the run. The possible values for IClass are 0-9:

0	zero bottom loss
1-5	MGS bottom class loss curves
6-9	user supplied tables.

The first time an IClass of 6 (as in Fig. 1), 7, 8, or 9 is read, a bottom-loss table is read, one value per degree, in decibels, 20 per card (in a 20F4.2 format) until a blank appears. (In Fig. 1 the table with an IClass of 6 is

1. 2. 3. 4. 5. 6. 7. 8. 9. 10. blank	
(zero grazing angle)	(9 degrees)

When an IClass of 6, 7, 8, or 9 is read in after the first time, the table does not need to be read in again. In reading in a table the last nonzero value is extended

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to all higher angles. If ISCP  $\neq 0$  on card II, a phase-shift table will be read after each loss table (classes 6-9; classes 0-5 have zero phase shift). The phase-shift table is read in, 20 values per card,  $1^\circ$  per value. The phase shifts are in radians. A zero value terminates read in; the last two nonzero values are used to extrapolate the phase shift to zero. (In Fig. 1 no phase-shift table was read in. The bottom-loss tables in Fig. 1 establish the following:

Grazing Angle (degrees)	Loss Until 457 km (dB)	Loss After 457 km (dB)
0	0	4
1	1	5
2	2	6
3	3	7
4	4	8
5	5	9
6	6	10
7	7	11
8	8	12
9	9	13
10	10	14
11	10	14
12	10	14
↓	↓	↓
90		

## V. Output Control Cards

Output control cards specify the range and depths at which intensities are to be calculated, whether a ray plot or ray tape will be made, whether ray depth distributions will be printed, etc.

Variable	Column	Remarks
R1	1-6	First range in kilometers.
DR	7-12	Range step in kilometers. If DR is negative, the range spacing will be logarithmic, with constant factor $f = 1 + \text{abs}(DR)/R1$ .
R2	13-18	Last range in kilometers. (In Fig. 1 the ranges specified are 100, 200, ..., 1000 kilometers on the first group V card, 5, 10, 15, ..., 1000 kilometers on the second card, 1, 2, ..., 100

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<u>Variable</u>	<u>Columns</u>	<u>Remarks</u>
		kilometers on the third card, and 0, 1, 2, ..., 1000 kilometers on the fourth card.)
IC	19-20	Continuation switch. 0 means this is the last output control card; (as on the last OCC in Fig. 1) otherwise more will be read in.
ISCP	21	Switch for type I coherent phase; 1 means on, and 0 means off.
IT1	22	Switch for type I random phase; 1 means on, and 0 means off. MUST = 1 when ISCP = 1.
IT2	23	Switch for type II; 1 means on, and 0 means off.
IT3	24	Switch for type III; 1 means on, and 0 means off.
IPER	25	Switch for type I eigenrays; 1 means on, and 0 means off.
LLMR	26	1 means Lloyd's mirror effect is included.
JVSR	27	0 means no intensity-vs-range plot for this output control card; 1 means a plot of type I vs range; 2 means a plot of type II vs range; 3 means a plot of type III vs range; 4 means coherent phase vs range. Only one intensity-vs-range plot can be made.
IRD	28	Switch for ray depth distribution (1 means on, as on the first group V card in Fig. 1), and 0 means off.
IRP	29	Switch for ray plot.
IRT	30	Switch for ray tape for Calcomp plot.

If any of the switches in columns 21-25 are on, receiver depths are needed. The first six, in meters, are on the output control card itself, as follows:

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<u>Variable</u>	<u>Columns</u>
RCD(1)	33-40
RCD(2)	41-48
RCD(3)	49-56
RCD(4)	57-64
RCD(5)	65-72
RCD(6)	73-80

If there are more than six, the next ten depths follow the output control card on one card, and then, if needed, the 17th through 26th on another card. Twenty-six is the maximum available. Receiver depths are read until a zero or blank is found. (In Fig. 1 five receiver depths are specified on each of the first three cards: 50, 150, 250, 350, and 450 meters.) If none of the switches 21-25 are on, then no intensities will be calculated, so no receiver depths are necessary. These and some earlier spaces are then used for the ray plot, as follows:

<u>Variable</u>	<u>Columns</u>	<u>Remarks</u>
DR	7-12	Becomes the spacing in kilometers between lines in the ray plot.
R2	13-18	Becomes the end of the ray plot.
RCD(1)	33-40	Becomes the number of rays to be plotted, $1 \leq N \leq 25$ . This must be punched with a decimal point. (On the fourth group V card in Fig. 1, 25 rays are specified to be plotted.)
RCD(2)	41-48	Becomes the maximum depth for the ray plot, in meters.

All these variables will be set to default values if not specified because of intensities. The defaults are: 1 kilometer spacing, 15 rays plotted, and the maximum bottom depth. Even if DR and R2 are set, the defaults for number of rays and (as in Fig. 1) maximum depth may be used if the columns are left blank.

VI. *Bottom Track*

## A. Ranges and Depths

There are 10 values to a card, with range and depths in pairs with respective units in kilometers and meters. The first range must be zero. A later blank or zero or negative value terminates the input. As many

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cards as necessary, up to 50 cards for 250 ranges, will be read. Thus  $R_1$  is in columns 1-8 of card 1,  $D_1$  is in columns 9-16 of card 1,  $R_2$  is in columns 17-24,  $D_2$  is in columns 25-32, etc. The format for range and depth is 10F8.4.

### VII. Sound-Speed Profiles

#### A. Range and Title

On the first card for each velocity profile, 0 is placed in column 1 if the curved-earth correction is desired. The range to the profile in kilometers is in columns 2-8. The title is in columns 9-80.

#### B. Depth and Velocity

There are 10 values per card after the range-and-title card. The first value on the card is the depth in meters for this profile. The second value is the sound speed in meters/second, at the first depth. As many sound speeds as depths are read in. A blank or negative value terminates input. The format for all cards is 10F8.4. (The number of input and internally generated points in a sound-speed profile cannot exceed 50; the number of internally generated points can be reduced by reading in profiles with common depths.)

### VIII. Program Termination

An end-of-file card terminates each data set or case. If multiple cases are desired, the program will go back to the first card, after the end-of-file card. To terminate the run two end-of-file cards should be placed after the last case.

## CONTROL CARDS FOR TRIMAIN

There are several equip cards, which have different functions (Fig. 2). Some of the cards are used for delayed printout, and some are used to punch cards. When using the program, one should change his job card to the form 7<sub>9</sub> JOB (30), charge, ID, time, rather than the usual form 7<sub>9</sub> JOB, charge, ID, time. The change from JOB to JOB (30) allows 30 additional logical units; without this change the program will abort.

If the output is not desired from a certain unit, it may be omitted by using the BY statement. Thus if one wanted to omit the output from logical unit 35, then one should have 7<sub>9</sub> EQUIP, 35=BY, where BY means bypass. The PR designation on an equip card means that unit will be printed. A PU designation means that logical unit will punch cards. The function for each card is as follows:

7<sub>9</sub> DEMAND, 50000B - This card is required for the restart option.

7<sub>9</sub> EQUIP, 3=PL - This card forces plotting of profiles if the program aborts, if the plot is requested.

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SEQUENCE C6660 STARTED PRINTING 06/06/73 AT 132946 ON LP00  
DRUM SCOPES 2,1 COMPUTER ONE, MAX. DEMAND IS 54000R VERSION 006 11/24/72  
SEQUENCE NUMBER 606660 STARTED AT TIME 132726 DATED 06/06/73  
JOB(30),8150162,014RGR,10  
DEMAND,500000  
COMMENT,THIS JCR PRODUCES DELAYED PRINTOUTS  
EQUIP,1=PT,41,\*,\*(TEST CASE,1,1,999),DA  
EQUIP,3=PL  
EQUIP,15=PT,LC,(TEST,1,1,999),DA  
EQUIP,16=PT,LE,\*,DA  
EQUIP,20=PT,HI,PG,(TRIMAIN,01,01,999)  
EQUIP,35=EY  
EQUIP,36=EY  
EQUIP,37=PR  
EQUIP,38=FR  
EQUIP,39=FR  
EQUIP,41=FR  
EQUIP,42=FR  
EQUIP,45=EY  
EQUIP,46=EY  
EQUIP,47=EY  
EQUIP,48=EY  
EQUIP,49=EY  
\*\*\*BINARY DFCK\*\*\*  
BANK,(0), LUMP  
LOAD,20  
RUN,10,10000

Fig. 2 — Example of control cards; this is the front page from the sample run

- 79 EQUIP, 35=BY(PU) - This will punch the bottom track and receiver depths if set equal to PU. Format 10F8.3.
- 79 EQUIP, 36=BY(PU) - This will punch intensity values in 16F5.1 format, for each range point. Each type of intensity will be punched for each receiver.
- 79 EQUIP, 37=PR - This produces a ray depth distribution if requested.
- 79 EQUIP, 38=PR - This produces a printplot of intensity vs range if requested on an output control card.
- 79 EQUIP, 39=PR - This prints the intensity values for the types specified.
- 79 EQUIP, 41=PR - This prints the Type I eigenrays when they are requested.
- 79 EQUIP, 42=PR - This produces the printplot of the ray trajectories when requested.
- 79 EQUIP, 45=BY(PU) - If this is set equal to PU, it will punch type I coherent intensity values for the contouring program. It should be set up for 19 receivers.

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- 79 EQUIP, 46=BY(PU) - If this is set equal to PU, it will punch type I random intensity values for the contouring program. It should be set up for 19 receivers.
- 79 EQUIP, 47=BY(PU) - If this is set equal to PU, it will punch type II intensity values for the contouring program. It should be set up for 19 receivers.
- 79 EQUIP, 48=BY(PU) - If this is set equal to PU, it will punch type III intensity values for the contouring program. It should be set up for 19 receivers.
- 79 EQUIP, 49=BY(PU) - This punches type I eigenrays; it punches everything that is printed in the eigenray printout.

### 79 EQUIP, 1=MT,HI,WQ,\*,DA-OUTPUT TAPE FOR CALCOMP PLOT OF RAY PATHS

The equip cards may be left in the deck if a certain option is not desired; there will be no output from that unit unless a write operation is performed in the program.

### SUBROUTINES

The main, or executive, program TRIMAIN is used chiefly for selecting options and calling the proper subroutine to compute the desired quantities. The subroutines are shown in Fig. 3, and these will be discussed on the succeeding pages. All of the output control cards (group V), title cards (group I), and source depths, frequency, etc. (group II) are read in by the main program. A listing of TRIMAIN and the subroutines is found in Appendix A. A comparison of calculated and experimental values is found in Appendix B.

### Subroutine INITRAYS

The subroutine INITRAYS (whose cards are identified in the right margin in Appendix A by INIT 1, INIT 2, ..., INIT 81) reads in the angle cards and the beam-pattern cards and sets up the initial values of each ray's tangent of the angle, depth, phase, and signal level. (card group numbers will be listed in the section). Information from card group II from the main program is passed in the common block /PATTERN/ (INIT 3, Appendix A), which contains the source depth, beam-pattern switch, degrees of down tilt, and source level (in decibels). INITRAYS then reads in card group III, comprising the fan cards and the beam pattern cards. Rays are started from the lowest angle of each fan to the top. If the low angle of a fan equals the highest angle of the previous fan, a continuous ray group results. Otherwise a buffer ray with zero signal strength separates the fans, and type I intensity calculations will not interpolate over the gap.

### Subroutine BRLTRD

The subroutine BRLTRD reads in the bottom-loss cards (group IV) and sets up the first loss table. On entry, dummy parameter RB is equated to ISCP (card group II), is

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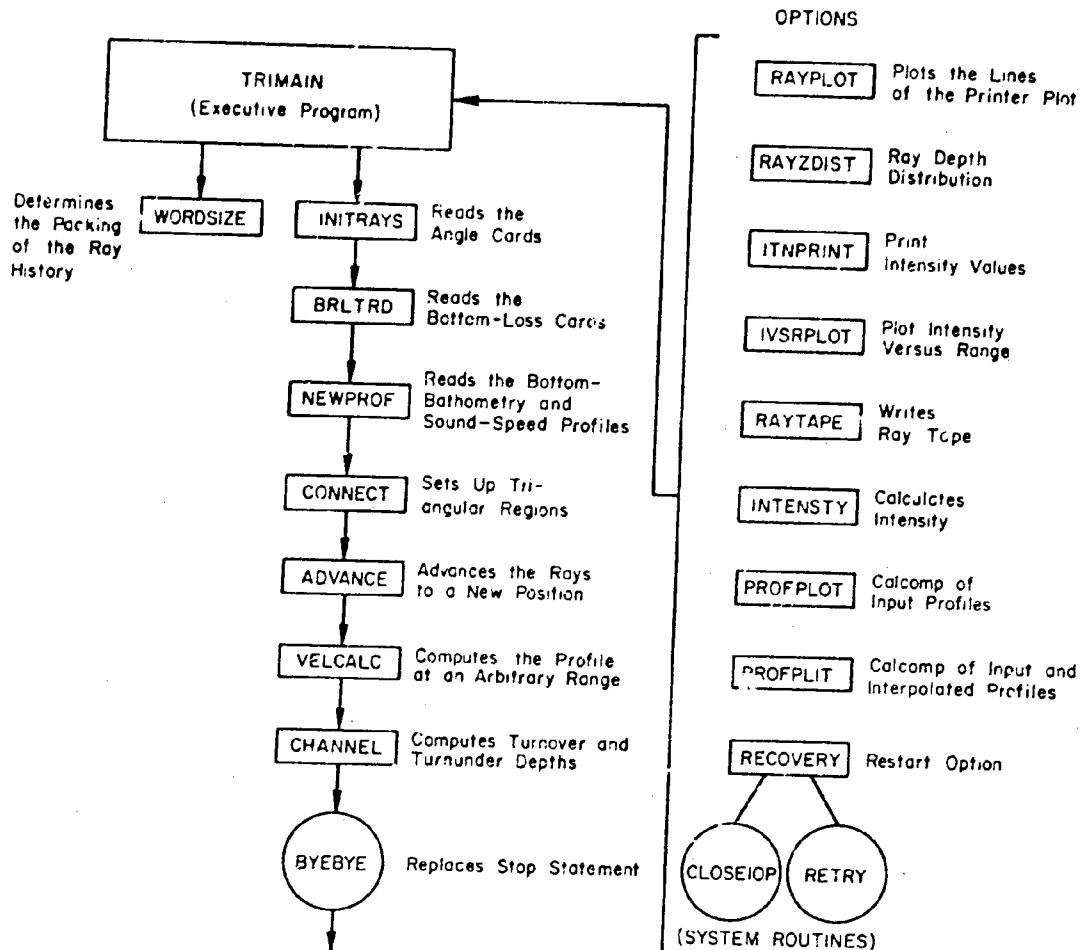


Fig. 3 — Function of each subroutine of the program TRIMAIN

either 1.0 or 0., and determines whether phase-shift tables will be read. On exit, RB is set to the range in kilometers until which the first loss table is to be used. The term ENTRY NWBRLT (as in BLRD 146) resets the loss table and RB. TRIMAIN will call NWBRLT whenever the rays pass RB. For example, if there are two loss tables, one for 0 to 100 km and the second for 100 km to the end of the run, BRLTRD will read in both tables, set BRLT and BPST in the common block /MIRRORS/ (BLRD 3, Appendix A) and set RB to 100. Later a call to NWBRLT sets BRLT and BPST to the second table of values, and RB to 1.E30 (i.e.,  $10^{30}$  km  $\gg$  end of run). Subroutine BRLTRD includes the Marine Geophysical Survey (MGS) classes 0 through 5, plus user classes 6

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through 9 stored in array BR, or user loss and phase classes 6 and 7, stored in arrays BR and BP. If a class 0 through 5 is specified, bottom phase classes do not have to be read in. A maximum of four user classes are available without phase shifts, and two classes are available with phase shifts. If classes 0 through 5 are used, a maximum of 50 cards is allowed.

#### Subroutine NEWPROF

Subroutine NEWPROF reads the bottom ranges, bottom depths (group VI), and the first two sound-speed profiles (group VII) on the first call. It then interpolates a profile for the first bottom point. Succeeding calls generate a new interpolated profile for each bottom point, unless this would pass the last read-in profile. In that case, a bottom point is interpolated to the profile range, and the profile is returned. A new profile is then read in. Thus the basic action of NEWPROF is to move  $R2$  (range to the current profile),  $N2$  (number of points in the current profile),  $Z2$  (depth array), and  $V2$  (sound-speed array) to  $R1$  (range to the previous profile),  $N1$  (number of points in the previous profile),  $Z1$  (depth array for the previous profile), and  $V1$  (sound-speed array for the previous profile) and set new values for  $R2$ ,  $N2$ ,  $Z2$ , and  $V2$ . It returns the maximum bottom depth in  $ZMAX$ . The printed output of NEWPROF is illustrated in Figs. 4a and 4b.

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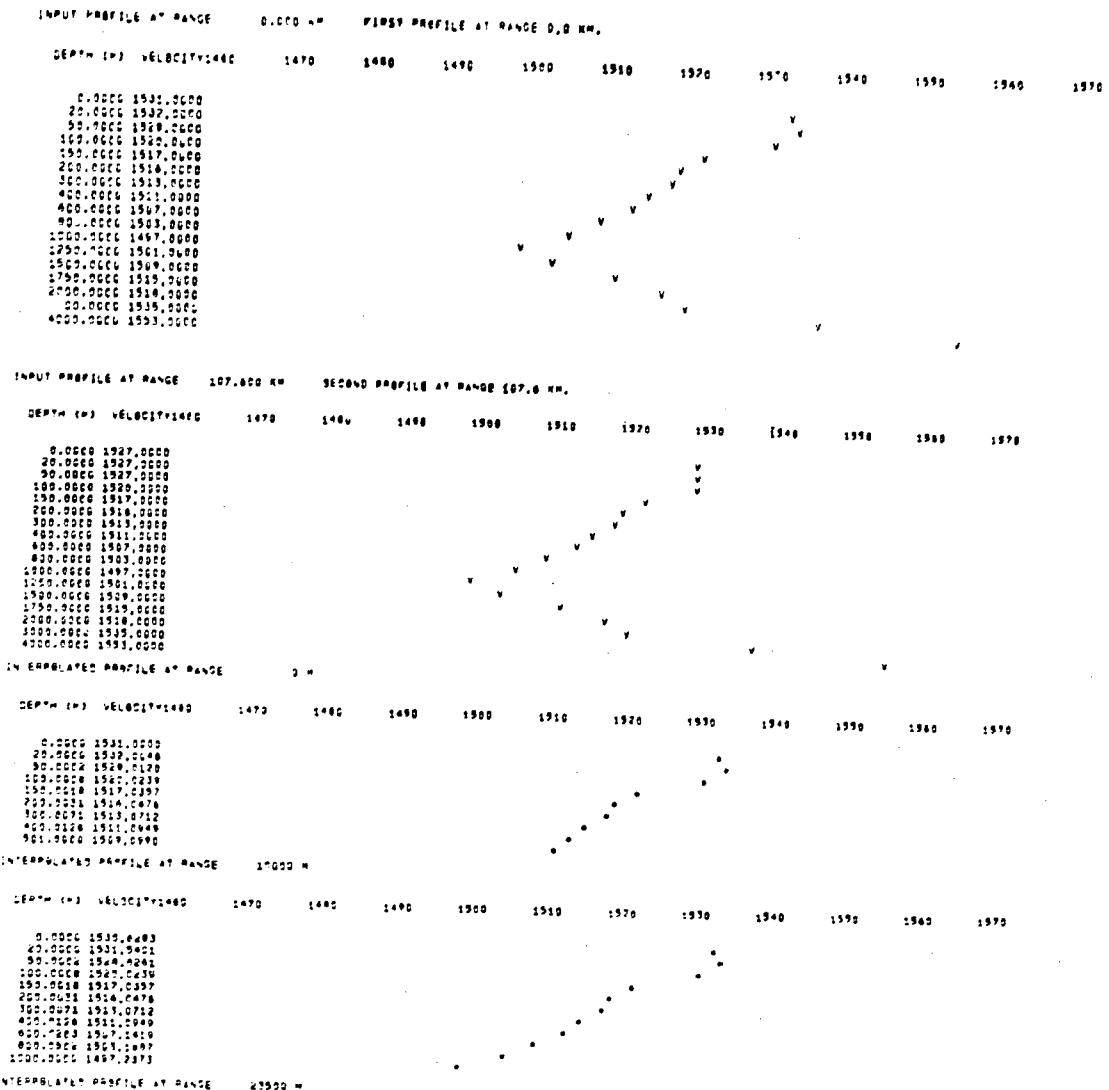


Fig. 4a — Output of NEWPROF. The first two input profiles are those of the sample case given in Fig. 1.

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DEPTH (F)	VELOCITY:1460	1470	1480	1490	1500	1510	1520	1530	1540	1550	1560	1570
0.0000	1570.1200											
20.0000	1530.9370											
50.0000	1520.9730											
100.0000	1520.0130											
150.0000	1520.0397											
200.0000	1510.0200											
300.0000	1500.0700											
400.0000	1500.0100											
600.0000	1500.1410											
800.0000	1500.1887											
1000.0000	1500.2339											
1250.0000	1500.2949											
1500.0000	1500.3393											
1750.0000	1500.4101											
2000.0000	1500.4765											
2500.0000	1500.7220											
3000.0000	1500.4921											
INTERPOLATED PROFILE AT RANGE	570000	*										
DEPTH (F)	VELOCITY:1460	1470	1480	1490	1500	1510	1520	1530	1540	1550	1560	1570
0.0000	1510.8810											
20.0000	1520.1981											
50.0000	1520.0320											
100.0000	1520.0239											
150.0000	1510.0397											
200.0000	1510.0470											
300.0000	1510.0712											
400.0000	1510.0800											
600.0000	1500.1000											
800.0000	1500.1887											
1000.0000	1500.2350											
1250.0000	1500.2949											
1500.0000	1500.3393											
1750.0000	1500.4101											
2000.0000	1500.4765											
2500.0000	1500.7220											
3000.0000	1500.4921											
INTERPOLATED PROFILE AT RANGE	511000	*										
DEPTH (F)	VELOCITY:1460	1470	1480	1490	1500	1510	1520	1530	1540	1550	1560	1570
0.0000	1510.5155											
20.0000	1510.1477											
50.0000	1510.1348											
100.0000	1500.5613											
150.0000	1500.0663											
200.0000	1500.0813											
300.0000	1520.0436											
400.0000	1520.2644											
600.0000	1520.2393											
800.0000	1510.2280											
1000.0000	1500.0785											
1250.0000	1500.0848											
1500.0000	1500.2553											
1750.0000	1510.0439											
2000.0000	1510.0891											
2500.0000	1510.1155											
3000.0000	1520.3677											
4000.0000	1550.9933											
INTERPOLATED PROFILE AT RANGE	1700000	*										
DEPTH (F)	VELOCITY:1460	1470	1480	1490	1500	1510	1520	1530	1540	1550	1560	1570
0.0000	1490.5330											
20.0000	1490.6694											
50.0000	1490.6764											
100.0000	1490.2420											
150.0000	1490.3794											
200.0000	1491.3113											
300.0000	1493.1003											
400.0000	1493.7245											
600.0000	1496.2876											
800.0000	1499.9469											
1000.0000	1500.7086											
1250.0000	1504.7682											
1500.0000	1500.3593											
1750.0000	1514.5476											
2000.0000	1519.3451											
2500.0000	1521.0636											
3000.0000	1521.1609											
INTERPOLATED PROFILE AT RANGE	1100000	*										
DEPTH (F)	VELOCITY:1460	1470	1480	1490	1500	1510	1520	1530	1540	1550	1560	1570
0.0000	1486.4466											
20.0000	1485.4897											
50.0000	1485.4927											
100.0000	1486.0647											
150.0000	1487.3924											
200.0000	1488.5283											
300.0000	1491.4674											
400.0000	1491.7825											
600.0000	1495.0713											
800.0000	1498.3603											
1000.0000	1501.9978											
1250.0000	1505.1575											
1500.0000	1509.3553											
1750.0000	1514.5933											
2000.0000	1519.4474											
2500.0000	1521.1609											

Fig. 4b -- Additional portion of the output of NEWPROF shown in Fig. 4a

### Subroutine CONNECT

Subroutine CONNECT uses  $R1, N1, Z1, V1, R2, N2, Z2$ , and  $V2$  from NEWPROF and connects the points into triangular ( $\Delta$ ) regions. The coefficients of the triangles go into the common block /TRIANG/ (CONN 3, Appendix A). The variables in TRIANG are the following:

AP, BP	coefficients of the $\Delta$ boundary in the prime frame, which is centered at RZERO and ZZERO and rotated by an angle $\theta$ ,
AL, BL	coefficients of the lower $\Delta$ boundary in the ocean frame.
ZZERO, RZERO	ocean frame coordinates of the center of the prime frame.
AA, BB	coefficients of $1/c^2$ in the prime frame, i.e., $1/c^2 = AA + BBz'$ ,
SST, CCT	sin and cos of $\theta$ , the angle between the ocean and the prime frames.

In the listing of the subroutine, the following conditions are true:

$$AL + BL \cdot R = \text{equation for boundary of triangle},$$

$$AA + BZ \cdot Z + BR \cdot R = \frac{1}{c^2}.$$

A typical network of triangular regions is illustrated in Fig. 5.

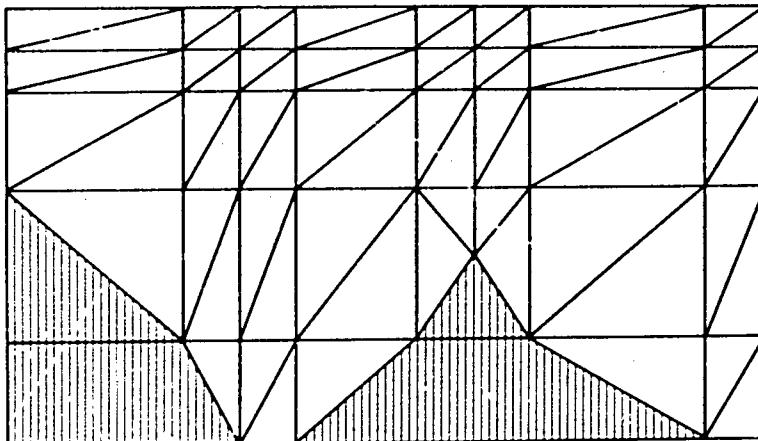


Fig. 5 — Typical network of triangular regions

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### Subroutine WORDSIZE

Subroutine WORDSIZE calculates some machine-dependent quantities. Four numbers are packed into array NCOUNT by using  $ITN$ , which is  $ITN = \sqrt[4]{1/4} JBIG$ , where  $JBIG$  is the largest integer, which will fit into one computer word. The four numbers in each location in NCOUNT are: number of turnovers for this ray, number of bottom reflections, number of turnunders, and number of surface reflections. ENTRY RAYTAPE writes one record on the ray tape. The first record will contain the title card. Each record contains:

NRAY (number of ray),  
 Range (meters),  
 Bottom depth (meters),  
 Tan  $\gamma$  (up is positive)  
 Ray depth (meters),  
 Signal strength (multiplicative factor),  
 NCOUNT (ray history),  
 Travel time (seconds),  
 Phase (radians).

}

Each one contains NRAY words. All tan  $\gamma$ 's precede all ray depths, etc.

### Subroutine ADVANCE

The basic function of subroutine ADVANCE is to advance the rays in the common block /RAYS/ from RSTART to RMAX. The procedure is as follows: First the proper triangle is found, the parabolic path is found, and intersections are calculated with the earliest intersection being used. Then surface and bottom reflections are performed. If ray is not at RMAX, the new triangle is determined, and a loop is made in the procedure to the calculation of intersections.

The explanation of various sections is as follows:

TANSUM (ADVA0012, Appendix A) is the tangent sum formula

$$\tan(\theta_1 + \theta_2) = \frac{\tan \theta_1 + \tan \theta_2}{1 - \tan \theta_1 * \tan \theta_2}.$$

DELT gives the time increment of a ray in terms of the range increment DR, the two tangents  $T$  and  $S$ , and the vertex velocity  $CMIS = 1/c_m^2$ .

The DO 100 IRAY = 1, NRAY (ADVA0015) (card sequence number) selects each ray in turn.

ADVA0018 checks to see if a ray has been terminated.

ADVA0019 through ADVA0023 move the ray variables into local variables.

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The DO 20  $I = 1$ , NRTI (ADVA0024 through ADVA0030) checks each triangle to see if the ray is in it. If a ray is on a boundary, it is in the layer it is pointing toward.

$C \cos \theta$ ,  $ST(\sin \theta)$ , (rotation), and ZO and RO (displacement) define the primed frame of reference in which there is no  $r'$  gradient.

ZRP and RRP are the initial primed ray position.

CIS =  $1/c^2$  at the ray.

Note: that TGR from TGAM (IRAY) is + for up rays and - for down rays, whereas TGRP =  $DZ'/dr'$  is + for down rays and - for up rays.

ALPHA ( $\alpha$ ) is the path curvature:

$$Z' = ZRP + TGRD*(r' - RRP) + ALPHA*(r' - RRP)^2$$

$$TA = 2\alpha = \frac{d^2 Z'}{dr'^2}.$$

The quadratic equation solved in advance is

$$C + Py - \alpha y^2 = 0,$$

where  $y = DRP = \text{change in } r' = RPNEW - RRP$ . ALPHA ( $\alpha$ ) is often small and is zero for isovelocity layers. For small  $\alpha$  the root

$$y = (P - \sqrt{P^2 + 4\alpha C})/2\alpha$$

is unstable. However, if  $\alpha$  is small, the iteration  $y = (\alpha y^2 - C)/P$  converges fast. The statement  $DRP = (\text{ALPHA} * ((\text{ALPHA} * DRP**2 - C)/P)**2 - C)/P$  is a double application of the above iteration and is used when

$$F = P - \sqrt{P^2 + 4\alpha C} \ll P.$$

When  $\alpha = 0$ , special linear path statements are used (ADVA0055 through ADVA0065 and ADAV0171 through ADVA0174). After statement 40 (ADVA0085), the next position is selected.

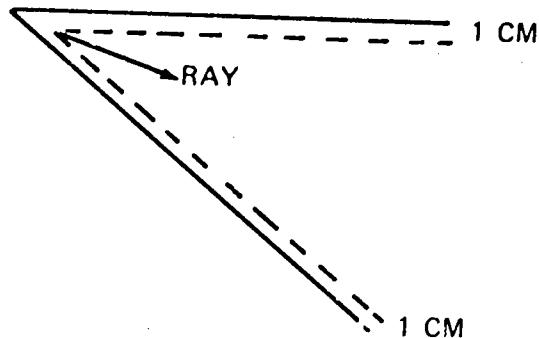
ONUP is true if a ray is on the upper boundary of a layer, meaning within 1 centimeter of the boundary and pointing in. ONLW is true if a ray is on the lower boundary.

There are four possibilities, in RPNEW, ZPNEW, ZNEW, and RNEW arrays. In general, the rule is

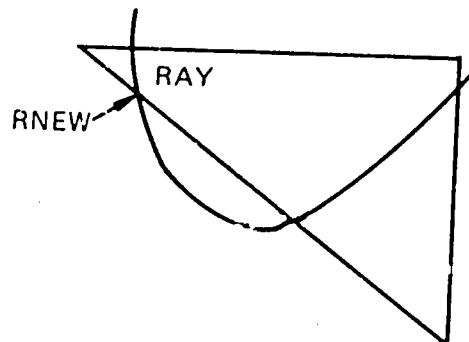
$$\text{RNEW} = \min(\text{RNEW}(k)) \text{ such that } \text{RNEW}(k) > RR.$$

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When a ray is on a boundary however the solution closest to the ray on that boundary is thrown out (ADVA0095, ADVA0096, ADVA0099, and ADVA100). Note, as shown in the following sketch, that a ray can be on both boundaries if it is on a corner.



If RNEW > RMAX, then the ray hits the vertical boundary (following sketch) and one goes to statement 50.



The cards from ADVA0129 to ADVA0163 increment the ray variables and decide on the next triangle.

ADVA0135 checks for vertices.

ADVA0136 decides whether a vertex is over or under.

ADVA0142 through ADVA0148 handles surface reflections.

ADVA0151 through ADVA0161 handles bottom reflections.

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Statement 50 starts the vertical boundary section. The boundary in the primed frame is  $Z' = AV + BVr'$ .

If  $ST = 0$ ,  $BV \rightarrow \infty$ ; hence small  $ST$ 's are handled by statement 60.

When two intersections are possible, the one with the smallest depth change is used.

Statement 52 checks for vertices.

The statements ADVA0204 and ADVA0205 (545) check the ray's final depth to be sure it is in the correct layer.

Volume attenuation is approximated by  $0.0001 \alpha$  (dB)/km  $V\Delta T$  decibels, since one should have  $S = \int v dt$  instead of  $V\Delta T$ .

The local variables are restored in the table ADVA0208 through ADVA0212, and a new ray is taken at statement 100.

Statements 60 through 68 (ADVA0214 through ADVA0235) use an iterative scheme to find the intersection with a vertical boundary. For  $ST = 0$  or  $\alpha = 0$  the first step is exact. The convergence limit is 1 centimeter, but seven steps are taken at once, so the usual error is very small.

Statement 80 terminates a ray and prints out the message RAY TERMINATED.

Statement 100 is the end of the outer loop of subroutine ADVANCE.

#### Subroutine PROFPLOT

Subroutine PRCFPLOT plots the input velocity profiles and also the bottom track on a Calcomp plot (Fig. 6). They may be plotted in range increments of nautical miles or kilometers. In Fig. 6 the three profiles are at 0, 107.6, and 1135.4 km, which ranges are indicated by + symbols on the abscissa axis. The total plot length is specified to give a suitable scale.

#### Subroutine RAYZDIST

Subroutine RAYZDIST prints out a ray depth distribution (Fig. 7) each time it is called. The following items will be printed: NRAY = number of ray, NTO - number of turnovers, NTU = number of turnunders, NSR = number of surface reflections, NBR = number of bottom reflections, DEPTH = current depth of ray, THETA = ray angle at the point in degrees, TIME = travel time of ray in seconds to this range. The losses column is  $10 \log_{10} SS$ , and is initially

$$10 \log_{10} [(\cos \theta_0) \Delta \theta_0] + SORLEV - \text{beam pattern.}$$

If SORLEV = beam pattern = 0 dB, and  $\Delta \theta_0 = 1^\circ$ , then losses start out -17.6 dB for a horizontal ray. In the plot line, B is the bottom, + is the lower vertex depth, \* is the present ray position, - is the upper vertex and S is the surface.

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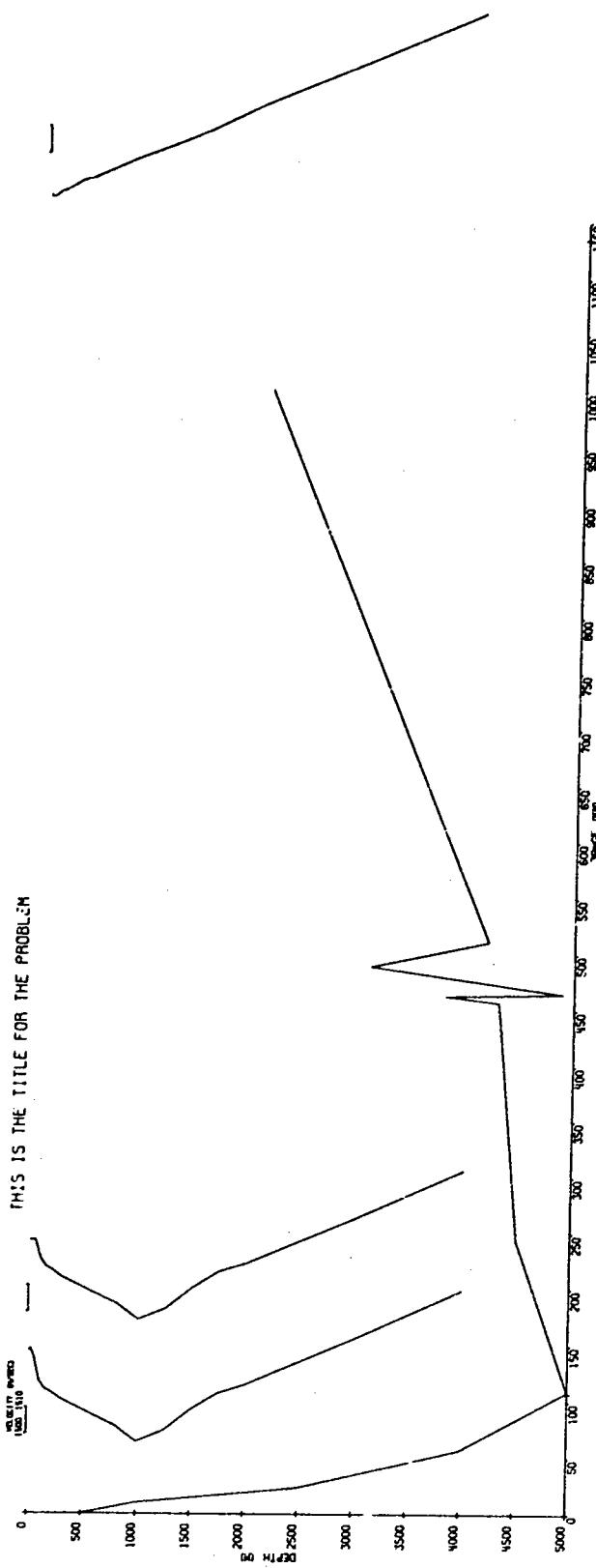


Fig. 6 — Colcomp plot of input profiles and the bottom track



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best available copy.

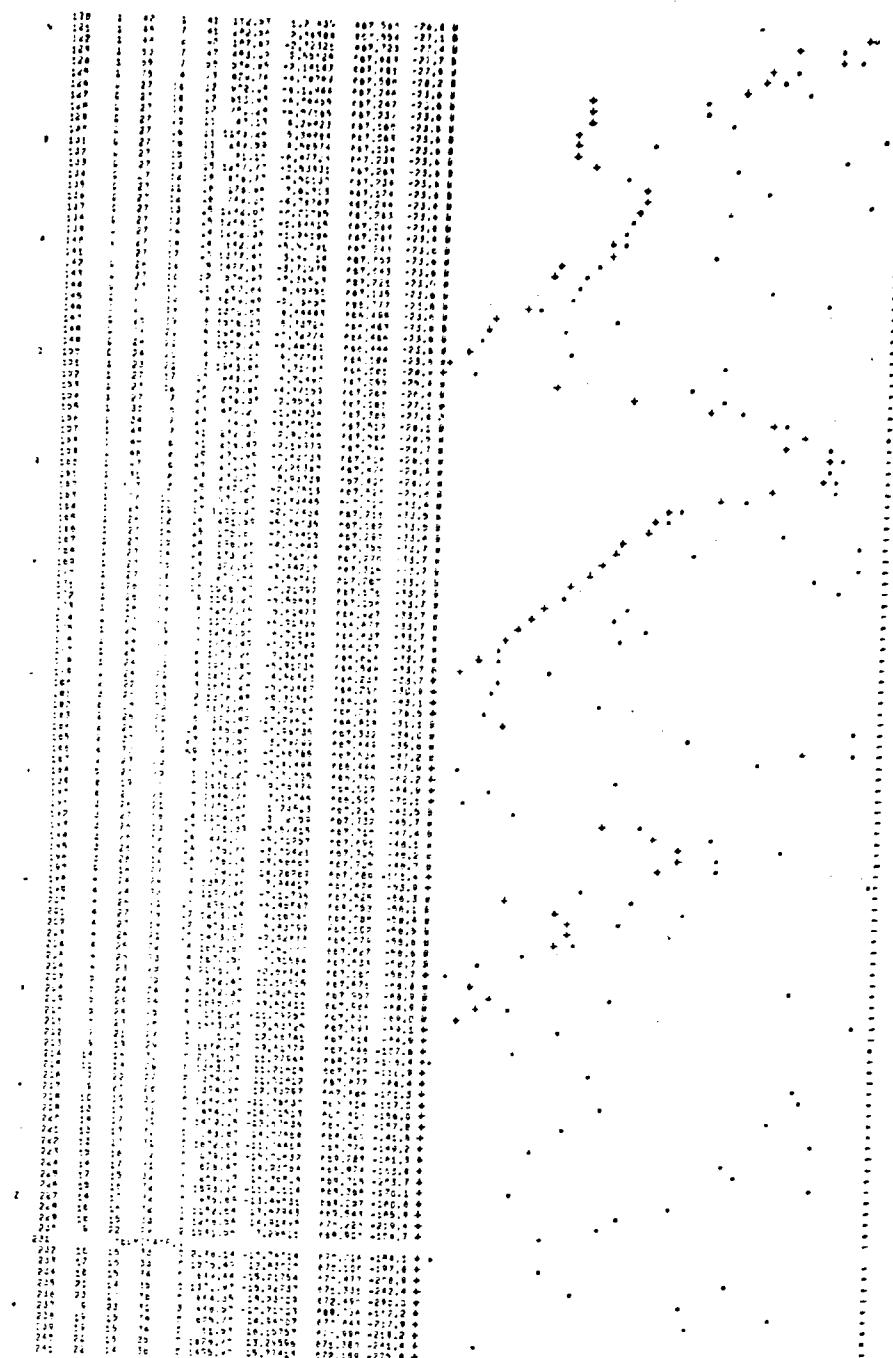


Fig. 7 (Continued) — Example of the output from RAYZLIST (second of four pages)

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RAY DEPTH DISTRIBUTION AT 10000 FEET ASL.			
RAY NO.	RAY DEPTH (FEET)	RAY DEPTH (FEET)	SCALAR
1	10000.000	10000.000	1.00000E+000
2	9999.999	10000.000	1.00000E+000
3	9999.998	10000.000	1.00000E+000
4	9999.997	10000.000	1.00000E+000
5	9999.996	10000.000	1.00000E+000
6	9999.995	10000.000	1.00000E+000
7	9999.994	10000.000	1.00000E+000
8	9999.993	10000.000	1.00000E+000
9	9999.992	10000.000	1.00000E+000
10	9999.991	10000.000	1.00000E+000
11	9999.990	10000.000	1.00000E+000
12	9999.989	10000.000	1.00000E+000
13	9999.988	10000.000	1.00000E+000
14	9999.987	10000.000	1.00000E+000
15	9999.986	10000.000	1.00000E+000
16	9999.985	10000.000	1.00000E+000
17	9999.984	10000.000	1.00000E+000
18	9999.983	10000.000	1.00000E+000
19	9999.982	10000.000	1.00000E+000
20	9999.981	10000.000	1.00000E+000
21	9999.980	10000.000	1.00000E+000
22	9999.979	10000.000	1.00000E+000
23	9999.978	10000.000	1.00000E+000
24	9999.977	10000.000	1.00000E+000
25	9999.976	10000.000	1.00000E+000
26	9999.975	10000.000	1.00000E+000
27	9999.974	10000.000	1.00000E+000
28	9999.973	10000.000	1.00000E+000
29	9999.972	10000.000	1.00000E+000
30	9999.971	10000.000	1.00000E+000
31	9999.970	10000.000	1.00000E+000
32	9999.969	10000.000	1.00000E+000
33	9999.968	10000.000	1.00000E+000
34	9999.967	10000.000	1.00000E+000
35	9999.966	10000.000	1.00000E+000
36	9999.965	10000.000	1.00000E+000
37	9999.964	10000.000	1.00000E+000
38	9999.963	10000.000	1.00000E+000
39	9999.962	10000.000	1.00000E+000
40	9999.961	10000.000	1.00000E+000
41	9999.960	10000.000	1.00000E+000
42	9999.959	10000.000	1.00000E+000
43	9999.958	10000.000	1.00000E+000
44	9999.957	10000.000	1.00000E+000
45	9999.956	10000.000	1.00000E+000
46	9999.955	10000.000	1.00000E+000
47	9999.954	10000.000	1.00000E+000
48	9999.953	10000.000	1.00000E+000
49	9999.952	10000.000	1.00000E+000
50	9999.951	10000.000	1.00000E+000
51	9999.950	10000.000	1.00000E+000
52	9999.949	10000.000	1.00000E+000
53	9999.948	10000.000	1.00000E+000
54	9999.947	10000.000	1.00000E+000
55	9999.946	10000.000	1.00000E+000
56	9999.945	10000.000	1.00000E+000
57	9999.944	10000.000	1.00000E+000
58	9999.943	10000.000	1.00000E+000
59	9999.942	10000.000	1.00000E+000
60	9999.941	10000.000	1.00000E+000
61	9999.940	10000.000	1.00000E+000
62	9999.939	10000.000	1.00000E+000
63	9999.938	10000.000	1.00000E+000
64	9999.937	10000.000	1.00000E+000
65	9999.936	10000.000	1.00000E+000
66	9999.935	10000.000	1.00000E+000
67	9999.934	10000.000	1.00000E+000
68	9999.933	10000.000	1.00000E+000
69	9999.932	10000.000	1.00000E+000
70	9999.931	10000.000	1.00000E+000
71	9999.930	10000.000	1.00000E+000
72	9999.929	10000.000	1.00000E+000
73	9999.928	10000.000	1.00000E+000
74	9999.927	10000.000	1.00000E+000
75	9999.926	10000.000	1.00000E+000
76	9999.925	10000.000	1.00000E+000
77	9999.924	10000.000	1.00000E+000
78	9999.923	10000.000	1.00000E+000
79	9999.922	10000.000	1.00000E+000
80	9999.921	10000.000	1.00000E+000
81	9999.920	10000.000	1.00000E+000
82	9999.919	10000.000	1.00000E+000
83	9999.918	10000.000	1.00000E+000
84	9999.917	10000.000	1.00000E+000
85	9999.916	10000.000	1.00000E+000
86	9999.915	10000.000	1.00000E+000
87	9999.914	10000.000	1.00000E+000
88	9999.913	10000.000	1.00000E+000
89	9999.912	10000.000	1.00000E+000
90	9999.911	10000.000	1.00000E+000
91	9999.910	10000.000	1.00000E+000
92	9999.909	10000.000	1.00000E+000
93	9999.908	10000.000	1.00000E+000
94	9999.907	10000.000	1.00000E+000
95	9999.906	10000.000	1.00000E+000
96	9999.905	10000.000	1.00000E+000
97	9999.904	10000.000	1.00000E+000
98	9999.903	10000.000	1.00000E+000
99	9999.902	10000.000	1.00000E+000
100	9999.901	10000.000	1.00000E+000

Fig. 7 (Continued) -- Example of the output from RAYZDIST (third of four pages)

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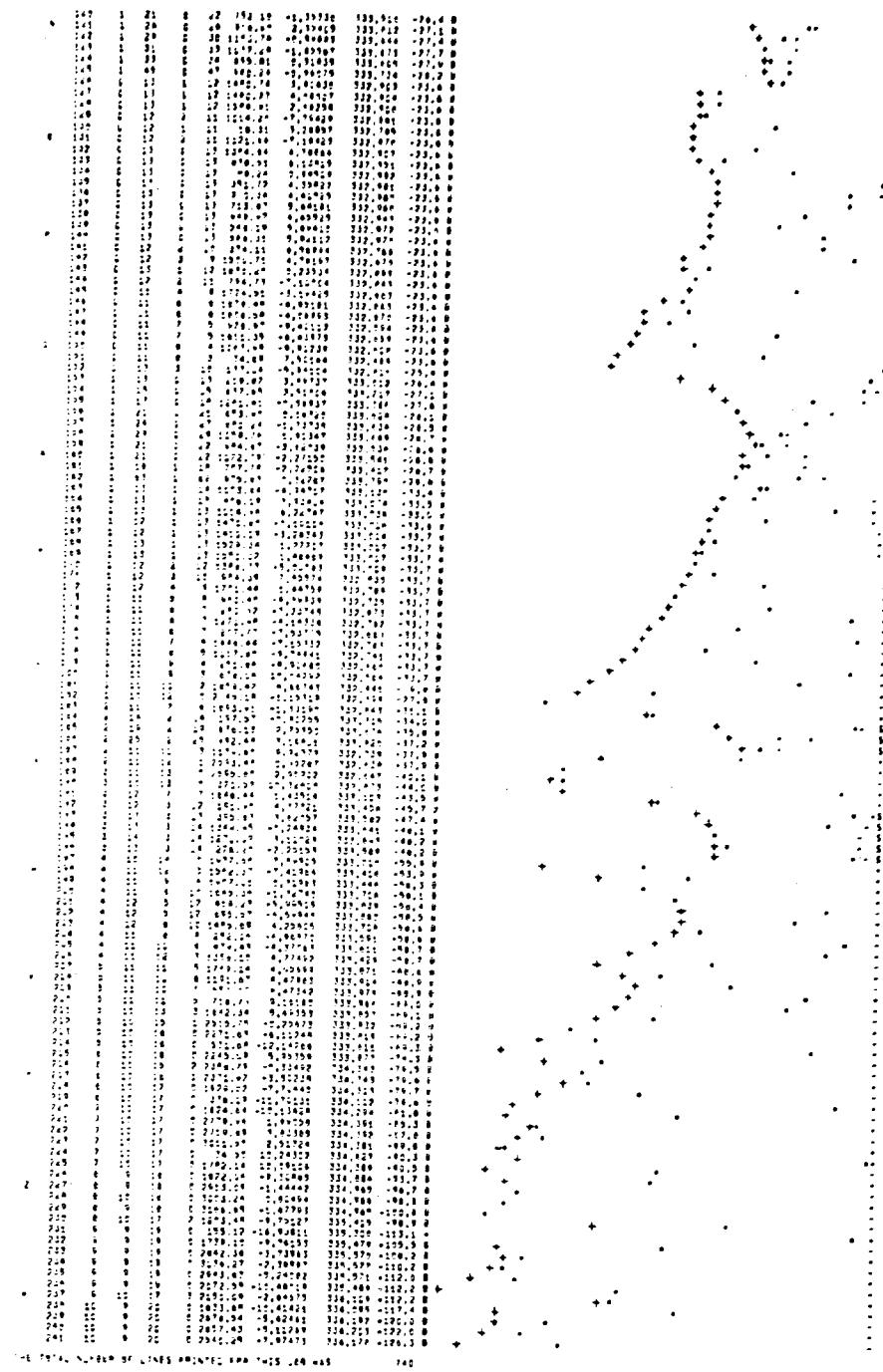


Fig. 7 (Continued) — Example of the output from RAYZDIST (fourth of four pages)

## NRL REPORT 7827

**Subroutine CHANNEL**

Subroutine CHANNEL calculates CM (vertex velocity) from ZR (ray depth) and  $T$  (tangent of the ray angle) and then finds ZTO (ray turnover depth) and ZTU (ray turn-under depth). The entry RCALC then calculates

$$R = \int_{ZTO}^{ZTU} \frac{1}{\tan \theta} dZ,$$

where  $R$  is the cycle length of the ray, which is used for the type III intensity calculations. The entry WDENS then calculates the probability density  $P(z)$  that a ray will be found at a depth  $z$ :

$$P(z) = \frac{1}{(\tan \theta)/R},$$

which is the type III depth distribution.

**Subroutine VELCALC**

Subroutine VELCALC calculates a velocity profile at each selected range for internal calculations (not a profile range or bottom point) using the information in the common block /TRIANG/.

**Subroutine RAYPLOT**

Each entry to RAYPLOT plots one line of the printer plot. In addition the first entry prints the heading for the plot, determines which rays will be plotted, and sets the scale. NP and ZMAX are used only on the first entry. Fig. 8 is an example of the printer plot.

**Subroutine PROFPLIT**

Subroutine PROFPLIT plots both the input and interpolated profiles on a Calcomp plot. They may be plotted in nautical miles or kilometers. The total plot length is specified in inches. The bottom track is also plotted.

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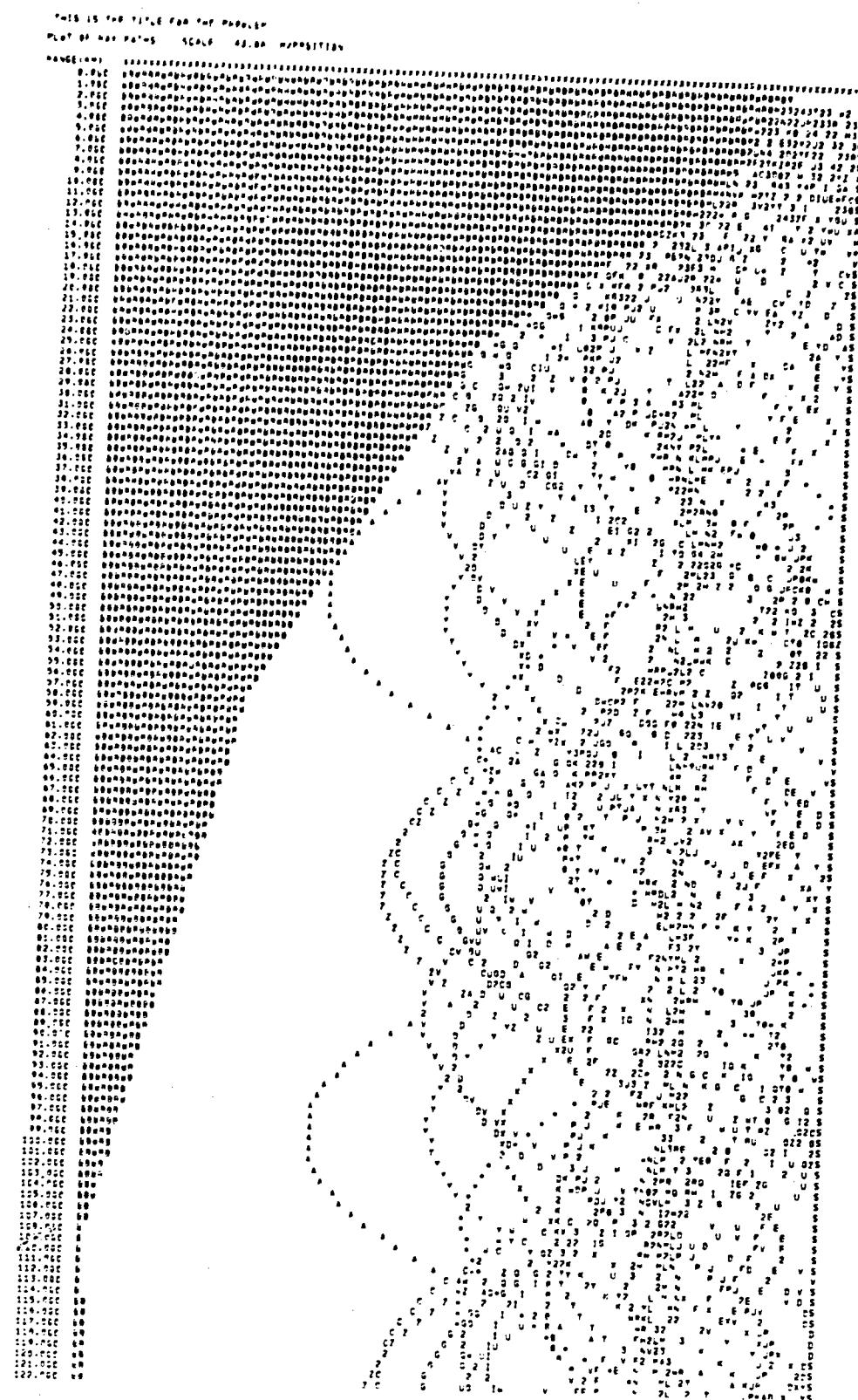
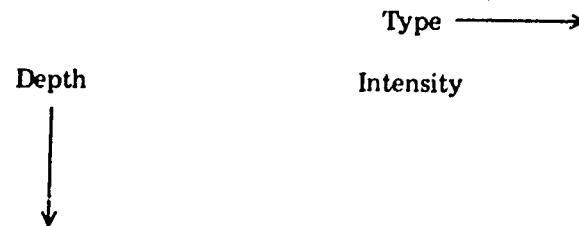


Fig. 8 — Ray plot

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**Subroutine ITNPRINT**

Subroutine ITNPRINT prints out the intensities. If receiver depths are the same for all intensity calculations, a table of intensities such as shown in Fig. 9 is printed. Otherwise a printer plot for each range with the arrangement



is printed.

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THIS IS THE TITLE FOR THE PROBLEM  
RECEIVED INTENSITY VS RANGE AT DEPTHS

RANGE	TYPE	50,000	100,000	250,000	350,000	450,000
1,000	0	-57.4	-57.5	-57.5	-57.6	-57.3
2,000	0	-62.4	-62.0	-62.7	-62.7	-62.4
3,000	0	-65.1	-64.7	-64.4	-64.0	-65.0
4,000	0	-67.6	-67.1	-66.5	-66.6	-68.3
5,000	0	-71.8	-72.3	-72.0	-71.6	-70.8
5,000	0	-69.1	-71.1	-70.6	-70.6	-70.5
6,000	0	-76.4	-81.1	-80.4	-79.8	-79.4
7,000	0	-77.4	-80.1	-79.1	-79.1	-74.2
8,000	0	-80.0	-84.6	-82.4	-79.7	-72.6
9,000	0	-78.1	-85.8	-82.2	-79.3	-73.5
10,000	1	-80.1	-77.8	-77.3	-76.6	-76.1
10,000	0	-82.9	-85.1	-78.8	-77.6	-76.0
11,000	0	-85.4	-87.4	-87.7	-86.1	-76.2
12,000	0	-91.6	-83.1	-87.7	-88.6	-81.2
13,000	0	-93.1	-85.9	-84.4	-84.0	-87.3
14,000	0	-94.9	-84.7	-87.8	-87.9	-84.7
15,000	1	-94.4	-83.7	-84.6	-81.6	-79.4
15,000	0	-94.3	-87.4	-81.3	-84.7	-89.0
16,000	0	-92.1	-86.5	-87.3	-89.3	-86.5
17,000	0	-114.7	-96.1	-99.8	-92.0	-98.5
18,000	0	-119.0	-113.7	-99.7	-89.1	-91.6
19,000	0	-112.8	-114.4	-93.3	-89.7	-89.0
20,000	1	-99.5	-86.7	-84.1	-82.3	-72.9
20,000	0	-119.4	-115.1	-114.8	-94.5	-90.9
21,000	0	-129.6	-117.5	-121.3	-122.6	-88.7
22,000	0	-138.6	-120.1	-120.3	-122.3	-122.5
23,000	0	-143.0	-119.4	-125.9	-121.6	-123.5
24,000	0	-145.4	-127.1	-121.5	-123.0	-123.0
25,000	0	-98.2	-87.8	-89.3	-70.3	-84.1
25,000	0	-143.0	-137.2	-120.8	-123.2	-123.3
26,000	0	-142.7	-139.9	-121.2	-122.9	-125.2
26,000	0	-147.1	-132.7	-120.8	-123.7	-84.9
26,000	0	-145.5	-133.4	-118.6	-124.0	-89.4
27,000	0	-117.1	-141.6	-125.7	-123.3	-99.6
28,000	0	-99.0	-88.7	-85.3	-84.6	-84.9
29,000	0	-158.9	-132.9	-119.6	-122.9	-99.4
31,000	0	-135.0	-134.7	-115.5	-123.0	-121.5
32,000	0	-162.2	-133.1	-115.1	-124.0	-111.2
33,000	0	-159.5	-135.1	-121.9	-124.2	-113.3
34,000	0	-180.0	-136.4	-123.0	-112.8	-113.3
35,000	0	-100.8	-89.3	-88.0	-85.2	-85.6
35,000	0	-166.6	-119.1	-124.5	-115.5	-92.7
36,000	0	-166.0	-165.7	-121.4	-117.9	-84.0
37,000	0	-165.6	-119.5	-127.5	-118.5	-86.3
38,000	0	-163.8	-121.6	-128.6	-114.5	-80.4
39,000	0	-164.0	-124.3	-124.1	-118.8	-85.1
40,000	1	-161.6	-88.9	-86.6	-85.8	-86.2
40,000	0	-163.1	-124.8	-101.4	-80.0	-89.3
41,000	0	-174.0	-104.3	-88.9	-78.3	-88.4
42,000	0	-102.3	-101.7	-81.3	-79.5	-87.0
43,000	0	-94.3	-94.7	-91.9	-81.1	-82.3
44,000	0	-98.2	-94.4	-84.3	-80.9	-83.6
45,000	0	-102.3	-96.4	-87.1	-86.3	-86.7
45,000	0	-97.5	-97.4	-82.9	-82.2	-83.8
46,000	0	-98.2	-99.4	-79.2	-81.3	-83.5
47,000	0	-99.1	-98.9	-85.1	-85.0	-79.0
48,000	0	-99.6	-98.8	-85.3	-81.6	-78.9
49,000	0	-100.1	-100.7	-81.6	-87.7	-84.1
50,000	1	-102.9	-99.9	-87.6	-86.0	-87.1
50,000	0	-100.4	-86.5	-79.6	-89.5	-95.2
51,000	0	-99.1	-85.7	-75.3	-89.9	-89.6
52,000	0	-101.3	-74.5	-84.3	-88.7	-88.1
53,000	0	-101.5	-99.2	-82.8	-84.4	-87.5
54,000	0	-100.6	-95.4	-82.5	-84.1	-89.2
55,000	0	-103.4	-91.3	-85.0	-84.1	-87.5
55,000	0	-120.0	-97.3	-85.1	-84.4	-95.0
56,000	0	-103.4	-93.1	-85.2	-84.7	-86.8
57,000	0	-85.1	-95.3	-94.2	-84.3	-89.2
58,000	0	-93.9	-91.0	-86.3	-101.3	-94.8
59,000	0	-99.4	-93.8	-92.3	-100.5	-87.5
60,000	0	-103.9	-93.7	-86.5	-83.1	-87.9
60,000	0	-110.0	-93.8	-87.1	-97.6	-93.6
61,000	0	-110.1	-94.0	-97.9	-98.3	-98.9
62,000	0	-116.4	-110.1	-101.5	-100.5	-94.8
63,000	0	-127.1	-107.9	-100.7	-101.1	-101.1
64,000	0	-156.7	-105.7	-97.0	-102.0	-102.6
65,000	0	-124.3	-92.0	-88.7	-87.9	-88.3
65,000	0	-115.1	-108.0	-108.9	-99.1	-102.7
66,000	0	-128.9	-114.5	-113.7	-100.7	-100.0
67,000	0	-140.4	-124.1	-122.0	-124.5	-101.5
68,000	0	-133.0	-125.7	-119.9	-129.9	-127.7
69,000	0	-135.3	-123.3	-122.2	-130.5	-119.1
70,000	0	-109.1	-92.4	-59.0	-88.3	-88.6
70,000	0	-138.1	-130.9	-127.4	-129.0	-120.2
72,000	0	-138.9	-130.2	-129.5	-116.6	-111.6
72,000	0	-134.4	-135.2	-127.4	-120.2	-93.4
73,000	0	-142.3	-136.1	-126.5	-121.3	-87.1
74,000	0	-147.9	-143.9	-126.0	-123.7	-87.4
75,000	0	-125.3	-115.7	-89.3	-88.5	-86.0
75,000	0	-144.4	-137.2	-135.9	-124.6	-87.3
76,000	0	-155.9	-138.9	-136.3	-124.2	-81.1
77,000	0	-156.4	-144.6	-136.8	-136.2	-81.6
78,000	0	-156.8	-134.6	-130.8	-84.4	-81.9
79,000	0	-143.9	-133.0	-133.0	-82.7	-87.7
80,000	1	-105.6	-93.1	-84.6	-85.8	-86.2
80,000	0	-100.0	-143.2	-126.8	-85.9	-87.5
81,000	0	-300.0	-101.2	-90.9	-83.5	-87.4
82,000	0	-300.0	-140.5	-92.9	-86.2	-89.5
83,000	0	-171.1	-124.6	-88.6	-87.5	-89.3
84,000	0	-111.1	-111.1	-88.5	-91.8	-89.1

Fig. 9 — Example of an output from ITNPRINT (first of three pages). The symbols that the subroutine uses in the second column are R for type I random phase calculations, S for type I coherent phase calculations, 2 for type II calculations, and 3 for type III calculations.

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Fig. 9 – Example of an output from ITNPRINT (second of three pages)

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559,009	3	-96,7	-97,6	-97,5	-97,8	-97,8
510,000	3	-97,0	-97,7	-97,5	-97,8	-97,7
511,000	1	-97,2	-97,9	-97,3	-97,9	-98,0
522,000	3	-97,4	-97,9	-97,5	-97,9	-97,7
523,000	3	-97,2	-98,0	-97,7	-98,0	-97,7
530,000	3	-97,6	-97,8	-97,9	-98,1	-97,7
531,000	1	-97,6	-97,4	-97,6	-98,2	-97,7
540,000	1	-98,6	-97,7	-98,0	-98,2	-97,7
545,000	1	-97,1	-97,7	-97,9	-98,3	-97,7
556,000	3	-97,2	-97,8	-98,0	-98,3	-97,7
555,000	3	-97,3	-97,9	-98,1	-98,2	-98,0
560,000	3	-98,9	-97,4	-99,2	-99,2	-98,1
569,000	3	-98,6	-97,7	-99,3	-99,3	-98,1
578,000	1	-98,6	-97,7	-99,3	-99,3	-98,1
579,000	1	-98,9	-97,1	-99,4	-99,1	-98,1
580,000	3	-98,6	-97,7	-99,5	-99,5	-98,1
585,000	3	-98,5	-98,7	-98,3	-99,7	-98,1
590,000	1	-98,5	-98,5	-98,0	-99,1	-98,1
595,000	1	-98,4	-98,5	-98,0	-99,2	-97,7
600,000	1	-98,6	-98,4	-98,4	-99,3	-97,8
605,000	1	-98,6	-98,4	-98,4	-99,3	-97,8
613,000	1	-97,0	-98,5	-98,5	-99,3	-97,5
615,000	1	-97,2	-98,4	-98,6	-99,4	-97,9
628,000	3	-97,0	-98,5	-98,3	-99,5	-98,1
625,000	1	-97,7	-98,4	-98,5	-99,3	-98,2
630,000	3	-97,1	-98,5	-98,3	-99,7	-98,2
635,000	1	-97,7	-98,5	-98,7	-99,1	-98,3
640,000	3	-98,1	-98,6	-98,7	-99,5	-98,4
645,000	3	-98,0	-98,7	-98,7	-99,0	-98,5
650,000	3	-98,1	-98,7	-98,8	-99,1	-98,5
655,000	3	-98,4	-98,9	-98,8	-99,3	-98,6
660,000	3	-98,4	-98,7	-98,8	-99,4	-98,6
665,000	3	-98,2	-98,6	-98,5	-99,5	-98,6
670,000	3	-98,6	-98,7	-98,8	-99,4	-98,6
675,000	3	-98,7	-98,5	-98,5	-99,5	-98,7
680,000	1	-98,6	-98,2	-98,4	-99,5	-98,7
685,000	1	-98,8	-98,7	-98,6	-99,4	-98,7
690,000	1	-97,8	-98,7	-98,4	-99,4	-98,7
695,000	1	-98,0	-98,1	-98,2	-99,4	-98,7
700,000	3	-98,8	-98,1	-98,2	-99,4	-98,7
706,000	3	-98,6	-98,1	-98,2	-99,4	-98,7
705,000	1	-98,4	-98,1	-98,2	-99,4	-98,9
710,000	1	-98,7	-98,1	-98,2	-99,4	-98,9
715,000	3	-98,7	-98,1	-98,2	-99,4	-98,9
720,000	3	-98,8	-98,2	-98,3	-99,4	-98,9
725,000	3	-98,9	-98,2	-98,3	-99,4	-98,9
730,000	5	-98,1	-98,2	-98,2	-99,5	-98,7
735,000	3	-99,2	-98,2	-98,2	-99,1	-98,0
740,000	3	-99,3	-98,7	-98,2	-99,5	-98,0
745,000	3	-98,3	-98,4	-98,4	-99,6	-98,0
750,000	3	-98,3	-98,4	-98,4	-99,6	-97,1
755,000	3	-98,3	-98,4	-98,4	-99,7	-97,1
760,000	3	-98,6	-98,5	-98,9	-97,3	-97,4
765,000	3	-98,7	-98,4	-98,4	-97,2	-97,6
770,000	3	-98,7	-98,4	-98,4	-97,2	-97,6
775,000	3	-98,7	-98,5	-98,3	-98,7	-97,6
780,000	3	-98,7	-98,5	-98,3	-98,7	-97,6
785,000	3	-98,7	-98,6	-98,4	-98,6	-97,8
790,000	3	-98,7	-98,7	-98,4	-98,5	-97,9
795,000	3	-98,7	-98,7	-98,4	-98,5	-98,0
800,000	3	-98,4	-98,7	-98,3	-98,9	-98,0
805,000	3	-98,4	-98,7	-98,3	-98,9	-98,0
810,000	3	-98,4	-98,7	-98,2	-98,6	-97,9
815,000	3	-98,4	-98,7	-98,2	-98,7	-97,9
820,000	3	-98,4	-98,7	-98,2	-98,7	-97,9
825,000	1	-98,2	-98,7	-97,8	-98,6	-97,9
830,000	1	-98,6	-98,7	-97,6	-98,6	-97,9
835,000	3	-98,6	-98,7	-97,3	-98,5	-97,8
840,000	1	-98,6	-98,7	-97,9	-98,6	-97,8
845,000	3	-98,6	-98,5	-97,0	-98,6	-97,9
850,000	1	-98,6	-98,5	-97,0	-98,5	-98,1
855,000	1	-98,6	-98,5	-97,0	-98,5	-98,1
860,000	3	-98,7	-98,5	-98,3	-98,5	-98,1
865,000	3	-98,7	-98,5	-98,3	-98,5	-98,1
870,000	3	-98,7	-98,6	-98,4	-98,5	-98,1
875,000	3	-98,7	-98,6	-98,4	-98,5	-98,1
880,000	1	-98,1	-98,6	-98,3	-98,1	-98,7
885,000	3	-98,4	-98,4	-98,3	-98,1	-98,7
890,000	3	-98,3	-98,5	-98,5	-98,1	-98,6
895,000	3	-98,4	-98,5	-98,6	-98,1	-98,6
900,000	3	-97,6	-98,7	-98,6	-97,4	-98,6
905,000	1	-97,6	-98,7	-98,6	-97,2	-98,6
910,000	1	-97,7	-98,4	-98,6	-97,2	-98,7
915,000	3	-98,1	-98,4	-98,8	-98,1	-98,7
920,000	3	-98,2	-98,4	-98,6	-98,2	-98,6
925,000	3	-98,3	-98,5	-98,7	-98,3	-98,5
930,000	1	-98,3	-98,5	-98,7	-98,3	-98,5
935,000	1	-98,2	-98,7	-98,6	-97,4	-98,6
940,000	1	-98,4	-98,4	-98,6	-98,6	-98,9
945,000	1	-98,5	-98,6	-98,8	-98,3	-98,9
950,000	3	-98,0	-98,4	-98,6	-98,1	-98,9
955,000	1	-98,4	-98,4	-98,6	-98,1	-98,7
960,000	1	-98,6	-98,4	-98,6	-97,9	-98,8
965,000	1	-97,7	-98,7	-98,2	-98,2	-98,5
970,000	1	-97,7	-98,7	-98,2	-98,2	-98,6
975,000	5	-97,9	-98,7	-98,4	-98,9	-98,8
980,000	1	-98,1	-98,7	-98,4	-98,9	-98,7
985,000	3	-98,1	-98,7	-98,3	-98,5	-98,7
990,000	1	-98,1	-98,7	-98,3	-98,5	-98,6
995,000	1	-98,2	-98,7	-98,3	-98,5	-98,6
1000,000	3	-98,3	-98,7	-98,4	-98,9	-98,7
1000,000	3	-98,3	-98,7	-98,4	-98,9	-98,7

Fig. 9 — Example of an output from ITNPRINT (third of three pages)

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**Subroutine IVSRPLOT**

Subroutine IVSRPLOT plots intensity versus range (Fig. 10). The first entry prints the heading, chooses the correct type of calculation, and then plots a line or the first range. Each succeeding call plots just a line for another range. Only one type may be plotted per data case.

**Subroutine INTENSTY**

Subroutine INTENSTY calculates all intensities. The switches ISCP, IT1, IT2, and IT3 determine what is calculated. When one selects coherent phase (ISCP = 1) one must also select random phase (IT1 = 1). Coherent phase intensity takes the phase of the ray into account in the calculations. If  $SL$  is a function of the random-phase sound level, then the coherent sound level is  $(\sqrt{SL} \cdot \cos(P))^2 + (\sqrt{SL} \cdot \sin(P))^2$ , where  $P$  is the phase angle. To get each, set IT2 = 1 for type II calculations and IT3 = 1 for type III calculations.

The only caustic correction which is applied to type I calculations is a ray-separation criterion: if two rays are closer together than 0.001 meter in depth, the eigenray for these two rays is thrown out. Type II and Type III intensity calculations do not have caustics.

**Subroutine RECOVERY**

Subroutine RECOVERY has two entry points: DUMP and RESTART. Its function is to enable one to restart a program. DUMP writes all the core locations on a tape when it is called, and RESTART restores core to its previous condition when it is called by reading the tape from DUMP.

**Subroutine RETRY**

Subroutine RETRY enables one to restart a program in which the multiple replacement option has been used (as was discussed for card II in the Input Description). Its chief function is to read any profile cards which have not yet been read and to write them on logical unit 6 for subroutine NEWPROF to read when required.

**Subroutine CLOSEIOP**

The function of subroutine CLOSEIOP is to alleviate a systems problem in punching intensity cards when using RESTART. Without this subroutine the cards would be punched in binary instead of BCD when RESTART is called. This subroutine might not be required in another computer system, if the proper modeing of logical units is accomplished automatically.

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THIS IS THE TITLE FOR THE PLOTTER  
RECEIVED INTENSITY IN RANGE  
RECEIVED AT SEVEN PLATES AS

45.000	.
145.000	2
245.000	3
345.000	4
445.000	5

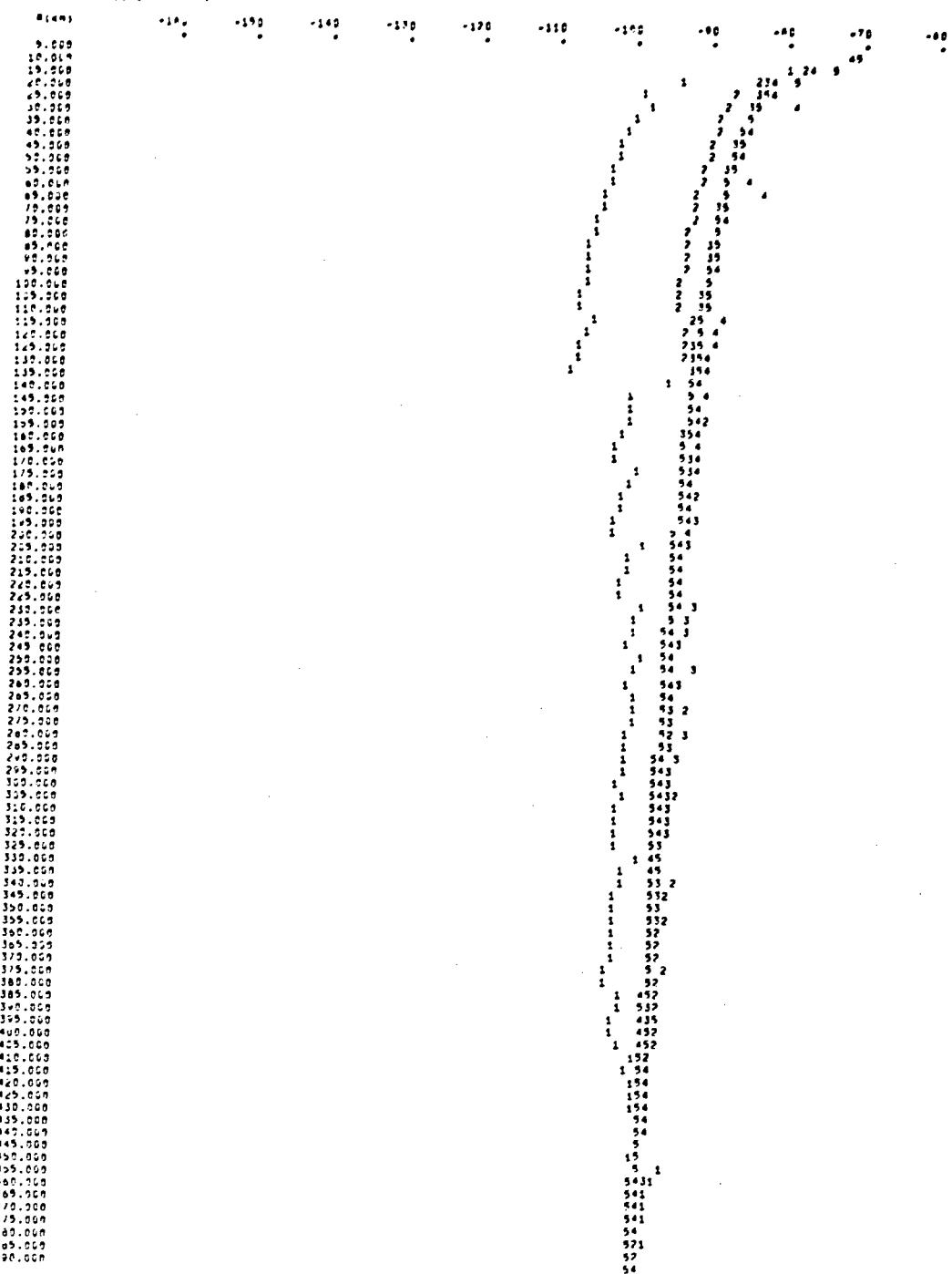


Fig. 10 — Example of the output from IVSRPLOT

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**Subroutine BYEBYE**

Subroutine BYEBYE is called in place of the Fortran statement STOP to terminate the program. It was written to avoid a CDC3800 systems problem when DUMP is called in the executive program. It might not be necessary to have this in another computer system, in which case the STOP statement could be reinserted, if desired.

**DIFFERENT INTENSITIES IN TRIMAIN**

In subroutine RAYZDIST (ray depth distribution) a quantity is printed titled LOSSES (Fig. 6). This quantity is equal to  $10 \log_{10} (S)$ , where  $S$  represents all the losses due to bottom interactions, surface interactions, and volume attenuation. Spreading loss is not included in these figures.

In subroutine INTENSTY a quantity is printed for the eigenray printout called  $SL$  (DB). If we let  $SS(I)$  denote the quantity called  $S$  in RAYZDIST for the current ray and  $SS(I-1)$  denote  $S$  for the previous ray, then we let  $S1 = \text{secant } (\text{current ray angle}) [SS(I-1)]$  and let  $DS = \text{secant } (\text{previous ray angle}) [SS(I)-S1]$ . The ray depth at a given point may be identified as  $ZZ(I)$ . So if we are considering ray  $I$ , then  $Z1 = ZZ(I-1)$  and  $DZ = ZZ(I) - Z1$ . If  $ZR$  is the receiver depth, then we let  $F = (ZR - Z1)/DZ$ . We let  $RMAX$  be the range to this point in meters. Then we define a quantity  $SL = (S1 + F DS)/[RMAX ABS(DZ)]$ . Thus the quantity printed for  $SL$ (DB) is  $10 \log_{10} (SL)$ .

The third parameter which is printed is the type I intensity and is derived in subroutine INTENSTY. This set consists of summing all the eigenrays, or the  $SL$ , for a given receiver and range point and then computing

$$10 \log \sum_{i=1}^N SL_i \text{ (incoherent or random phase sum),}$$

where  $N$  is the number of eigenrays determined for this point. If the Lloyd's mirror switch is not on, the final intensity value can be arrived at as stated, but if the Lloyd's mirror switch is on, each eigenray is multiplied by a factor before they are summed; thus it is not always possible to sum the eigenrays as printed to arrive at the final intensity.

The type II intensity calculation was initially proposed [2] using a Gaussian distribution, which smears a ray over a displaced bundle of intensity. DZBAR is a size parameter for that smearing and is defined by  $DZBAR = SDZ/SW$ , where we are using the mean absolute difference between ray depths, weighted by the signal strength of the ray, such that

$$SW = \sum_{i=2}^{NRAY} W_i = \sum_{i=2}^{NRAY} \min (SS_i, SS_i - 1),$$

which is the sum of the weights, and

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$$SDZ = \sum_{i=2}^{NRAY} w_i (ZZ_i - ZZ_{i-1})$$

which is the sum of the weighted mean differences.

If DZBAR is less than a wavelength, then DZBAR is set equal to a wavelength.  $DZM = ZB/\sqrt{NRAY}$ , where  $ZB$  is the bottom depth and  $NRAY$  is the number of rays traced. If DZBAR is greater than  $DZM$ , then  $DZBAR = DZM$ . This is a check to see that DZBAR is not a large fraction of the bottom depth. If 100 rays were traced, then DZBAR would never be larger than 1/10 of the bottom depth.

If RMAX is the range of this point, then let  $F = 2.0 * RMAX * DZBAR$ . Let  $ER = e^{-(ZR/DZBAR)}$ , where  $ZR$  is the receiver depth, let  $EB = e^{-(ZB/DZBAR)}$ , and let  $EZ = e^{-(ZZ(I)/DZBAR)}$ . Now  $SL = B * \sec\theta * SS(I)/F$  where  $B$  is the volume attenuation. If a ray is close to the bottom, it does not get its full share of the intensity, since the intensity is distributed exponentially on either side of the ray. Thus, it is necessary to renormalize the distribution by saying  $SL = SL/(1 - .5 * ((EB/EZ) + EZ))$ .

We now want to calculate the quantity  $A = e^{-(ABS(ZZ(I)-ZR)/DZBAR)}$ , which expression is always less than 1.0. The final expression for each ray is then  $S_i = SL * A$ . The final intensity at a receiver is given by computing, in subroutine ITNPRINT,

$$10 \log \sum_{i=1}^N S_i$$

In calculating the Type III intensity [2] it is assumed that a current velocity profile prevails to represent a local average over a convergence zone, which wipes out the phase of a ray. The ray turnover and turnunder depths are calculated for each ray, and then the ray cycle length is computed. Next the expression  $SL = B * SS(I)/RMAX$  is computed to get cylindrical spreading. If a given receiver is between the turnunder and turnover depths, entry WDENS is called, which returns the parameter  $S$ , the signal strength parameter, which represents the probability density that the ray is at this depth. This probability density  $T = 1/ABS(TAN\theta)$  is normalized in WDENS by dividing by the ray cycle length. The cylindrical spreading term is multiplied by signal-strength parameter  $S_i$  to get a contribution for each ray which is then summed as

$$10 \log \sum_{i=1}^N SL_i * S_i$$

to arrive at the final values.

## EIGENRAY OUTPUT OPTION

The computer coding for the eigenray output option appears within the subroutine INTENSTY. If a request is made either for type I random intensity or type I coherent intensity, then it is possible to obtain an eigenray output (Fig. 11) by setting column 25 on the output control card (card group V in Fig. 1) equal to 1. The concept of an eigenray may be envisioned as an interpolated ray which will strike a receiver and is found by linearly interpolating between two rays which bracket a receiver. For certain cases eigenrays will be formed from rays which do not bracket a receiver. This is caused primarily by consecutive rays which have different histories; in this case there is some ray between the two existing rays which would give an eigenray if it were traced. Thus the program extrapolates a value. The program prefers two rays with the same history which bracket a receiver. This represents an IQUAL of 1. If it cannot achieve this, if the next ray history is different from the current ray history, if the previous ray history is the same as the current ray history, and if the receiver is within a distance of 1/2 the ray separation, a forward extrapolation is performed and IQUAL = 2. The same condition may happen on the first two rays of a set, and in this condition IQUAL = 3. If an interpolated ray is found later, the IQUAL = 3 ray will be thrown out, and the IQUAL = 1 ray used. This is indicated by \*\* after the IQUAL = 1, and the ray which is replaced is the last ray with a 3\* at the same receiver depth. The number which is listed for NRAY is the current ray number, and this forms an eigenray in conjunction with the previous ray. The NBR column gives the number of bottom reflections for this ray. The NTU column is the number of turnunders for this ray. NSR gives the number of surface reflections and NTO gives the number of turnovers. RANGE is the distance in meters from the source to this receiver. DEPTH is the ray depth for a given receiver at this range. THETA is an interpolated value for the ray arrival angle at the receiver. TIME is the travel time in seconds to this receiver from the source and is also an interpolated value between the travel times for two rays bracketing a receiver. SL(DB) is discussed in the preceding section of this report.

EIGENRAY SET				TEST CASE FOR INTENSITY							
NRAY	NBR	NTU	NSR	RANGE	DEPTH	THETA	TIME	SL(DB)	IQUAL	REM	
										*	
8	0	7	7	370000	350.0000	-10.6075	248.56510	-106.4	3		
8	0	7	7	370000	700.0000	-9.6028	248.60291	-106.5	1		
17	0	11	0	370000	350.0000	5.4116	249.38608	-99.5	2		
17	0	11	0	370000	700.0000	5.1751	249.36221	-99.5	1		
28	0	7	7	370000	350.0000	9.4668	248.56477	-107.9	1		
28	0	7	7	370000	700.0000	8.9143	248.52684	-107.9	1		
17	0	22	0	740000	700.0000	6.7384	498.73865	-103.7	2		
26	0	22	22	1110000	350.0000	4.3020	746.19729	-113.1	1		
26	0	22	22	1110000	700.0000	4.4851	746.16336	-113.1	1		

Fig. 11 — Example of an eigenray printout

## THE LLOYD'S MIRROR OPTION FOR RECEIVERS

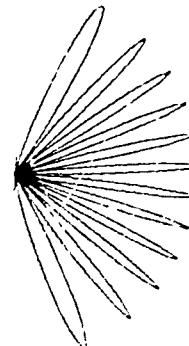
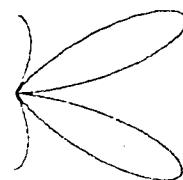
Some examples of the Lloyd's mirror beam pattern are presented in Fig. 12. The receiver depth is at the point where all the lines converge for each plot.

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FREQUENCY =

50 HERTZ RECEIVER DEPTH= 18.260 FREQUENCY =

50 HERTZ RECEIVER DEPTH= 91.440



FREQUENCY =

100 HERTZ RECEIVER DEPTH= 18.260 FREQUENCY =

100 HERTZ RECEIVER DEPTH= 91.440

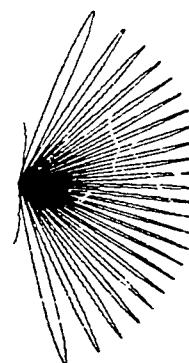
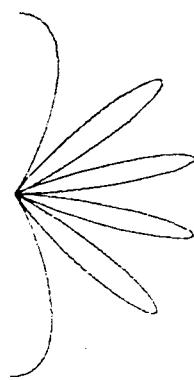


Fig. 12 — Examples of Lloyd's mirror beam patterns for receivers

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The computer coding for the Lloyd's mirror option for receivers appears within the subroutine INTENSTY. The switch LLMR, in column 26 of the output control cards, is a receiver Lloyd's mirror switch. When the switch is off (0 or blank), the old intensity is returned, and when on (nonzero), the beam pattern

$$2 \sin^2 \left( \frac{2\pi z}{\lambda} \sin \theta \right) ,$$

where  $z$  is the depth, is used for type I random phase, type I coherent phase, Type II, and Type III intensity calculations for all receiver depths. For Type I and II calculations,  $\theta$  is the ray angle, and for Type III calculations Snell's law is used to calculate the ray angle at the receiver. One can calculate some intensities with and some without the Lloyd's mirror by specifying them on different output control cards.

#### ADDITIONAL INSTRUCTIONS FOR THE RESTART OPTION

If the restart option is desired, a tape for output must be provided and a backup tape can be provided. Logical unit 15 is the primary output tape. Logical unit 16 is the back-up output tape. Logical unit 17 may be used as a second backup tape, but this is optional. If the tape on logical unit 15 was bad when the program attempted the dump and it had to write on logical unit 16 or 17, then that tape would become logical unit 15 for restart. Logical units 16 and 17 may be omitted if you are sure you have a good tape on logical unit 15. The control deck should then have these cards:

79 EQUIP, 15 = MT, LO, \*\*, DA

79 EQUIP, 16 = MT, LO, \*\*, DA (optional)

79 EQUIP, 17 = MT, LO, \*\*, DA (optional)

For dumping on tape the job request form should be as follows:

<u>Logical Unit No.</u>	<u>Input</u>	<u>Output</u>	<u>Save</u>	Tape No. (if not specified, the Computation Center sells you one and assigns a number)
15	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	Number for tape
16 (Optional)	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	Number for tape
17 (Optional)	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	Number for tape
20 (Program tape)	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>	573
1 (Used only for ray tape)	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	Number for tape

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In addition the second card in each case should contain the word DUMP in columns 73 through 76 if a restart capability is desired. If the program runs out of time, one may restart it according to the following procedure.

1. Change the job request form for logical units 15 and 1 as follows:

<u>Logical Unit No.</u>	<u>Input</u>	<u>Output</u>	<u>Save</u>	<u>Tape No.</u>
15	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	Number for tape
1	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	Number for tape

However, the output block for logical unit 15 is checked only if a dump is desired again if the program runs out of time, and the input block for logical unit 1 is checked only if the ray tape is being restarted.

2. The first card after your run card must contain RESTART in columns 1 through 7. If a dump is desired again if the program aborts because of lack of time, DUMP is entered in columns 9 through 12 of the same card. One looks through the listing and determines what cards were read last, pulls out all these cards and places the remaining cards behind the card containing the word RESTART. If the multiple replacement option is being used, the profile remaining to be read should be read in from the case in which  $LA = 1$ . For the next case all cards would have to be read in again. Also the run must have progressed at least one range increment before dump can be called. Thus, if these conditions are not met, the entire deck must be resubmitted. Also, if the last data card read was an end-of-file card, then the first data card read must be the restart card and then the end-of-file card is read. If multiple replacement is being used, one should have the restart card and then a blank card followed by a card with the word START in columns 1 through 5, followed by remaining data. This can be determined by looking at the comment which is printed at the end of the program. Reference 7 is a more complete writeup on the restart option.

## CAUTIONS TO THE USER

The following are some cautions to the user:

- If you have six receivers, then you must insert a blank card after the output control card containing the six receivers.
- The number of input and internally generated points in a sound-speed profile cannot exceed 50. The number of internally generated points can be reduced by reading in profiles with common depths.
- Do not read in the second speed-profile at a range less than the second bottom point; otherwise a diagnostic is printed and program aborts. Thus the range to your second bottom point should equal or be less than the range to the second profile.

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- The source depth and sound-speed depth for any profile should not be the same; otherwise a diagnostic is printed and the program aborts. To correct this fault, change the source depth by 0.01 meter.
- The first bottom point must be at range zero.
- The maximum number of rays which may be traced is 1000.
- If the program runs for a long time and produces no results, you have specified too large a distance between bottom points or output values and the program is forced to set up long thin triangles. In this case there is difficulty in arriving at the proper ray intersections with the triangles. To correct this condition, insert either additional bottom points or additional output at shorter range increments.

## PROGRAM TRIPLT

Program TRIPLT performs a Calcomp plot of the ray trajectories (Fig. 13). It reads an output tape from the main program and plots selected rays to a given range. Cubic splines are employed to give the proper trajectories. A maximum of 512 rays and a maximum of 2000 range increments may be plotted. A portion of the range may be plotted by specifying the number of records (one record being one range increment). A description of the input follows.

The input ray tape should be read in on logical unit 1. Thus the first equip card should be

79 EQUIP, 1 = *MT*, density, *RO*, label.

Logical unit 2 should be equipped for the disk file as 79 EQUIP, 2 = *DF*.

Logical unit 10, the plot unit, may be equipped as 79 EQUIP, 10 = *PL* or 79 EQUIP, 10 = *MT*, *LO*, label, *DA* (to write an output tape to be plotted later).

The job request form should be checked as follows:

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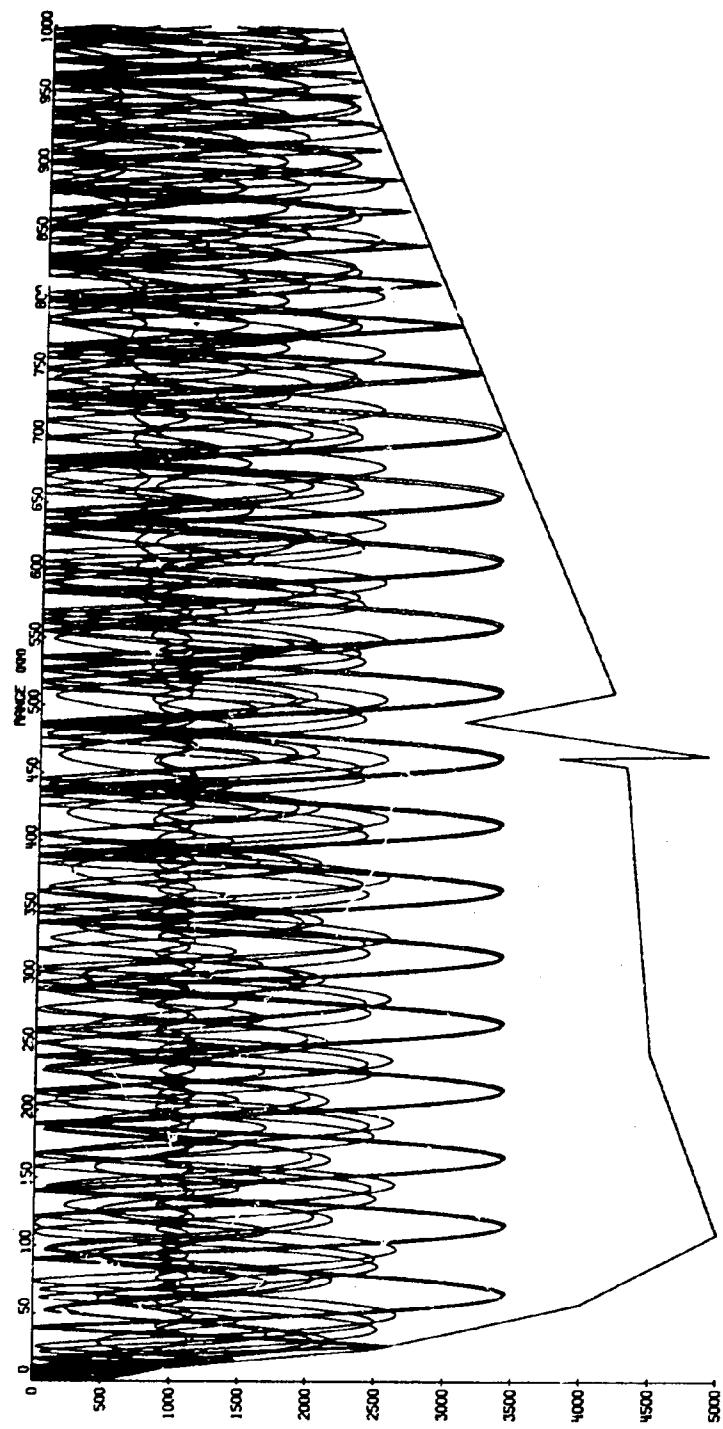


Fig. 13 — Example of a Calcomp plot.

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<u>Logical Unit No.</u>	<u>Input</u>	<u>Output</u>	<u>Sav</u>	<u>Tape Serial No.</u>
1	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>	Input Tape No.
2	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	DF
10	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	Output Tape No.

Logical unit 10 need be specified only if writing an output tape; if the plot is to be done on line, the 79 EQUIP, 10 = *PL* may be used or the card may be omitted. Computer 1 should be specified on the job request form also, because it contains the plotter package. The data deck input is as follows:

<u>First-card Columns</u>	<u>Variable</u>	<u>Meaning</u>
1-2	ITNC	Total number of cases.
<u>Second-card Columns</u>	<u>Variable</u>	<u>Meaning</u>
1-8	AL	Plot length in inches, which must be $\leq 120.0$ .
9-16	ZMAX	Maximum depth of plot, in either feet or meters.
17-20	NRMAX	Number of records to be plotted. There is one record for each range increment on the tape. Plots for a portion of the range from range ZERO may be made by specifying the number of records to that point. To plot the entire range a number may be specified which is larger than the actual number but less than 2001.
21-25	IKNM	If IKNM $< 0$ , the range scale will be plotted in nautical miles; if IKNM $\geq 0$ , the range scale will be in kilometers.
26-30	IFMC	If IFMC $< 0$ , the depth scale will be plotted in feet; if IFMC $\geq 0$ , the depth scale will be plotted in meters.

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Second-card Columns	Variable	Meaning
31-35	NFSK	Number of files to skip on the tape before plotting this case.
36-40	ITTR	If ITTR < 0, a title card is read to replace the title on the tape; if ITTR $\geq 0$ , the title from TRIMAIN will be used for the title.
41-45	NSR1	Maximum number of surface hits allowable. The ray will be terminated at this surface hit. If this is left blank, the previous limits from TRIMAIN will be used.
46-50	NBR1	Maximum number of bottom hits allowable, analogous to NSR1.
51-60	ALIM1	Maximum dB loss allowed per ray, similar to NSR1 and NBR1. It is read in as a positive floating-point number, such as 200.0.

Third-card  
Columns  
(If ITTR < 0)

1-80

## Variable

## Meaning

Title of the plot. This card is omitted if  $ITTR \geq 0$  in columns 36 through 40 of the second card; if this card is omitted, the fourth card becomes the third card.

Fourth-card  
Columns  
(or Third-card  
Columns if  
ITTR  $\geq 0$ )

1-4

## Variable

## Meaning

Number of the first ray to be plotted, which corresponds to the number of the ray in the program TRIMAIN.

5-8

## NRPLOT(1)

Number of the second ray to be plotted.

...

## NRPLOT(2)

...

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Fourth-card Columns (or Third-card Columns if ITTR > 0)	Variable	Meaning
76-80	NRPLOT(20)	Number of the 20th ray to be plotted.
...	...	
Additional-card Columns	Variable	Meaning
1-80	NRPLOT(N)	Numbers of the rays to be plotted, continued 20 per card until the desired number N is reached.

An end of file card terminates each case. The cards beginning with the second card are repeated ITNC times for multiple cases.

## REFERENCES

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2. "The Hudson Laboratories Ray Tracing Program," Technical Report 150, Hudson Laboratories of Columbia University, Dobbs Ferry, New York.
3. J.J. Cornyn, Grass: "A Digital-Computer Ray-tracing and Transmission-Loss Prediction System," Volume 1-Overall Description," NRL Report 7621, Dec. 1973.
4. H. Weinberg, "A Continuous-Gradient Curve Fitting Technique for Acoustic-Ray Analysis," J. Acoust. Soc. Am. 50, 971 (1971).
5. B.G. Roberts, Jr., "Retrieval Program for Archival Nansen-Cast Data," NRL Report 7633, 1973.
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Appendix A  
LISTING OF THE PROGRAM

.4A

07/25/73

```

PROGRAM TRIMAIN
DIMENSION JLRK(10), R1(10), DR(10), R2(10), STRCD(26,10), JNRC(10), INTTRIM
1 (10), IT(6,10), IRT(10), IRD(10), ISCPED(6), Z(2,50), V(2,50), T1(9) TRIM 1
EQUIVALENCE (ISCP,ISCPFO)
COMMON /MIRRORS/ FSRL, PRLT(200), PRST(200)
C6M484 /INFO/ RSTART, RMAX, RMega, ATT, IPRAY, ITN, ITN2, ITN3, IBIG,
1 ISCP, IT1, IT2, IT3, IPER, IFTIMS, LTRT, LTER, LTPP, LPIN, IATT TRIM 3
C6M484 /PREFIL/ REKE, N1, Z1(50), V1(50), RTK0, N2, Z2(50), V2(50), IBOTC, TRIM 4
1 IFPL TRIM 5
C6M484 /LELNESS/ LNRC, RCD(100), DIVT(400) TRIM 6
C6M484 /PREV/ IPREP, IKNM, PLTL, RV, IPCB, IFPR TRIM 7
DATA (LTRA=1), (LTER=41), (LTPR=42), (LPIN=60) TRIM 8
C6M484 /PATTER/ SD, ITAP, DATD, SORLEV TRIM 9
COMMON /PIDEF/ PI, CTPI, THPI
C6M484 /LIMITS/R1, CR, P2 TRIM 10
C6M484 /ITLE/ ITITLE(16) TRIM 11
C6M484 /ABC/PUNCHB (16), INCR, NRBS, NSRS, ALIM, IFT, IFT1 TRIM 12
C6M484 /IFCY/ IFE, IA, IB, IP, ID, IS, LA TRIM 13
C6M484 /PANST/ RTWM, IREC, IFSK, SDS TRIM 14
PI=4, *ATAN(1., SIFT=0 SIFT1=0 $ IPCG=0 STHEPI=PI+PI*SDTR=180./PI TRIM 15
1 READ 900, ITITLE ISPT=ITITLE(1) $ WRITE (19) ITITLE TRIM 16
REWIND 19 TRIM 17
IF (EGF, 60) 155, 2 TRIM 18
2 IF (ISPT.EQ.0) RESTART GO TO 104 $ GO TO 122 TRIM 19
900 FORMAT(10A8) TRIM 20
155 IF (IFE.EQ.1) GO TO 152 $ IFE=1 $ GO TO 1 TRIM 21
122 PRINT 901, ITITLE $ RSTART=0, 0 SRMAX=0.0 $ NTPLT=0 TRIM 22
901 FFORMAT(*1HORIZONTAL GRADIENT RAY TRACE .,10AM) TRIM 23
READ 902, SD, FKHZ, IATT, SORLEV, ITBP, DATD, SLDR, IABST, ISCP, NRECUR, TRIM 24
1IBOTC, IFPL, IPREP, IKNM, PLTL, NBRS, NSRS, ALIM, IA, IB, IP, ID, IS, LA, ISPT TRIM 25
AL1=ALIM $ SDS*SD TRIM 26
FSPL=0.0*(1.-SLCB) SIF(ALIM, NE, 0.0) ALIM=PWRFC(4.0, 0.0*(ALIM/0.0)) TRIM 27
902 FFORMAT(F8.3,F5.3,I1,F5.2,I1,2F5.2,7I1,F8.3,2I5,F10.3,6I1,1X,AB) TRIM 28
MEGA =2000.*PI*FKHZ SIF (ALIM, EQ, 0.0) ALIM=1.0E-30 $ S2=FKHZ**2 TRIM 29
PRINT 903, SD, SORLEV, FKHZ, ITBP, DATD, NBRS, NSRS, AL1, IA, IB, IP, ID, IS, LATRIM 30
1, ISPT TRIM 31
903 FFORMAT(*0SOURCE DEPTH=.F8.2, * LEVEL=.F6.1, * FREQ(KHZ)=.F6.3, * BEATRIM 32
1*PATTERN *12,3X,*ANGLE=.F5.1,5X,*NRRS=.15,5X,*NSRS=.15,5X,*DB TRIM 33
2*LIMIT=.F10.3,/.5X,*IA=.I1,5X,*IB=.I1,5X,*IP=.I1,5X,*ID=.I1,35X,*IS=.I1,5X,*LA=.I1,5X,*IR=.I1,5X,*IT=.I1,5X,*AT=.I1,5X,*ITBP=.I1,5X,*AB) TRIM 34
IF (NRECUR.GT.0.AND.IBOTC.GT.0) SD=SD*(1.+5.*SD/6371221.3) TRIM 35
ATT=0.0003025*S2 *44, *S2/(4100.*52) TRIM 36
IF (IATT.EQ.0) ATT=0, $ IF (NBRS,E0,0) NBRS=2500 $ IVSR=0 TRIM 37
PRINT 904, ATT, SLDR $ IF (NSRS,E0,0) NSRS=2500 TRIM 38
904 FFORMAT(*0VALUME ATTENUATION=.F10.6,* DB/KM, SURFACE LESS=.F7.2, TRIM 39
1 * DB.*)
CALL INITRAYS $ DE 985 J=1,10 SR1(J)=0.0 $ DR(J)=0.0 TRIM 40
985 R2(J)=0.0 SIF(IABST,NE,0) GO TO 15 $ RR=ISCP TRIM 41
CALL BRTRD(RB) SIF ((LA,E0,1,0R,1B,E0,1,AR,1B,E0,3) REWIND 9 TRIM 42
IF ((LA,E0,1,0R,1B,GE,2)) REWIND 8 $ GO TO 18 TRIM 43
15 PRINT 905 TRIM 44
RB=1.E30 TRIM 45
905 FFORMAT(*0BTTCM ABSORB5 ALL INCIDENT SOUND ENERGY*) TRIM 46
18 N=1 SIF ((P,EQ,0,A,D,LA,E0,0,0R,LA,EC,1) LPC=60 SIF((P,E0,1)LPC=4 TRIM 47
20 IF ((LPC,E0,60)READ(LPC,906)R1(N),DR(N),R2(N),IC,(IT(I,N),I=1,6),JVSTRIM 48
19, IRD(N),IPR, IPT(N),IPRAY,(STRCD(I,N),I=1,6) TRIM 49

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1F(LPC,EQ, 4)READ(LPC) R1(N),DR(N),R2(N),IC,(IT(1,N),I=1,6),JVSTRIM 57
3R,IRD(N),IRP, IRT(N),IPRAY,(STRCD(I,N),I=1,6) TRIM 58
1F(LA,EQ,1)WRITE( 4) R1(N),DR(N),R2(N),IC,(IT(1,N),I=1,6),JVSRTTRIM 59
1,IRD(N),IRP, IRT(N),IPRAY,(STRCD(I,N),I=1,6) TRIM 60
FORMAT(3F8.2,I2,1I1I1X,6F8.4) TRIM 61
INT(N)=0 TRIM 62
INT(N)=INT(N)+IABS(IT(1,N)) TRIM 63
IF (IT(5,N),GT,0) IPER=IT(5,N) TRIM 64
IF(INT(N),EQ,0) G6 T8 30 TRIM 65
PRINT 907,R1(N),DR(N),R2(N),(IT(1,N),I=1,6) TRIM 66
IF(DR(N).LT,0.) DR(N)=-1.*DR(N)/R1(N) TRIM 67
IH=6 TRIM 68
23 IF(STRCD(IH,N).GT,0.) G8 T8 25 TRIM 69
24 IH=[IH+1] TRIM 70
IF(STRCD(IH,N).GT,0.) G8 T8 26 TRIM 71
IF([IH,LE,1] 26,24 TRIM 72
IL=[IH+1] TRIM 73
IH=[IH+10] TRIM 74
IF(LPC,EQ,60,READ (LPC,908),(STRCD(I,N),I=IL,IH) TRIM 75
IF(LPC,EQ,4)READ (LPC) (STRCD(I,N),I=IL,IH) TRIM 76
IF(LA,EQ,1)WRITE ( 4) (STRCD(I,N),I=IL,IH) TRIM 77
C THE SWITCH ITIM IS NOW LLMR, THE LLBYDS MIRROR SWITCH FOR ALL TRIM 78
C RECEIVERS ON A GIVEN RANGE FAN CARD TRIM 79
907 FORMAT(*0OUTPUT RANGES*,3F8.2,5H ISCP,I2,4H IT1,I2,4H IT2,I2,4H ITTRIM 80
13,I2,5H IPER,I2,5H LLMR,I2) TRIM 81
908 FORMAT(10F8.2) TRIM 82
G8 T8 23 TRIM 83
26 JNRC(N)=IN TRIM 84
PRINT 909,(STRCD(I,N),I=1,[IH]) TRIM 85
IF (NRECUR,LE,0) G8 T8 29 TRIM 86
D8 31 I=1,IH TRIM 87
31 STRCD (I,N)=STRCD(I,N)*(1.+.5*STRCD(I,N)/6371221.3) TRIM 88
909 FORMAT(*0RCD*,10F9.2) TRIM 89
29 IF(JVSR.EQ,0) G8 T8 27 TRIM 90
PRINT 910,JVSR TRIM 91
910 FORMAT(*0INTENSITY VERSUS RANGE PLOT WILL BE MADE FOR TYPE*,I3) TRIM 92
IF(IVSR,NE,0) PRINT 911 TRIM 93
911 FORMAT(5H **,*,*CALTION*, ONLY THE LAST I VS R PLOT WILL BE MADE*)TRIM 94
IVSR=JVSR TRIM 95
NVSR=N TRIM 96
27 IF(IRP,EQ,0) G8 T8 28 TRIM 97
NTPLT=15 TRIM 98
ZMAX=0, TRIM 99
DRPLT=1, TRIM 100
RLPLT=1,E6 TRIM 101
PRINT 915 TRIM 102
28 IF(IRD(N),NE,0) PRINT 912 TRIM 103
IF(IRT(N),NE,0) PRINT 913 TRIM 104
915 FORMAT (*0RAY PLOT WILL BE MADE*) TRIM 105
912 FORMAT (*0RAY DEPTH DISTRIBUTION WILL BE MADE*) TRIM 106
913 FORMAT (*0RAY TAPE WILL BE MADE*) TRIM 107
30 G8 T8 40 TRIM 108
IF(IRP,EQ,0) G8 T8 33 TRIM 109
NTPLT=STRCD(1,N)*.1 TRIM 110
IF(NTPLT.LT,1) NTPLT=15 TRIM 111
                                         TRIM 112

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ZMAX=STRCD(2,N)
DRPLT=DR(N)
RLST=R2(N)
RLPLT=R2LST
PRINT 915
PRINT 914,R1(N),DR(N),R2(N)
33 IF(IRD(N)=IRT(N),EC,0) GO TO 35
PRINT 914,R1(N),DR(N),R2(N)
914 FORMAT(*0OUTPUT RAAGES*,3F10.4)
IF(IRD(N),NE.0) PRINT 912
IF(IRT(N),NE.0) PRINT 913
GO TO 40
35 N=N+1
40 IF(IC,EO.0) GO TO 45
N=N+1
IF (N,GT,10)41,20
41 PRINT 42
42 FORMAT (1H0,*NUMBER OF OUTPUT CONTROL CARDS EXCEFD 10, PROGRAM
1ABORTED*)
CALL BYEBYE
45 NR=N S IF (LA,EC,1.0P,IP,EO,1) REWIND 4
JRT=0
RMAX1=0.
D=1.0 S D1=DRPLT S DELTH=0.0 S ICA=0 SDELT=0.0
DG 47 I=1,NR
IF (DR(I),LT,D) D=DR(I) S IF (DR(I),LT,D1) D1=DR(I)
IF(R2(I),GT,RLST) RLST=R2(I)
IF(IRT(2,I),EC,0) GO TO 47
IF(R2(I),GT,RMAX1) RMAX1=R2(I)
47 JRT=JRT+IRT(I)
D=D/2.0
CALL INIT
CALL NEWPRF(ZM)
CALL NEWPRF
CALL CONNECT
IF(ZMAX,EO,0.) ZMAX=2M
RPLT=1.E6
IF(NTPLT,EO,0) GO TO 49
RPLT=DRPLT
CALL RAYPLRT(NTPLT,ZMAX)
49 IF(JRT,EO,0) GO TO 51
CALL RAYTAPE
51 NGLD=-10
J=0
NINT=1
C     IF ALL THE INTENSITY CALCULATIONS HAVE THE SAME RCDS
C     A TABULAR FORMAT WILL BE USED
D6 55 I=1,NR
IF(INT(I),EQ,0) GO TO 55
IF(J,EO,0) J=1
IF(J,EO,1) GO TO 55
IF(JNRC(I),NE,JNRC(J)) GO TO 54
K=JNRC(I)
D6 53 L=1,K
IF(ABS(STRCD(L,I)-STRCD(L,J)),GT,.1) GO TO 54
53 CONTINUE
                                         TRIM 113
                                         TRIM 114
                                         TRIM 115
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      G8 T0 55
  54  NINT=2          TRIM 169
      G8 T0 95          TRIM 170
  55  CCONTINUE       TRIM 171
  95  RMAX=0;          TRIM 172
 100  RN=1.E6          TRIM 173
      DE 103 I=1,NR      TRIM 174
      IF (R1(I).LT.RN) RN=R1(I)
 103  CCONTINUE       TRIM 175
      RSTART=RMAX        TRIM 176
      RMAX=A MIN(1,.001*RTW0,RPLT,RN)*1000.
      RT=.C01*(RMAX+1.)
      IF (PT,GT.RLST+D)   G8 T0 140
      IF (IOPT,NE,8HDUMP)  G8 T0 104
      TILT=PTILT
      TILT=TIMELEFT(1)
      DELT=TILT-P-TILT
      IF (DELT.LT.0.0) G8 T0 108
      ICA=ICA+1
      FICA=ICA
      DELTA=DELTA+DELT
      DELTM=DELTA/FICA
 108  RER=(RLST-(RSTART/1000.0))/D1
      TGTIME=RER*DELM=2.0
      TGTIMM=TGTIME/60.0
      IF (TILT.LE.90.0+DELM) AND (TGTIMM.GE.30.0+DELM) 107;104
 107  IF (JRT.NE.0) BACKSPACE 1  $ CALL DUMP
      PRINT 105,TILT,TGTIMM
 105  FFORMAT(1H0,•PROGRAM ABRTED, INSUFFICIENT RUN TIME, TIME REMAININ•TRIM 197
      1G=•,F10.3,• SECONDS•,5X,•ESTIMATED TIME TO FINISH RUN•,F10.3,    TRIM 198
      2• MINUTES•)
      PRINT 101,RTW0M
 101  FFORMAT (1H0,•REMOVE DATA DECK THROUGH PROFILE AT RANGE•,F10.3,• KHM•TRIM 200
      1 BEFORE RESTARTING CASE•,/)
      IF (IFE,EQ,1) PRINT 106
      IF (IS,EQ,1,AND,IFE,FQ,0) PRINT 112
 112  FFORMAT (1H0,•INSERT BLANK CARD AFTER RESTART CARD, FOLLOWED BY A CTRIM 205
      1ARD WITH WRD START IN COLUMNS 1-8, FOLLOWED BY REMAINING DATA•,/) TRIM 206
 106  FFORMAT (1H0,•INSERT END OF FILE CARD AFTER RESTART CARD BEFORE RESTRI•TRIM 207
      1TING CASE•,/)
      IF (IFE,EQ,1) G8 T0 111
 109  READ 900,JUNK
      IF (EOF,6C)111;109
 111  CALL BYEBYE
 104  IF (IOPT,NE,BHRESTART) G8 T0 102
      IF (IOPT,EQ,BHRESTART) CALL RESTART $ CALL CLOSEIOP
      PRINT 90,ITITLE $ DB 113 J=1,10
 113  JUNK(,)=ITITLE(J) $ READ (19) ITITLE
      REWIND 19
      IF (ITITLE(1).EQ.BHRESTART ,AND,IS,EQ,1,AND,IFE,EQ,0) CALL RETRY
      IOPT1=ITITLE(2)
      IF (IOPT1,EQ,8H      ) IOPT=IOPT1 $ DB 114 J=1,10
 114  ITITLE(J)=JUNK(J) $ IF (JRT,EQ,0) G8 T0 102 $ DB 121 J=1,IFSK
 121  CALL SKIPFILE (1)   $ DB 123 J=1,IREC
 123  READ (1)
 102  CALL ADVANCE S IF(RMAX>1.LT,RTW0) G8 T0 110      $ CALL NEWPROF TRIM 224

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110 CALL CONNECT
110 IF(RT,LT,RPLT) GO TO 115      S CALL RAYPLOT
RPLT=RPLT+DRPLT
115 IF(RPLT.GT.RPLT*.1) RPLT=1,E6
IF(RT,LT,AN) GO TO 135
GO 130 I=1,NR
IF(R1(I),GT,RT) GO TO 130
IF(INT(I),EQ,0) GO TO 125
IF(I.EQ.NBLD) GO TO 120
LNRC=JNRC(I)
GO 117 J=1,LNRC
117 RCD(J)=STRCD(J,I)
GO 119 J=1,6
119 ISCOPEQ(J)=IT(J,I)
120 CALL INTENSTY
CALL ITNPRT(NINT)
IF(I.EQ.NYSR) CALL IVSPPLT(IVSR)
NGLD=1
125 IF(IRD(I),NE,0) CALL RAYZDIST (NTPLT)
IF(IRT(I),NE,0) CALL RAYTAPE
IF(DR(I).LT,0.) GO TO 126
R1(I)*R1(I)+DR(I)
GO TO 127
126 R1(I)=R1(I)+DR(I)
127 IF(R1(I).GT,R2(I)*.001) R1(I)=1,E6
130 CGNTINUE
135 IF(RT,GT,RB) CALL RWBRLT(RB)
GO TO 100
140 IF(JRT.EQ,0) GO TO 150
ENDFILE LTRT
ENDFILE LTRT
BACKSPACE LTRT
150 IF (INCR.GT,1.AND.INCR.LE,16) 151,153
151 INCRCPINCR-1
WRITE (36,910) (PLANCHDR(I),I=1,INCR)
910 FFORMAT (16F5.1)
153 IF (IFE.EQ,1) GO TO 158
IF (LA.EQ,1,OR.IS.EQ,1) GO TO 160
157 READ 900,JUNK
IF (EOF,60) 158,157
160 IF (LA.EQ,1,OR.IS.EQ,0:AND.LA,EQ,0) LPM=60
IF (IS.EQ,1) LPM=6
176 IF(LPM.EQ,60)READ (LPM,1903) NCUR,RB,TI
IF(LPM.EQ, 6)READ (LPM)      NCUR,RB,TI
IF(EOF,LPM ) 177,178
177 IF (LA.EQ,1) ENDFILE 6
REWIND 6
GO TO 158
178 IL=1 S IF (LA.EQ,1) WRITE (6)      NCUR,RB,TI
179 IH=IL+4
IF(LPM,EC,60)READ(LPM,1900)(Z(2,I),V(2,I),I=IL,IH)
IF(LPM,EO, 6)READ(LPM)      (Z(2,I),V(2,I),I=IL,IH)
IF(LA,EQ,1)WRITE ( 6)      (Z (2,I),V (2,I),I=IL,IH)
IF(V (2,IH).LE,0.) GO TO 176
IL=IL+5
GO TO 179

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TRIM 225  
TRIM 226  
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TRIM 280

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1503 FORMAT(1I1,F7.3,9A8)
1507 FORMAT(10F8.4)
158 IFPR1=IFPR $ IF (IFPR1,NE,1) IFPR=1 $ IF (IPFL,EO,0) GO TO 159
    IF (IFPR1,EO,0,AND,IPFL,EO,1) CALL PR0FPL0T (2,0,5,1)
    IF (IPFL,EO,2,AND,IFPR1,EO,0) CALL PR0FPL1T (2,0,5,1)
159 IFC=1 $ IFT1=IFT1+1 $ IF (IS,EO,0) GO TO 1
161 READ 900,JUNK $ IF (EAF,60) 1,161
152 IF (IPC0,NE,0) CALL STRPPLAT
    CALL BYEBYE
    END
```

TRIM 281  
TRIM 282  
TRIM 283  
TRIM 284  
TRIM 285  
TRIM 286  
TRIM 287  
TRIM 288  
TRIM 289  
TRIM 290

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5.4DS TRIMAIN

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ED

PROGRAM LENGTH	IDENT	TRIMAIN
ENTRY POINTS	04624	
BLOCK NAMES	01572	
MIRRORS	00621	
INFO	00024	
PREFIL	00316	
LOUDNESS	00765	
PRE	00006	
PATTERN	00004	
PIDEF	00003	
LIMITS	00036	
TLE	00012	
ABC	00026	
IFC	00037	
RANST	00004	

## EXTERNAL SYMBOLS

C8CENTRY  
 THEND,  
 C2C07111  
 C1C10100  
 C8CDICT,  
 INITRAYS  
 BRLTRD  
 RYEBYE  
 INIT  
 NEAPRF  
 CONNECT  
 RAYPLOT  
 RAYTAPE  
 TI-LEFT  
 DUMP  
 RESTARY  
 CLOSEIOP  
 RETRY  
 SKIPFILE  
 ADVANCE  
 INTENSTY  
 ITNPRINT  
 INSRPLT  
 RAYZDIST  
 NBRLT  
 PRSPLOT  
 PREPPLIT  
 STAPPLOT  
 PSURE  
 MINIF  
 ATANF  
 CBCIFEGF  
 EFT.  
 BSP.  
 RE-.  
 TS-.  
 TSB.  
 STH.  
 STB.

SLE.  
 SLI.  
 CNSINGL,

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CLOSEIOP				IDENT	CLOSEIOP	07/12/73	ED 00000	PAGE NO.	1
PROGRAM LENGTH		00012						C1OP	1
ENTRY POINTS	CLOSEIOP	00004							
EXTERNAL SYMBOLS			IOP.						
				ENTRY	CLOSEIOP				
				EXT	IOP.				
				BSS	2				
				ENI	**+1				
				OLDA	SAVEAO				
				CLOSEIOP	OCT	0			
				DSTA	(*)SAVEAO				
								C1OP	2
								C1OP	3
								C1OP	4
								C1OP	5
								C1OP	6
								C1OP	7
								C1OP	8
								C1OP	9
								C1OP	10
								C1OP	11
								C1OP	12
								C1OP	13
								C1OP	14
								C1OP	15
								C1OP	16

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SLH4ELT15 RETRY
DIMENSION TITLE (V),2IL(2,50),VIL(2,50)
15 LEAD 1,1C
  1 FGHAT (48)
    IF (EEF,HD) 15,14
  14 IF ([L,EN,FINSTANT] 1 RD TE 75
    GE TE 15
    75 LPA=60
  76 IF (LPA,EN,60)HEAD (LEN +903) ACLR,PU,TITLE
    IF (EEF,LPA) 77,78
  77 ENDFILE A
    RE-IND 9
    GE TE 92
  78 IL=1   *FITE (6)      NCUR,R0,TITLE
  79 IF =IL+4
    IF (LPA,EN,60)HEAD (LEN +903) (ZIL(2,1),VIL(2,1),I=IL,[H])
    WHITE ( 6)          (ZIL(2,1),VIL(2,1),I=IL,[H])
    IF (VIL(2,1H),LE,0,) CE TE 76
    IL=IL+5
    GE TE 78
  900 FGHAT(12FA,4)
  903 FGHAT (11,F7,3,948)
  62 RETL44
  END

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	RETY
1	RETY
2	RETY
3	RETY
4	RETY
5	RETY
6	RETY
7	RETY
8	RETY
9	RETY
10	RETY
11	RETY
12	RETY
13	RETY
14	RETY
15	RETY
16	RETY
17	RETY
18	RETY
19	RETY
20	RETY
21	RETY
22	RETY
23	RETY
24	RETY

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DS RETRY

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EC

0

PROGRAM LENGTH	IDENT	ENTRY
ENTRY POINTS	00546	RETRY
EXTERNAL SYMBOLS	00340	

THEND,  
DSDICT,  
DSCIFER  
EFT,  
REN,  
TSH,  
STR,  
SLC,  
ONSINGL,

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144
SUBROUTINE INITRAY
DIMENSION VBP(91)
C6446A /PATTERN/ SC,ITFP,DATE,SEPLEV
C6446A /PDEF/ PI,CTR,TREP1
C6446A /RAYS/ ARAY,TGAM(1000),ZZ(1000),SS(1000),TIME(1000),
1 NCTR(1000),PHASE(1000)
C6446A /IFC/ IFE,IA,IB,IP,IC,IS,LA
ARAY=0
EG=1000
PRINT 905
905 FORMAT (*, GAMLD GAMDC OGAMD IC SL PHASE *)
IF ((IA,EQ,0,AND,LA,EC,C,GR,LA,EG,1,OR,IA,EO,2)) LPC=60
IF ((IA,EQ,1,SH,IA,EG,3)) LPC=2
10 IF(LPC,EG,6) READ(LFC,900)GAMLD,GAMDC,OGAMD,IC,SL,PH
IF(LPC,EG,2) WRITE(LFC) GAMLD,GAMDC,OGAMD,IC,SL,PH
IF((LA,EG,1)=R1TE(2)) GAMLD,GAMDC,OGAMD,IC,SL,PH
PRINT 906,GAMLD,GAMDC,OGAMD,IC,SL,PH
906 FORMAT (1H0, 3F10.4, 1E, 2F7.2)
SL=10,*(1*(SL+SEPLEV))
IFF=1
IF(ARS(EG+GAMDC),LT,,0C1) GE TE 20
IF(NRAY,EG,0) GE TE 15
ARAY=NRAY+1
SS(NRAY)=0,
15 EG=EGAMD-GAMDC
SEG$|=N(EG/DTR)
IFF=0
20 S=90+EGAMD
S=SIN(G/DTR)
ARAY=NRAY+1
IF(NRAY,GT,1000) GE TE 100
TGAM(NRAY)=S/SCRT(1,-S*S)
ZZ(NRAY)=SD
TIME(NRAY)=C,
NCTR(NRAY)=C
PHASE(NRAY)=PH/DTH
SS(NRAY)=SL*,5*ABS(S-SEG)
IFF(NE,0) SS(NRAY+1)=SS(NRAY+1)+SL*,5*ABS(S-SEG)
IFF=1
EG=G
SEG=S
IF ((G + ,0000001),LT, GAMLD ) GE TE 20
IF((C,NE,0)) GE TE 10
23 IF((ITRP,IEQ,0)) GE TE 35
IL=1
25 IH=IL+1Y
IF ((IA,EQ,0,AND,LA,EC,C,GR,LA,EG,1,OR,IA,EO,1)) LP =60
IF ((IA,GE,2)) LP=7
IF(LP,EG,60) READ(LF ,901)(VBP(),I=IL,IH)
IF(LP,EG,7) READ(LF ) (VBP(),I=IL,IH)
IF((LA,EG,1)=R1TE(7)) (VBP(),I=IL,IH)
PRINT 907,(VBP(),I=IL,IH)
907 FORMAT(*,0VBP *,20F5,1)
IF(VBP(IH),EC,0,) GE TE 27
IL=IL+2U
GE TE 25
INIT 1
INIT 2
INIT 3
INIT 4
INIT 5
INIT 6
INIT 7
INIT 8
INIT 9
INIT 10
INIT 11
INIT 12
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INIT 56

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14A
27 IF(IH,EJ,1) GE TS 28      INIT 57
IF(VBR(IH),E3,0,) GE TS 27      INIT 58
28 GE 29 INIT,90      INIT 59
29 VBPI(+1)=VBPH(IH)      INIT 60
GE 31 I=1,NRAY      INIT 61
CHABS(DIR=ATAN(TGAM(I))+CATD)      INIT 62
I=0      INIT 63
C=0.0      INIT 64
C=(1.+0)*VBR(N+1)+C*VBR(N+2)      INIT 65
SS(I)=SS(I)+10.0*(+1,E+1*D)      INIT 66
PRINT 902      INIT 67
PRINT 903,(I,TGAM(I),SS(I),PHASE(I),I#1,NRAY)      INIT 68
IF (LA,EQ,1,ER,IA,EG,1,ER,IA,EG,3) REWIND 2      INIT 69
IF (LA,EQ,1,ER,IA,EG,2) REWIND 7      INIT 70
RETURN      INIT 71
100 IF(IC,EJ,0) GE TS 23      INIT 72
READ 904,IC      INIT 73
GE TS 100      INIT 74
900 FORMAT(3F10.4, 1D, 2F5.2)      INIT 75
901 FORMAT(2DF4.1)      INIT 76
902 FORMAT(*0 INITIAL TAN GAMMA, SIGNAL LEVEL, AND PHASE//)      INIT 77
903 FORMAT( 2(I10, 3F15.5 ))      INIT 78
904 FORMAT(1BX,12)      INIT 79
END      INIT 80
INIT 81

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## 5 INITRAYS

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ED 0

	ICCAT	INITRAYS
PROGRAM LENGTH	01026	
ENTRY POINTS	00220	
BLOCK NAMES		
PATTERN	00004	
PICEF	00003	
PAYS	13561	
IFC	00007	
EXTERNAL SYMBOLS		
THEAD,		
02007111		
01010100		
01003100		
GSELECT,		
SQRTF		
SINF		
ATANF		
HEX,		
TSW,		
TSF,		
STH,		
STR,		
ONSINGL,		

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SUBROUTINE BLTRO(66) $ COMMENT /PIPEDEF/ PI,DTR,T40P!
COMMENT /INFO/ IDUM(2),EMEG4,ICMP(17)
COMMENT /M1NRHS/ KERL,EMLT(200),EPST(200)
DIMENSION DB(50),LG(50),CTSTR(600),BR(91,4),BP(91,4),ISW(4),
1  RL(50),ICL(50),UTH(600)
COMMENT /TC/ IFE,IAT,IP,IC,IS,LA
EGUI[VALENCE (LR,DTSTR(551)),(LG,CTSTR(501)),(ICL,DTSTR(451)),
1  (RL,DTSTR(401)),(IS,DTSTR(397)),(BR,DTSTR),(ISCP,DTSTR(396)),BLRD 1
2  (IE,DTSTR(395)),(IR,DTSTR(394)),(K,DTSTR(393)),BLRD 2
3  (IL,DTSTR(392)),(IM,DTSTR(391)),(IC,DTSTR(390)),BLRD 3
EQUIVALENCE (R,DTSTR(389)),(T,DTSTR(388)),(F,DTSTR(387)),(PH),
1  DTSTR(386)),(UE,DTSTR(385)),(R,DTSTR(384)),BLRD 4
2  (RN,DTSTR(383)) $ ECLIVALENCE (RH,DTSTR(193))
DATA ((DTSTR(1,1,501,600))=BLRD 5
1  19., 35., 40., 52., 6(90.),BLRD 6
2  19., 25., 35., 45., 55., 5(90.),BLRD 7
3  11., 20., 25., 35., 45., 56., 4(90.),BLRD 8
4  11., 20., 30., 40., 55., 5(90.),BLRD 9
5  5., 7.5, 16.5, 17.5, 19., 20., 21., 22.5, 2(90.),BLRD 10
1  0., 3.7, 4.5, 7(6.),BLRD 11
2  0., 2.3, 4.6, 6.5, 6(8.),BLRD 12
3  0., 3., 4.4, 6.7, 8.3, 5(10.),BLRD 13
4  2., 5.2, 7.7, 9.8, 6(12.),BLRD 14
5  4., 5.2, 12., 12.5, 13.4, 13.7, 13.9, 3(14.) ,BLRD 15
DATA ((DTSTR(1,1,401,500))=BLRD 16
1  16., 30., 40., 50., 55., 5(90.),BLRD 17
2  17., 20., 30., 40., 50., 55., 4(90.),BLRD 18
3  13., 20., 35., 45., 52.5, 5(90.),BLRD 19
4  7.5, 11., 20., 25., 30., 34., 4(90.),BLRD 20
5  2.5, 5., 7.5, 15., 17.5, 20., 22., 3(90.),BLRD 21
1  0., 2.6, 4.4, 5.4, 6(6.),BLRD 22
2  0., 1.3, 4.6, 7., 8.5, 5(9.),BLRD 23
3  3., 5.3, 8.7, 10.3, 6(11.),BLRD 24
4  3., 4., 10.4, 12.7, 13.7, 5(14.),BLRD 25
5  6., 8.7, 10., 14.1, 15., 15.8, 4(16.) ,BLRD 26
DATA ((DTSTR(1,1,301,400))=BLRD 27
1  19., 25., 35., 45., 51., 5(90.),BLRD 28
2  18., 25., 35., 45., 55., 5(90.),BLRD 29
3  14., 20., 30., 40., 50., 53., 4(90.),BLRD 30
4  8., 11., 20., 22.5, 26., 5(90.),BLRD 31
5  2.5, 4.5, 7.5, 10., 14.5, 17.5, 20., 23., 2(90.),BLRD 32
1  0., 1.5, 3.2, 5.1, 6(6.),BLRD 33
2  0., 2.8, 5.5, 7.6, 4(9.),BLRD 34
3  3., 5., 7.5, 9.4, 10.8, 5(11.),BLRD 35
4  5., 6.2, 12.2, 13.2, 5(14.),BLRD 36
5  9., 10., 12., 13.9, 16., 17.1, 17.7, 3(18.) ,BLRD 37
DATA ((DTSTR(1,1,201,300))=BLRD 38
1  16., 23., 30., 40., 50., 55., 4(90.),BLRD 39
2  17., 20., 25., 30., 35., 45., 55., 3(90.),BLRD 40
3  13., 25., 30., 35., 42.5, 45., 50., 3(90.),BLRD 41
4  9., 12.5, 20., 22.5, 27., 5(90.),BLRD 42
5  2.5, 4.5, 7.5, 10., 14.5, 17.5, 20., 23., 2(90.),BLRD 43
1  3., 2., 4., 6., 7.4, 5(8.),BLRD 44
2  3., 1.7, 3.3, 5.6, 6.8, 8.8, 4(10.),BLRD 45
3  3., 6.6, 8., 9.1, 10.4, 10.7, 4(11.),BLRD 46

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4    7.,   8.,   12.,  13.,  13(14.),  

5    9.,   10.,  12.,  13.,  16.,  17.,  17.,  3(18.)      )     BLRD  97  

  DATA ((DTSTR(I),I=101,200))  

1  2.,  10.,  12.,  15.,  20.,  25.,  30.,  35.,  40.,  90.,  

2  2.,  15.,  7.,  12.,  20.,  25.,  32.,  37.,  42.,  2(90.),  

3  2.,  5.,  7.,  12.,  17.,  22.,  27.,  32.,  2(90.),  

4  2.,  5.,  7.,  10.,  11.,  13.,  15.,  20.,  24.,  2(90.),  

5  2.,  5.,  5.,  8.,  10.,  12.,  15.,  20.,  22.,  27.,  90.,  

1  3.,  5.,  5.,  6.,  6.,  7.,  8.,  9.,  9.,  2(10.),  

2  4.,  6.,  9.,  11.,  11.,  13.,  13.,  13(13.5),  

3  7.,  9.,  11.,  11.,  14.,  14.,  15.,  15.,  15(15.5),  

4  9.,  13.,  13.,  15.,  15.,  16.,  16.,  17.,  17.,  3(17.5),  

5  11., 13., 13., 16., 17., 18., 18., 19., 19., 2(20.)      )     BLRD  69  

  DATA ((UTSTR(I),I=1,100))  

1  7.,  11.,  13.,  15.,  17.,  20.,  25.,  27.,  2(90.),  

2  7.,  10.,  11.,  14.,  15.,  17.,  20.,  25.,  29.,  90.,  

3  7.,  12.,  15.,  18.,  20.,  22.,  25.,  27.,  90.,  90.,  

4  7.,  10.,  14.,  17.,  20.,  22.,  25.,  28.,  90.,  90.,  

5  2.,  5.,  5.,  8.,  10.,  15.,  17.,  20.,  23.,  90.,  90.,  

1  6.,  5.,  6.,  9.,  8., 10., 11., 11., 12., 3(13.),  

2  7.,  8.,  10., 10., 10., 11., 11., 11., 12., 2(14.),  

3  8.,  11., 12., 14., 14., 14., 15., 15., 15., 3(16.),  

4  9.,  11., 13., 14., 14., 15., 16., 16., 16., 3(17.),  

5  10., 13., 15., 16., 17., 18., 18., 18., 18., 3(19.)      )     BLRD  79  

IF (IFT1.EQ.1) GO TO 2  

DE 1 J=1,600  

1 DTH(J)=UTSTR(J)  

IFT<1  

GE TO 3  

2 DE 4 J=1,600  

4 DTSTR(J)=UTH(J)  S IE=0  

3 FR=EMEGA/TWBPI  S IF(FR.LT.100,) GO TO 25  

IF (FR.GT.1500,) GO TO 10  S IF(FR.LT.750,) GO TO 5  S IC=301  

GE TO 20  

5 IC=401  S GO TO 20  

10 IF (FR.LT.1.2750,) GO TO 15  S IC=101  S IF(FR.GT.6000,) IO=1  

GE TO 20  

15 IC=201  

20 DE 24 I=5(1,400  S DTSTR(I)=DTSTR(IO)  

24 IC=IC+1  

25 DE 30 I=1,500  

30 DTSTR(I)=0,  S ISCP=RE  

IF (Iw.E0,0,44C,LA,EG,C,ER,LA,EG,1,8R,1J,ED,2) LPB=60  

IF (Iw.E0,1,ER,1J,ED,3) LPB=9  

40 IB=IB+1  S IF(LPB,EG,60)READ (LPB,900)RBL(IB),ICL(IB)  

IF (LPB,EG,9)READ (LPB) RBL(IB),ICL(IB)  

IF (LA,ED,1)WRITE (9) RBL(IB),ICL(IB)  S IF(RBL(IB)) 41,41,42 BLRD 100  

RBL(IB)=1,EG0  

41 IF(ICL(IB)) 43,43,44  

42 IF(ICL(IB)) 43,43,44  

43 ICL(IB)=0  S GE TO 60  

44 IF(ICL(IB)=9) 46,46,45  

45 ICL(1B)=ICL(1B)/10  

46 IF(ICL(1B)=5) 60,60,47  

47 K=ICL(1B)+5  S IF(K>(K)) 48,48,60  

48 ISW(K)=1  S IL=1  

49 IF(IL>1)  S IF(LPB,EG,60)READ (LPB,901)(BR(I,K)),I=IL,1H)     BLRD 112

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IF (LPP,EO,0)READ (LFB)(BR ((I,K),I=IL,IH)
IF (LA,EO,1)=RITE ( 9) (BR((I,K),I=IL,IH)) S IL=IL+20      ALRD 113
IF(BR((I,M,K))) 51,51,46      ALRD 114
IF(BR((I,M,K))) 51,51,53      ALRD 115
IH=IH+1 S IF((IH)>2152,50      ALRD 116
IH=1      ALRD 117
D6 54 I=IH,90      ALRD 118
BR((I+1,K)=BR((I,M,K)) S IL=1 S IF((ISCP) 60,60,55      ALRD 119
IH=IL+1Y S IF ((IJ,EC,C,AND,LA,EG,C,OR,LA,EO,1,OR,IJ,EO,1) LPP=60      ALRD 120
IF((IJ,GE,2)LPP=8 S IF(LPP,EC,60)READ (LPP,901) (BP((I,K)),I=IL,IH)ALRD 121
IF (LPP,EO,0) READ (LPP) (BP((I,K)),I=IL,IH)      ALRD 122
IF (LA,EO,1) WRITE(8) (BP((I,K)),I=IL,IH)      ALRD 123
IF(BP((I,M,K))) 55,60,55      ALRD 124
IF(RBL(1B),LT,1,E15) GE T0 40 S D0 65 K=6,9      ALRD 125
IF((S=(K=5)) 65,65,61      ALRD 126
PRINT 902,K=5 PRINT 903,(I,BR(I+1,K=5),BP(I+1,K=5),I=(E,90)      ALRD 127
C6NTINUE S PRINT 900 S D0 70 I=2,1B S RN=RBL(I=1)      ALRD 128
PRINT 904,R,RN,ICL(I+1)      ALRD 129
R=RN S PRINT 905,R,ICL(IH) S IE#1      ALRD 130
IC=ICL(IE) S IF(IC) 76,76,80      ALRD 131
D6 77 I=1,200 S BHLT(I)=1,      ALRD 132
BPST(I)=0, S GE T0 100      ALRD 133
D6 99 I=1,200 S TSETR=ATANT,01*(I-1) S K=IC-5 S IF(K) 61,81,93      ALRD 134
IL=10*IC S IF(DG(IL=9),GE,T) G0 T0 93      ALRD 135
IF(DG(IL=8),GE,T) GG T0 92 S IL=IL+1 S G0 T0 82      ALRD 136
DCB=CH(IL=9)*(T-DG(IL=9))*(DB(IL=8)-DB(IL=9))/(DG(IL=8)-DG(IL=9))      ALRD 137
GE T0 94      ALRD 138
DCB=CH(IL=9)      ALRD 139
PHI=0, S GO T0 9M      ALRD 140
NET S F=TE,N S DCHE=ER(N+1,K)+F*(BR(N+2,K)-BR(N+1,K)) S PHI=0,      ALRD 141
IF((ISCP,NE,0) PHI=EP(N+1,K)+F*(BP(N+2,K)-BP(N+1,K))      ALRD 142
BPST(I)=PHI      ALRD 143
BRLT(I)=10,00*(-,1*ICE)      ALRD 144
RR=RBL(IE) S RETURN S ENTRY NWRLT S IE=IE+1      ALRD 145
IF(IC=ILL(IE)) 75,100,75      ALRD 146
900 FORMAT(F8.4,12)      ALRD 147
901 FORMAT(20F4.2)      ALRD 148
902 FORMAT(3SHUSER SUPPLIED BETTER LOSS TABLE CLASS ,15/1X      ALRD 149
1 3(2HG,A,6X,2HCB,/X,3FHFI,10X))
903 FORMAT(3(|3,F10.3,F6.3,9X))
904 FORMAT(5H FHFM,F10.2,3L T0,F10.2,16H XM RGTION CLASS,15)
905 FORMAT(5H FHFP,F10.2,3L T0,3X,23HEND OF RUN BETTER CLASS,15)
END      ALRD 154
                                         ALRD 155

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BALTRD

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ED 0

	ICCAT	BALTRD
PROGRAM LENGTH	03503	
ENTRY POINTS	02361	BALTRD
	02371	
BLOCK NAMES		
PIPER	00003	
INFL	CFC24	
MIRRORS	00021	
ABC	00026	
IFC	00007	
EXTERNAL SYMBOLS		
01010100		
THEME,		
01003100		
02007111		
ROCLIST,		
ATANF		
TSR,		
TSR,		
STH,		
STB,		
0NSINGL,		

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SUBROUTINE WORD SIZE
CEMMEN /RAYS/  NRAY,TCAM(1000),ZZ(1000),SS(1000),TIME(1000),
1  NCOUNT(1000),PHASE(1000)          WORD  1
CEMMEN /INFO/  RSTART,RMAX,EDEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,
1  ISCP,ITS,IT2,IT3,IPER,IFTIMS,LTHT,LTER,LTRP,LPIN,IATT      WORD  2
CEMMEN /TRIANG/ AP(100,2),BP(100,2),AL(100),BL(100),ZZERO(100),
1  RZERS(100),AA(100),BB(100),SST(100),CCT(100),NTRI        WORD  3
CEMMEN /TLE/ ST;TLE (1C)           WORD  4
CEMMEN /ABC/PLANCHDR (16),INCR,NBRS,NSRS,ALIM,IFT,IFT1      WORD  5
CEMMEN /TRANST/ RDLF,IREC,IFSK,SCLM      WORD  6
DATA (JBIG=3777777777777777), (IENT=0) , (IFSK=-1)
ENTRY JN1
IF (IFT1,EQ,0) G3 T6 2
JBIG=3777777777777777    S IENT=0
2 ITN=SCR((SORT(JBIG/4,)))
ITN2=ITN+02
ITN3=ITN2+ITN
IBIG=ITN3+ITN
RETURN
ENTRY RAY TAPE
ZB=AL(NIR)+BL(NTR)+RMAX
IF (IENT,NE,0) G8 T6 1
WRITE (LTAT)TITLE,ALIM,NBRS,NSRS,ITN
IEN1=1  S IREC=1  S IFSK=IFSK+1
1 WRITE (LTHT) NRAY,FMAX,ZB,(TGAM(I),I=1,NRAY),(ZZ(I),I=1,NRAY),
1  (SS(I),I=1,NRAY),(NCOUNT(I),I=1,NRAY),(TIME(I),I=1,NRAY),
2  (PHASE(I),I=1,NRAY)    S IREC=IREC+1
RETURN
END

```

WORD 7  
WORD 8  
WORD 9  
WORD 10  
WORD 11  
WORD 12  
WORD 13  
WORD 14  
WORD 15  
WORD 16  
WORD 17  
WORD 18  
WORD 19  
WORD 20  
WORD 21  
WORD 22  
WORD 23  
WORD 24  
WORD 25  
WORD 26  
WORD 27  
WORD 28  
WORD 29

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S WORDSIZE		07/02/73	ED	0
PROGRAM LENGTH		IDENT	WORDSIZE	
ENTRY POINTS	INIT	00217		
	RAYTAPE	00012		
	WORDSIZE	00044		
BLOCK NAMES	WORDSIZE	00005		
	RAYS	13561		
	INFO	00024		
	TRIANG	02261		
	TLE	00012		
	ABC	00026		
	RANST	00004		
EXTERNAL SYMBOLS				
	01C10100			
	THEND,			
	QBCDICT,			
	SJRTF			
	STB,			
	SLE,			
	ONSINGL,			

**UNCLASSIFIED**

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SUBROUTINE NEWPROF(ZMAX)
COMMON /INFB/ RSTART,RMAX,8MEGA,ATT,!PRAY,ITN,ITL2,ITN3,IBIG,
1   !SCP,ITL,IT2,IT3,!PER,!PTIMS,LTRT,LTER,LTRP,LPIN,!ATT
COMMON /PRBFIL/ R1,N1,Z1(50),V1(50),R2,N2,Z2(50),V2(50),IBOTC,IPFLNEWP
COMMON /INPUT/ RBOT(250),ZBOT(250),ZIL(2,50),VIL(2,50),NN(2),ICAN2NEWP
1,50)                                             NEWP 5
COMMON /TLE/STITLE (10)                           NEWP 6
COMMON /PRB/ !PRBF,[KNM,PLTL,RH,!PCB,!FPR
DIMENSION TITLE(9),PM(3),LIN (114)               NEWP 7
COMMON/ABC/PUNCHDB (16) !INCR,NBRS,NSRS,ALIM,IFT,IFT1
COMMON /IFC/ IFE,IA,IB,IK,ID,IS,LA               NEWP 8
COMMON /RANST/ RS,!DUM,!DUMM,SDS                NEWP 9
DATA (NBPT=0),(IEFF=0),!(LIN=114(1W)),(IFT2=0),(IRH=0)    NEWP 10
1 IF=IEFF S IF (IFT1,EO,IFT2) GA TO 952          S1BH=0 $IFT2=IFT1
552 IF (IFT1,EO,0,0,IRH,EO,1) GO TO 950          S NBPT=0 SIEFF=0 SIEF=IEFF
18H=1 $ A2=0 $ R2=0.0 $ N1=0 $ R1=0.0 $ IPF=0
951 GO 951 Ja1,114                               NEWP 14
551 LIN(J)=1W                                     NEWP 15
950 IF(NBPT,GT,0) GO TO 20                         NEWP 16
C      FIRST ENTRY, READ IN BOTBHM TRACK           NEWP 17
1 IL=1 $ IF (ID,EO,0,AND.LA,EO,0,OR.LA,EO,1) LP1=605!F([D,EO,1])LP1=5$NEWP 18
2 IH=IL+4                                         NEWP 19
3 IF(LP1,EO,60)READ (LP1,900) (RBOT()),ZBOT(),I=IL,[W]     NEWP 20
4 IF(LP1,EO,5)READ (LP1) (RBOT()),ZBOT(),I=IL,[W]     NEWP 21
5 IF(LA,EO,1)WRITE (5) (RBOT()),ZBOT(),I=IL,[W]     NEWP 22
6 IF(RBOT(IH),LE,0,) GO TO 3 $ IL=IL+5 $ GO TO 2     NEWP 23
7 IH=IH+1 $ IF(RBOT(IH),LE,0,) GO TO 3             NEWP 24
8 IF (LA,EO,1,OR.ID,EO,1) REWIND 5                 NEWP 25
9 PRINT 901,(RBOT(),ZBOT(),I=1,NBPT) $ IF (IBOTC,LE,0) GO TO 1
10 DO 5 I=1,NBPT                                    NEWP 26
5 ZBOT()=ZBOT()*(1.+5*ZBOT()/.6371221.3)          NEWP 27
11 CONTINUE $ WRITE (35,611),STITLE,(RBOT(J),ZBOT(J),J=1,NBPT)    NEWP 28
611 FORMAT (10F8.3)                                NEWP 29
511 FORMAT (10F8.3)                                NEWP 30
ZMAX=0, $DB 4 I=1,NBPT                          NEWP 31
4 IF(ZBOT(I),GT,ZMAX) ZMAX=ZBOT(I)              NEWP 32
CONTINUE                                         NEWP 33
13BPT=0 S IF (IS,EO,0,AND.LA,EO,0,OR.LA,EO,1) LPN=60
NN(2)=0 S IF (IS,EO,1) LPN=6                      NEWP 34
DO 55 I=1,2                                      NEWP 35
DO 55 J=1,50                                     NEWP 36
ZIL(I,J)=0.0                                     NEWP 37
VIL(I,J)=0.0                                     NEWP 38
55 ICAN(I,J)=0.0                                 NEWP 39
NN(1)=0                                         NEWP 40
NIB=0                                           NEWP 41
DO 56 J=1,50                                     NEWP 42
Z1(J)=0.0                                       NEWP 43
V1(J)=0.0                                       NEWP 44
Z2(J)=0.0                                       NEWP 45
56 V2(J)=0.0                                     NEWP 46
ASSIGN 6 TO IRET
GO TO 70                                         NEWP 47
6 AT 70 IS THE READIN AND CONNECT ROUTINE. RETURN IS TO IRET
ASSIGN 20 TO IRET                                NEWP 48
GO TO 70                                         NEWP 49
C
6

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20  IBPT=IBPT+1
    IF((IBPT.LE.NBPT) GO TO 21
    RBT=.001+R2*100,
    IFPR=1
    GO TO 22
21  RBT=RBT(IBPT)
    ZBT=ZBT(IBPT)
    IF (RM.LE.RBT.AND.IFE0F.EQ.1.AND.RS.NE.0.0) IFPR=1
22  IF(RBT.LE.RB) GO TO 25
C   GET NEW INPUT PROFILE
    ASGIGV 23 TO IRET
    GO TO 70
23  IF ((IBPT.GT.NBPT) GO TO 25
    IBPT=IBPT+1
    ZBT=ZBT+(RA-RBT)*(ZBT-ZB0T([IBPT]))/(RBT-RB0T([IBPT]))
C   THIS IS THE BOTTOM DEPTH AT PROFILE RANGE
    RBT=RA
25  R1=R2
    N1=N2
C   MOVE PROFILE 2 TO PROFILE 1
    D0 27 I=1,N2
    Z1(I)=Z2(I)
27  V1(I)=V2(I)
    R2=1000.+RBT
    FA=(RB-RBT)/(RB-RA)
    FB=1.+FA
    N2=1
29  IF (ICBN(1,N2).GT.NN(1)) ICBN (1,N2)=NN(1)
    IF (ICBN(2,N2).GT.NN(2)) ICBN (2,N2)=NN(2)
    Z=FA*ZIL(1,[ICBN(1,N2)])+FB*ZIL(2,[ICBN(2,N2)])
    V=FA*VIL(1,[ICBN(1,N2)])+FB*VIL(2,[ICBN(2,N2)])
    IF (N2.GT.1.AND.Z.LT.Z? (N2-1)) 125,126
125 Z=Z2(N2-1)
    V=V2(N2-1)
126 IF(Z.GT.ZBT-1.) GO TO 35
    Z2(N2)=Z
    V2(N2)=V
    N2=N2+1
    IF(N2.LE.NIB) GO TO 29
C   EXTRAPOLATION TO BOTTOM
    Z2(N2)=ZBT
    M=N2-1
31  M=M-1
    Z=Z2(M)
    IF(ABS(Z-Z2(N2-1)).LT.1,E-5+Z) GO TO 31
    V=V2(M)
    V2(N2)=V2(M) +(ZBT-Z)*(V2(N2-1)*V)/(Z2(N2-1)-Z)
    GO TO 40
35  Z2(N2)=ZBT
    V2(N2)=V2(N2-1)+(ZBT-Z? (N2-1))*(V-V2(N2-1))/(Z-Z2(N2-1))
C   REMOVE DUPLICATE POINTS
40  M=2
    IBC=0
42  IF ((Z2(M).GT.Z2(M-1)+0.0001) GO TO 45
    IBC=1
    N2=N2+1
    GO TO 70
    NEWP 57
    NEWP 58
    NEWP 59
    NEWP 60
    NEWP 61
    NEWP 62
    NEWP 63
    NEWP 64
    NEWP 65
    NEWP 66
    NEWP 67
    NEWP 68
    NEWP 69
    NEWP 70
    NEWP 71
    NEWP 72
    NEWP 73
    NEWP 74
    NEWP 75
    NEWP 76
    NEWP 77
    NEWP 78
    NEWP 79
    NEWP 80
    NEWP 81
    NEWP 82
    NEWP 83
    NEWP 84
    NEWP 85
    NEWP 86
    NEWP 87
    NEWP 88
    NEWP 89
    NEWP 90
    NEWP 91
    NEWP 92
    NEWP 93
    NEWP 94
    NEWP 95
    NEWP 96
    NEWP 97
    NEWP 98
    NEWP 99
    NEWP 100
    NEWP 101
    NEWP 102
    NEWP 103
    NEWP 104
    NEWP 105
    NEWP 106
    NEWP 107
    NEWP 108
    NEWP 109
    NEWP 110
    NEWP 111
    NEWP 112

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        D0 44 I=M,N2          NEWP 113
        Z2(I)=Z2(I+1)        NEWP 114
        V2(I)=V2(I+1)        NEWP 115
        M$=M+1                NEWP 116
        IF(M.LE.N2) G0 T0 42  NEWP 117
        IF (IDC,GT,0) G0 T0 40  NEWP 118
        IF (Z2(N2+1),EQ,0,0) G0 T0 46  NEWP 119
        N5=N2+1                NEWP 120
        D0 47 I=N5,N0          NEWP 121
        Z2(I)=0,0              NEWP 122
        47 V2(I)=0,0          NEWP 123
        46 IF (IPROP,EQ,0,GR,IPROP,EQ,1) G0 T0 54  NEWP 124
        PRINT 902,R2            NEWP 125
        PRINT 914                NEWP 126
        D0 7 J=1,N2            NEWP 127
        NV=V2(J)=1455,5        NEWP 128
        IF (NV.LT.,4,GR,NV,GT,114) G0 T0 48  NEWP 129
        LIN(NV)=1H#
        PRINT 915,Z2(J),V2(J),LIN  NEWP 130
        LIN(NV)=1H               NEWP 131
        G0 T0 7                  NEWP 132
        48 PRINT 915,Z2(J),V2(J)  NEWP 133
        7 CONTINUE                NEWP 134
        54 IF (IPFL,EQ,1) CALL PRPFPLT (RB,N3,INPF)  NEWP 135
        IF (IPFL,EQ,2) CALL PRPFPLIT (RB,N3,INPF)  NEWP 136
        IF (RS,GE,RRBT(2),ER,IFEBF,EQ,1) RETURN $ PRINT 275 $ CALL BYERE  NEWP 137
        275 FORMAT (5X,*PROGRAM ABRTED, TWO SOUND SPEED PROFILES INPUT REFORGENEWP 138
        1 SECOND BOTTOM POINT*)  NEWP 139
        70 IF (NN(2),EQ,0) G0 T0 75      $ NB=NN(2)  $ D0 71 I=1,NB  NEWP 140
        ZIL(1,I)=ZIL(2,I)          NEWP 141
        71 VIL(1,I)=VIL(2,I)          NEWP 142
        RA=RB                      NEWP 143
        75 NH(1)=NN(2)                NEWP 144
        IF (IFEZF,EO,0) G0 T0 76    NEWP 145
        RB=RB1,E6                  NEWP 146
        G0 T0 82                  NEWP 147
        76 IF (LPN,EO,60)READ (LPN ,903) NCUR,RB,TITLE  NEWP 148
        IF (LPN,EO, 6)READ (LPN)   NCUR,RB,TITLE  NEWP 149
        IF (EOF,LPN ) 77,78        NEWP 150
        77 IFEZF=1 $ IFE=IFEZF  NEWP 151
        RB=RA+1,E6 $ IF (LA,EO,,) ENDFILE 6  NEWP 152
        IF (LA,EO,,GR,IS,EO,,)REWIND 6 $ G0 T0 82  NEWP 153
        78 IL=1 $ IF (LA,EO,,) WRITE (6)   NCUR,RB,TITLE  $ RS=RB  NEWP 154
        IH=IL+4                  NEWP 155
        IF (LPN,EO,50)READ (LPN ,900) (ZIL(2,I),VIL(2,I),I=IL,IH)  NEWP 156
        IF (LPN,EO, 6)READ (LPN)   (ZIL(2,I),VIL(2,I),I=IL,IH)  NEWP 157
        IF (LA,EO,,)WRITE ( 6)   (ZIL(2,I),VIL(2,I),I=IL,IH)  NEWP 158
        IF (VIL(2,IH).LE,0,) G0 T0 81  NEWP 159
        IL=IL+5                  NEWP 160
        G0 T0 79                  NEWP 161
        IH=IH+1                  NEWP 162
        IF (VIL(2,IH).LE,0,) G0 T0 81  NEWP 163
        NN(2)=IH                 NEWP 164
        N3=IH                     NEWP 165
        INPF=0                    NEWP 166
        IF (IPROP,EO,0) G0 T0 74  NEWP 167
        NEWP 168

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PRINT 904,RR,TITLE
PRINT 914
74 GO TO 1,IH
IF (VIL(2,I).LT.1400.0) GO TO 58,5
58 PRINT 920,RR,ZIL(2,I),VIL(2,I)
920 FORMAT(1H1,5X,•INPLT ERROR IN PROFILE AT RANGE•,F10.4,5X,•VALUE AT•NEWP 169
1 DEPTH•,F10.3,••,F10.3,• M/SEC•)
CALL BYEBYE NEWP 170
57 IF (ZIL(2,I).NE.SCS) GO TO 257 S PRINT 258,ZIL(2,I),RR$CALL BYEBYE NEWP 171
258 FORMAT (5X,•PROGRAM ABORTED, INPUT PROFILE DEPTH•,F10.3,1X,••SOURCE•NEWP 172
1E DEPTH, AT RANGE•,F10.3,• KM•)
257 IF (I.EQ.1) GO TO 157 $IF (ZIL(2,I).LT.ZIL (2,I-1)) GO TO 52 NEWP 173
157 IF (IPREP.EQ.0) GO TO 28 SNV=VIL(2,I)-455.5 NEWP 174
IF (NV.LT.4.0R.NV.GT.114) GO TO 38 S LIN(NV)=1HV NEWP 175
PRINT 915,ZIL(2,I),VIL(2,I),LIN NEWP 176
LIN (NV)=1H NEWP 177
GO TO 23 NEWP 178
38 PRINT 915,ZIL(2,I),VIL(2,I)
29 CONTINUE NEWP 179
IF (INCUR.GT.0) GO TO 89 NEWP 180
DO 80 I=1,IH NEWP 181
VIL(2,I)=VIL(2,I)*(1.+ZIL(2,I)/6371221.3) NEWP 182
69 IF (IPFL.EQ.1) CALL PROFPLAT (RR,N3,INPF) NEWP 183
IF (IPFL.EQ.2) CALL PROFPLIT (RR,N3,INPF) NEWP 184
IF (NN(1).EQ.0) GO TO 1RET,(6,20,23) NEWP 185
82 ICBN(1,1)=1 NEWP 186
ICBN(2,1)=1 NEWP 187
NA=2 NEWP 188
NB=2 NEWP 189
NIB=2 NEWP 190
83 IF (ZIL(2,NIB).EQ.ZIL(1,NIB)) GO TO 92 NEWP 191
IF (NB.LE.NN(2)) GO TO 84 NEWP 192
IP=2 NEWP 193
GO TO 88 NEWP 194
84 IF (NA.LE.NN(1)) GO TO 85 NEWP 195
IP=1 NEWP 196
GO TO 88 NEWP 197
85 DVMA=VIL(1,NA)-VIL(1,NA-1) NEWP 198
DVLA=DVMA NEWP 199
DVHA=DVMA NEWP 200
IF (NA.GT.2) DVLA=VIL(1,NA-1)-VIL(1,NA-2) NEWP 201
IF (NA.LT.NN(1)) DVHA=VIL(1,NA+1)-VIL(1,NA) NEWP 202
DVME=VIL(2,NB)-VIL(2,NB-1) NEWP 203
DVLB=DVMB NEWP 204
DVHB=DVMB NEWP 205
IF (NP.GT.2) DVLB=VIL(2,NB-1)-VIL(2,NB-2) NEWP 206
IF (NB.LT.NN(2)) DVHB=VIL(2,NB+1)-VIL(2,NB) NEWP 207
PM(1)=ABS(ZIL(1,NA-1)-ZIL(2,NB)) NEWP 208
IF (DVLA=DVMB.GE.0,.AND.DVHA=DVHB.GE.0;) PM(1)=PM(1)-250, NEWP 209
IF (DVLA=DVMB.GE.0,.AND.DVHA=DVMB.GE.0;) PM(2)=PM(2)-250, NEWP 210
IF (DVMA=DVMB.GE.0,.AND.DVHA=DVMB.GE.0;) PM(3)=PM(3)-250, NEWP 211
BP=PM(1) NEWP 212
IP=1 NEWP 213
IF (DVLA=DVMB.GE.0,.AND.DVHA=DVHB.GE.0;) PM(1)=PM(1)+250, NEWP 214
IF (DVLA=DVMB.GE.0,.AND.DVHA=DVMB.GE.0;) PM(2)=PM(2)+250, NEWP 215
IF (DVMA=DVMB.GE.0,.AND.DVHA=DVMB.GE.0;) PM(3)=PM(3)+250, NEWP 216

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D6 87 I=2,3          NEWP 225
IF(pM(1).GE.BP) G8 T8 87      NEWP 226
IP=1                  NEWP 227
BP=PM(1)              NEWP 228
87 G8 T8 {90,91,92},1P      NEWP 229
88 IC9N(1,NIB)=NA-1      NEWP 230
90 IC9N(2,NIB)=NB      NEWP 231
NB=NB+1              NEWP 232
G8 T8 93              NEWP 233
91 IC9N(1,NIB)=NA      NEWP 234
IC9N(2,NIB)=NB+1      NEWP 235
NA=NA+1              NEWP 236
G8 T8 93              NEWP 237
92 IC9N(1,NIB)=NA      NEWP 238
IC9N(2,NIB)=NB      NEWP 239
NA=NA+1              NEWP 240
NB=NB+1              NEWP 241
93 IF(NA.GT.NN(1).AND.NB.GT.NN(2)) G8 T8 IRET,(6,20,23)  NEWP 242
NIB=NIB+1              NEWP 243
IF (NIB.LE.50) G8 T8 83      NEWP 244
PRINT 905              NEWP 245
CALL BYEBYE            NEWP 246
900 FORMAT(10F8.4)        NEWP 247
901 FORMAT(24H0LISTING OF BOTTOM TRACK/1H0.4X,5(6H R(KH),6X,4HZ(M),4X) NEWP 248
1 //({X,10F10.3})      NEWP 249
902 FORMAT(30H0INTERPOLATED PROFILE AT RANGE,F10.0,2H M//)  NEWP 250
903 FORMAT(1,1F7.3,9A8)    NEWP 251
904 FORMAT(23H1INPUT PROFILE AT RANGE,F11.3,3H KH,5X,9A8//)  NEWP 252
914 FORMAT (3X,*DEPTH(M)=,2X,*VELCITY*,*1460*,6X,*1470*,6X,*1480*,6X,NEWP 253
1*1490*,6X,*1500*,6X,*1510*,6X,*1520*,6X,*1530*,6X,*1540*,6X,*1550*,6X,NEWP 254
2,6X,*1560*,6X,*1570*,//)  NEWP 255
915 FORMAT (1X,F11.4,F10.4,11A1)  NEWP 256
905 FORMAT ( 29H0TOP MANY POINTS INTERPOLATED)  NEWP 257
END                      NEWP 258
                                NEWP 259

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DS NEWPRBF

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ED 0

	IDENT	NEWPRBF
PROGRAM LENGTH	03072	
ENTRY POINTS	00471	NEWPRBF
BLOCK NAMES		
INFO	00024	
PRBFIL	00316	
INPUT	01442	
TLE	00012	
PRO	00006	
ABC	00026	
IFC	00007	
RANST	00004	

## EXTERNAL SYMBOLS

THEND,  
\$1010100  
\$80DICT,  
PRBFPLT  
PRGFPLIT  
BYEBYE  
\$8C1FE0F  
EFT,  
REW,  
TSW,  
TSB,  
STM,  
STB,  
SLB,  
SLY,  
ONSINGL,

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SUBROUTINE CONNECT
C34461 /PROFIL/ N1,N1,Z1(50),V1(50),P2,N2,Z2(50),V2(50),IBOTC,IPFL,CONN 1
C34461 /THIANG/ AP(100,2),BP(100,2),AL(100),BL(100),ZZFR0(100),   CENN 2
      RZEN0(100),AA(100),E0(100),SST(100),CCT(100),NTRI           CENN 3
      NA=N3=1               CENN 4
      NTRI=0               CENN 5
      IAD0=0               CENN 6
      NTRI=NTRI+1          CENN 7
      IF(NB,E0,N2) GE TO 12 CENN 8
      IF((I400,E0,1,PR,NA,E0,V1) GE TO 30 CENN 9
      RZER0(NTRI)=R2          CENN 10
      ZZFR0(NTRI)=Z2(V4)    CENN 11
      AL(NTRI)=Z1(NA+1)     CENN 12
      BL(NTRI)=(Z2(NA)+Z1(NA+1))/(R2+R1) CENN 13
      AA(NTRI)=1./V2(NB)*2 CENN 14
      RZ=(1.,D0/V2(NA)**2+1.,DC/V1(NA)**2)/(Z1(NA)+Z1(NA+1)) CENN 15
      PR=(1.,D0/V2(NB)**2+1.,DC/V2(NB)**2+RZ*(Z2(NB)+Z1(NA))/(R2+R1)) CENN 16
      NA=NA+1               CENN 17
      IAD0=1               CENN 18
      GE TO 40               CENN 19
      RZER0(NTRI)=R1          CENN 20
      ZZFR0(NTRI)=Z1(NA)    CENN 21
      AL(NTRI)=Z1(NA)        CENN 22
      BL(NTRI)=(Z1(NA)-Z2(NB+1))/(R1+R2) CENN 23
      AA(NTRI)=1./V1(NA)**2 CENN 24
      RZ=(1.,D0/V2(NA)**2+1.,DC/V2(NB+1)**2)/(Z2(NB)-Z2(NB+1)) CENN 25
      PR=(1.,D0/V1(NA)**2+1.,DC/V2(NB)**2+RZ*(Z1(NA)-Z2(NB))/(R1+R2)) CENN 26
      NB=NB+1               CENN 27
      IAD0=0               CENN 28
      GE TO 40               CENN 29
      RZ(NTRI)=S1*(S2*(R2**2+R4**2),R2) CENN 30
      IF(BB(NTRI),E2,0,1) GE TO 41 CENN 31
      SST(NTRI)=R2*BB(NTRI) CENN 32
      CCT(NTRI)=R2*BB(NTRI) CENN 33
      GE TO 42               CENN 34
      CCT(NTRI)=1,             CENN 35
      SST(NTRI)=0,             CENN 36
      AL(NTRI)=AL(NTRI)+BL(NTRI)*R1 CENN 37
      TANT=S1(NTRI)/AMAX1(CCT(NTRI),1,E=100) CENN 38
      BP(NTRI,2)=R2*(BL(NTRI)*TANT)/(1,-BL(NTRI)*TANT) CENN 39
      R=AL(NTRI+1)            CENN 40
      IF(NTRI,E2,1) R=0       CENN 41
      BP(NTRI,1)=(R+TANT)/(1,-E*TANT) CENN 42
      AP(NTRI,1)=AP(NTRI,2)=0, CENN 43
      IF(NA,L1,N1,P2,N2,V2,LT,N2) GE TO 10 CENN 44
      RETURN                 CENN 45
      END                   CENN 46
                                         CENN 47

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DS CONNECT

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	IDENT	CONNECT
PROGRAM LENGTH	00414	
ENTRY POINTS	CONNECT	00003
BLOCK NAMES		
PROFILE	00316	
THIANG	02261	
EXTERNAL SYMBOLS		
01C1921J		
01C0421J		
08TDCIT,		
SQRTF		
MAXIF		

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SUBROUTINE PREPPLT (R1,N3,INPF)
COMMON /PREFIL/ R1,N1,Z1(50),V1(50),R2,N2,Z2(50),V2(50),IBTC,IPFLPLT 1
COMMON /DIMEN/ X(4),XP(50),Y(50),PLTARRAY(254),ZDEPTH(250),XRANGPLT 2
COMMON /XT(10),X(4),XP(50),Y(50),PLTARRAY(254),ZDEPTH(250),XRANGPLT 3
1E (250),XL(50),YL(400),YP(10) PLT 4
COMMON /INPUT/ RBOT(250),ZBOT(250),ZIL(2,50),VIL(2,50),NN(2),ICON(2PLT 5
1,50)
COMMON /LIMITS/R0(10),DR(10),R02(10) PLT 6
COMMON /PREP/ IPREP,IKNM,PLTL,RM,IPC0,IFPR PLT 7
COMMON /TITLE/ (10) PLT 8
COMMON /ABC/ PUNCHDB (16),INCR,NBRS,NSRS,ALIM,IFT,IFT1 PLT 9
DATA (IPL0=0),(IST=0),(IFT2=0),(IRH=0),(IJ=0) PLT 10
IF (IPC0.EQ.1.AND.IPL0.EQ.0,IR,IST,FQ,1) GO TO 10n PLT 11
IF (IPL0.EQ.1) GO TO 1 $ CALL PLGTS (PLTARRAY,254,3) PLT 12
100 IF (IFT1.EC,IFT2) GO TO 952 $ IRH=0 $ IFT2=IFT1 PLT 13
152 IF (IFT1.EC,0.AND.IJ.EQ.1,IRH.EQ.1) RETURN PLT 14
IRH=1 $ IPL0=1 $ IPC0=1 $ IST=0 $ IJ=1 PLT 15
RM=MAX1F(R02(1),R02(2),R02(3),R02(4),R02(5),R02(6),R02(7),R02(8),PLT 16
1R02(9),R02(10)) $ IDI=n $ K=0 PLT 17
20 K=K+1 $ IF (RM.GT.RBOT(K)) 20,21 PLT 18
21 ZMAX=ZBOT(1) PLT 19
D622 J=2,K PLT 20
22 ZMAX= MAX1F(ZBOT(J),ZMAX) PLT 21
IF (ZMAX.LE. 250.0,AND,ZMAX.GT. 0.0 ) ZMAX= 250.0 PLT 22
IF (ZMAX.LE. 500.0,AND,ZMAX.GT. 250.0 ) ZMAX= 500.0 PLT 23
IF (ZMAX.LE. 1000.0,AND,ZMAX.GT. 500.0 ) ZMAX= 1000.0 PLT 24
IF (ZMAX.LE. 2000.0,AND,ZMAX.GT.1000.0 ) ZMAX= 2000.0 PLT 25
IF (ZMAX.LE. 4000.0,AND,ZMAX.GT.2000.0 ) ZMAX= 4000.0 PLT 26
IF (ZMAX.LE. 5000.0,AND,ZMAX.GT.4000.0 ) ZMAX= 5000.0 PLT 27
IF (ZMAX.LE.10000.0,AND,ZMAX.GT.5000.0 ) ZMAX=10000.0 PLT 28
CG 25 J=1,11 PLT 29
A=(ZMAX/10.0)*(J-1) PLT 30
IF (J.EQ.6) CALL SYMBGL (-1.00,5.0,0.14,9HDEPTH (H),90,0,9) PLT 31
XL(J)=0.0 PLT 32
Y(J)=(11-J) PLT 33
25 CALL NUMBER(-0.80,Y(J),0.140,A,0.0,4HF3,0) PLT 34
CALL LINE (XL,Y,11,1,3,0.105,1) PLT 35
CG 26 J=1,250 PLT 36
28 YL(J)=0.0 PLT 37
IF (PLTL.GT.156.0) CALL BYEBYE PLT 38
RSCALE=PLTL/RM PLT 39
NTM=AMIN1(PLTL+1.,40.5) PLT 40
RT=1. PLT 41
RMAX=RM PLT 42
IF (IKNM.GT.0) RMAX=RM /1.852 PLT 43
NTERMAN/RT PLT 44
IF(NT,LE.NTM) GO TO 57 PLT 45
RT=2.*RT PLT 46
NTERMAN/RT PLT 47
IF(NT,LE.NTM) GO TO 57 PLT 48
RT=2.*RT PLT 49
NTERMAN/RT PLT 50
IF(NT,LE.NTM) GO TO 57 PLT 51
RT=2.*RT PLT 52
GO TO 56 PLT 53
57      PLT SURFACE AXIS PLT 54
      CALL PL0T(0., 0.,3) PLT 55
                                         PLT 56

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XN=0,
RSCALE1=RSCALE
IF (IXNM.GT.0) RSCALE1=1.852*RSCALE
DX=R*T*RSCALE1
R=0,
IF=0
58 CALL PL0T(XN,0.,2)
CALL PL0T(XN,-0.05,2)
R=R
CALL NUMBER(XN,-48,-0.19,1.4E-1,RK,0.,4HF4,0)
IF(R,LY,RMAN/2,) GO TO 59
IF(IF,EG,1) GO TO 59
IF (IXNM,EG,0) 4,7
7 CALL SYMBGL(XN-0.30,-0.40,0.0,14,10HRANGE (NM),0.,10)
GO TO 8
4 CALL SYMBGL(XN-0.30,-0.40,0.0,14,10HRANGE (NM),0.,10)
8 CALL SYMBEL (XN-7.20,10,15,0.21,STITLE,0.,00)
IF=1
59 CALL PL0T(XN,0.,3)
IF(R,GE,RMAN) GO TO 60
XN=XN+DX
R=R+RT
GO TO 58
60 IDP=0
1 IF ((IFPR,EG,1) GO TO 5
X(3)=(R2/1000.0)*RSCALE
IF (1,PF,EG,0) X(3)=R1*RSCALE
X(1)=X(3)+1.5
IF (1,PF,EG,1) GO TO 2   S IF (X(3).GT,PLTL) GO TO 35
DS ,5 J=1,N3
15 XP()=((0.5*VIL(2,)-735.0)*0.1)*X(3)
IDI=IDI+1
XL(IDI)=X(3)
IF (IDI,GE,2) GO TO 50
CALL SYMBEL (X(1)*0.02,10,27,0.10,16HVELCITY (M/SEC),0.0,16)
TX=0.5
50 N=2
DS 55 J=1,N
XT(J)=X(1)+(J-1)*TX
YP(J)=10.02
XM=1500.0
DX=10.0
PL=XM*(J-1)*DX
IF (IDI,EG,1) CALL NUMBER(XT(J)-0.07,10,10,,103,PL,0.0,4HF4,0)
55 CONTINUE
IF(X(3).LE.PLTL) CALL LINE (XT,YP,N,1,13.0,0.07,1)
IF (1,PF,EG,1) GO TO 2
DS 3 I=1,N3 SY(I)=10.0*(1.0-(ZIL(2,I)/ZMAX))
3 IF (Y(I).LT.0.0) Y(I)=0.0
IF (X(3).LE.PLTL) CALL LINE (XP,Y,N3,1,-2.0,0.0)
35 INPF=1
GO TO 5
2 DS 6 I=1,N2 SY(I)=10.0*(1.0-(Z2(I)/ZMAX))
6 IF (Y(I).LT.0.0) Y(I)=0.0
IDP=IDP+1
ZDEPTH(IDP)=Y(N2)
XRANGE (IDP)=X(3)
5 IF ((IFPR,EG,0) GO TO 30
CALL LINE (XRANGE,ZDEPTH,1,1,1,0.0,0)
CALL LINE (XL, YL,1D1, 1,3,0.140,*1)
CALL PLOTS (0,0)  S CALL PL0T (PLTL*10.0*0.0,-3)  S IST=1
30 RETURN
END
      PL0T  57
      PL0T  58
      PL0T  59
      PL0T  60
      PL0T  61
      PL0T  62
      PL0T  63
      PL0T  64
      PL0T  65
      PL0T  66
      PL0T  67
      PL0T  68
      PL0T  69
      PL0T  70
      PL0T  71
      PL0T  72
      PL0T  73
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      PL0T  75
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      PL0T  78
      PL0T  79
      PL0T  80
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      PL0T  90
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      PL0T  94
      PL0T  95
      PL0T  96
      PL0T  97
      PL0T  98
      PL0T  99
      PL0T 100
      PL0T 101
      PL0T 102
      PL0T 103
      PL0T 104
      PL0T 105
      PL0T 106
      PL0T 107
      PL0T 108
      PL0T 109
      PL0T 110
      PL0T 111
      PL0T 112
      PL0T 113
      PL0T 114
      PL0T 115
      PL0T 116
      PL0T 117
      PL0T 118
      PL0T 119

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DS PREFPLOT

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ED 0

	IDENT	PREFPLOT
PROGRAM LENGTH	03700	
ENTRY POINTS	PREFPLOT	02503
BLOCK NAMES		

PREFIL	00316
INPUT	01442
LIMITS	00036
PRO	00006
TLE	00012
ABC	00026

## EXTERNAL SYMBOLS

01010100
280DICT,
PLOTS
SYMBOL
NUMBER
LINE
BYEBYE
PLOT
MINIF
MAXIF

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      IF (PL.GE.1400.0.AND.PL.LE.1500.0) PL=PL-1400.0          PLIT  57
55 CALL NUMBER (XT(J)=0.07,10,10,0.07,PL,0.0,4HF2.0)          PLIT  58
      CALL LINE (XT,YP,N,1,13,0.07,1)                           PLIT  59
      IF (INPF.EQ.1) GO TO 2                                    PLIT  60
60 INPF=1
      IDI=IDI+1
      XI{IDI}=X{J}
      IF (X{J}.GE.RJ/4.0.AND.ITAL.EQ.0) 35,5                PLIT  61
35 ITL=1
      IF (IKNM.EQ.0) CALL SYMBOL (RJ/2.0-0.6,-0.40,0.14,10HRANGE (KM),0,PLIT 66
10,10)                                                 PLIT  67
      IF (IKNM.GT.0) CALL SYMBOL (RJ/2.0-0.6,-0.40,0.14,10HRANGE (NM),0,PLIT 68
10,10)                                                 PLIT  69
      CALL SYMBOL (RJ/2.0-4.8,10.20,0.14,STITLE,0.0,80)        PLIT  70
      GO TO 5                                              PLIT  71
2 DO 6 I=1,N2
      Y{I}=10.0*(1.0-(Z2{I})/ZMAX))  S IF(Y{I}).LT.0.0) Y{I}=0.0  PLIT  72
      XL{I}=X{3}
6 CALL NUMBER (X{2}*X{1},Y{I},0.07,Z2{I},0.0,4HF4.0)          PLIT  73
      CALL LINE (XL,Y,N2,1,3,0.07,1)                           PLIT  74
      CALL LINE (XP,Y,N2,1,1,0.07,1)                           PLIT  75
      CALL NUMBER (X{3}-0.30,-0.25,0.105,X{4},0.0,4HF4.0)        PLIT  76
      IDP=IDP+1
      ZDEPTH(IDP)=Y(N2)
      XRANGE (IDP)=X{3}
      IF (X{3}.GE.RJ/4.0.AND.ITAL.EQ.0) 45,5                PLIT  77
45 ITL=1
      IF (IKNM.EQ.0) CALL SYMBOL (RJ/2.0-0.6,-0.40,0.14,10HRANGE (KM),0,PLIT 84
10,10)                                                 PLIT  85
      IF (IKNM.GT.0) CALL SYMBOL (RJ/2.0-0.6,-0.40,0.14,10HRANGE (NM),0,PLIT 86
10,10)                                                 PLIT  87
      CALL SYMBOL (RJ/2.0-0.6,10.20,0.14,STITLE,0.0,48)        PLIT  88
5 IF (IFPR.EQ.0) GO TO 30                                  PLIT  89
      CALL LINE (XRANGE,ZDEPTH,IDP,1,1,0,0,0,                  PLIT  90
      CALL LINE (XRANGE,YL,IDP,1,3,0.105,1)                   PLIT  91
      CALL LINE (XI,YL,IDL,1,3,0.21,1)                         PLIT  92
      CALL PLOT (0,0)  S  CALL PLOT (PLT,10.0,0,/-3)  S  IST=1    PLIT  93
130 RETURN
      END                                              PLIT  94
                                                PLIT  95

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DS PREFPLIT

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ED 0

	IDENT	PREFPLIT
PROGRAM LENGTH	03745	
ENTRY POINTS	02654	
BLOCK NAMES		
PREFIL	00316	
INPUT	01442	
LIMITS	00036	
PRE	00006	
TLE	00012	
ABC	00026	

## EXTERNAL SYMBOLS

C1C10100  
G82DICT,  
PLTS  
SYMBOL  
NUMBER  
LINE  
BYEBYE  
SCALE  
PLST  
MAX1F

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SUBROUTINE ADVANCE  
 CEMMER /THIARG/ AP(100,2),BP(100,2),AL(100),BL(100),ZZERO(100),  
 1 HZERO(100),AA(100),EB(100),SST(100),CCT(100),NTRI  
 CEMMER /RAYS/ ARAY,TGAM(1000),ZZ(1000),SS(1000),TIME(1000),  
 1 NCEUNT(1000),PHASE(1000)  
 CEMMER /INFO/ RSTART,RMAX,CMEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,  
 1 ISCP,ITS,IT2,IT3,IPER,IFTIMS,LTRT,LTER,LTRP,LPIN,IATT  
 CEMMER /PIDEF/ PI,ETA,TWEP  
 CEMMER /MIRRORS/ SL,BRLT(200),RPST(200)  
 CEMMER /ARC/PLANCHOB (16),INCR,NBRS,NSRS,ALIM,IFT,IFT1  
 DIMENSION RPNEW(4),RAE(4),ZAEW(4),ZPNEW(4)  
 LEGICAL BNUP,ENLW  
 TANSLM(A,B)=(A+B)/(1,-A\*B)  
 CELL(TR,T,S)=ABS(LR)\*SCHT(CM(S))\*(1.+(T\*(T+S)+S\*S)/3.)  
 C       LEGP OVER ALL THE RAYS  
 DO 100 IRAY=1,ARAY     \$ IHIST=0           \$ SSR=SS(IRAY)  
 IF (NBRS,EQ,2500,AND,NSHS,EQ,2500) GO TO 10  
 N=NCEUNT(IRAY) \$H=NA/ITN \$A=AM/ITN \$N=NN/ITN \$H=NN/ITN \$ABR=MADV  
 10 IF (ABS(\$SH),LT,ALIM,ER,NBR,GT,NBRS,UR,NSR,GT,NSRS) GO TO 100  
 ZR=ZZ(IRAY)     \$ RR=RSTART  
 TGR=TGAM(IRAY)  
 TRAY=TIME(IRAY)  
 I+REPHASE(IRAY)  
 NCTR=NCEUNT(IRAY)  
 DE 20 I=1,NTRI  
 C       FIND CORRECT LAYER  
 P=ZR=AL(I)=BL(I)\*RR  
 IF (P,.EQ.,0.001,GT,0.) GO TO 20  
 \TRR=I  
 IF (ABS(P),GT,.0001,GT,TGR,GT,=BL(I)) GO TO 30  
 20 CONTINUE  
 GE TG 80  
 30 CT=CCT(NTRR)  
 IF (IPRAY,NE,1) PRINT 666,IRAY,NTRR,ZR,RR,TGR,NCTR  
 ST=SS(NTRR)  
 ZD=ZZERO(NTRR)  
 C       TRANSFORM TO PRIMED COORDINATES  
 R0=RZERO(NTRR)  
 ZRP=CT\*(ZR-ZD)+ST\*(RR-R0)  
 RRP=CT\*(RR-R0)+ST\*(ZR-ZD)  
 CIS=AA(NTRR)+BB(NTRR)\*ZRP  
 TANT=ST/AMAX1(CT,1,E-300)  
 TGRP=TANSLM(TANT,+TGR)  
 CMIS=CIS/(1.+TGRP\*.2)  
 C       CALCULATE PARABOLIC RAY PATH; ALPHA IS THE CURVATURE  
 ALPHAS=.25\*BB(NTRR)/CMIS  
 TA=2.\*ALPHA  
 C       FIND INTERSECTIONS WITH UPPER AND LOWER LAYER BOUNDARIES  
 DE 40 I=1,2  
 APNTR=AP(NTRR,I)  
 BPNTR=BP(NTRR,I)  
 C=APNTR-BPNTR=RRP-ZRP  
 P=BPNTR-TGRP  
 IF (ABS(ALPHA),GT,1,E-25) GO TO 303  
 RAY PATH IS LINEAR FOR THESE STATEMENTS  
 CRP=-C/P

ADVA0000  
 ADVA0001  
 ADVA0002  
 ADVA0003  
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 ADVA0044  
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 ADVA0049  
 ADVA0050  
 ADVA0051  
 ADVA0052  
 ADVA0053  
 ADVA0054  
 ADVA0055

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K=2*I+1          ADVA0056
RPNEW(K)=RRP+CRP   ADVA0057
ZPNEW(K)=ZRP+TGRP+CRF   ADVA0058
ZAEW(K)=CT*ZPNEW(K)+ST*HPNEW(K)+ZO   ADVA0059
RNEW(K)=CT*RNNEW(K)+ST*ZPNEW(K)+RO   ADVA0060
ZAEW(K+1)=I,E300   ADVA0061
ZPNEW(K+1)=I,E309   ADVA0062
RNEW(K+1)=I,F300   ADVA0063
RNNEW(K+1)=I,E303   ADVA0064
GE TO 40          ADVA0065
C      SOLVE QUADRATIC EQUATION FOR PARABOLIC PAY PATH   ADVA0066
303  DISC=P0+4,*ALPHA+C   ADVA0067
IF(DISC<LT,0,) GO TO 32   ADVA0068
DISC=SQRT(DISC)   ADVA0069
DE 31 J=1,2   ADVA0070
K=2*I+J+2   ADVA0071
S=2*J+3   ADVA0072
F=P+S/DISC   ADVA0073
CRP=F/TA   ADVA0074
C      ITERATION TO IMPROVE ACCURACY FOR SMALL CURVATURE PAYS   ADVA0075
IF(ABS(F),LT,,1+ABS(F)) CRP=(ALPHA*((ALPHA*DHP**2+C)/P,**2-C))/P   ADVA0076
305  RPNEW(K)=RRP+CRP   ADVA0077
ZPNEW(K)=ZRF+CRP*(TGRP+ALPHA*CRP)   ADVA0078
ZAEW(K)=CT*ZPNEW(K)+ST*RPNEW(K)+ZO   ADVA0079
RNEW(K)=CT*RPNEW(K)+ST*ZPNEW(K)+RO   ADVA0080
GE TO 40          ADVA0081
32  DE 33 J=1,2   ADVA0082
K=2*I+J+2   ADVA0083
33  RNEW(K)=I,E300   ADVA0084
40  CONTINUE   ADVA0085
CNL=ABS(ZR-AL(NTRR)-BL(NTRR)*RR),LT,,G1,AND,TGR,GT,-BL(NTRR)   ADVA0086
C      SELECT CORRECT INTERSECTION AS NEXT POSITION   ADVA0087
IF(NTRR,EQ,1) GO TO 405   ADVA0088
BNUP=ABS(AL(NTRR+1)+BL(NTRR+1)*RR-ZH),LT,,01   ADVA0089
1  AND1 TGR,LT,-BL(NTRR+1)   ADVA0090
GE TO 41          ADVA0091
405  BNUP=ABS(ZR),LT,,01,AND,TGR,LT,0,   ADVA0092
ILP=IDN#2   ADVA0093
IF(,NGT,BNUP) GO TO 411   ADVA0094
ILP#1   ADVA0095
IF(ABS(RNEW(1)),LT,ABS(RR+RNEW(2))) IUP#2   ADVA0096
IF(RNEW(IUP),LT,RR,EF,RNEW(ILP),GT,RMAX) IUP#0   ADVA0097
IF(,NGT,BNLW) GO TO 412   ADVA0098
IDN#3   ADVA0099
IF(ABS(RR+RNEW(3)),LT,ABS(RR+RNEW(4))) IDN#4   ADVA0100
IF(RNEW(IDN),LT,RR,EF,RNEW(IDN),GT,RMAX) IDN#0   ADVA0101
IF(ILP,GE,0) GO TO 414   ADVA0102
ILP#0   ADVA0103
RTRY=RMAX   ADVA0104
DE 413 I=1,2   ADVA0105
IF(RNEW(I),LT,RR,EF,RNEW(I),GT,RTRY) GO TO 413   ADVA0106
RTRY=RNEW(I)   ADVA0107
ILP#1   ADVA0108
413  CONTINUE   ADVA0109
414  IF(IDN,GE,0) GO TO 413   ADVA0110
IDN#0   ADVA0111

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RTRY=RMAX
GE 415 I=3,I4
IF(RMAX=(),LT,PH,ER,ENEN(),GT,RTRY) GE TO 415
IEN=1
RTRY=ENEN()
415 CONTINUE
416 IF((EN,EO,0)) GE TO 420
417 IF((UP,NE,U)) GE TO 418
418 ITRY=IDN
RTRY=ENEN(IDN)
GE TO 429
419 IF((RMAX=()|UP),GE,RMAX(1EN)) GE TO 417
420 ITRY=JUP
RTRY=ENEN(1UP)
GE TO 429
421 IF((UP,EO,0)) GE TO 50
422 GE TO 419
423 TGRPN=TA*(RPNEN(|TRY)-RPN)*TGRP
THAY=TRY+DELT(RPNE-(|TRY)=RPN,TGRP,TGRPN)
TGR=+TANSUM(TGRPN,-TANT)
RMAX=TRY
Z=2*EN*TRY.
C      CHECK FOR SURFACE AND BETTER HITS, TURNOVERS AND TURNUNDERS
IF(TGR=IGRN,GE,0,) GE TO 44
IF(TGR,GT,0,) GE TO 43
ACTRANCIR=ITR2
GE TO 44
43 ACTRANCIR=1
44 IF(|TRY,GT,2) GE TO 45
ACTRANCIR=1
IF(NTHR,GT,0,) GE TO 46
NTHR=1
SSR=SSR+SL
PHR=PHR+P1
ACTRANCIR=1
TGR=TGRN
GE TO 30
45 ACTRANCIR=1
IF(NTHR,LE,NTHR) GE TO 46
ACTRANCIR=1
ACTRANCIR=ITR3
TGRAZE=+TANSUM(TGRN,BL(NTR1))
S=100,*ABS(TGRAZE)+1,
N=S
S=SEN
IF(N,GT,199) N=199
SSR=SSR+((1,-S)*BMLT(N)+S*BRLT(N+1))
PHR=PHR+((1,-S)*BHST(N)+S*BPST(N+1))
TGR=+TANSUM(TGRAZE,BL(NTR1))
IF(TGR,LT,1,BL(NTR1)) 80,30
TGR=TGRN
GE TO 30
C      CALCULATE MAY INTERSECTION WITH VERTICAL BOUNDARY, RMAX
50 IF(ABS(ST),LT,2,E-4) GE TO 60
BV=+CT/ST
AV=(RMAX+H0)/ST
ADVA0112
ADVA0113
ADVA0114
ADVA0115
ADVA0116
ADVA0117
ADVA0118
ADVA0119
ADVA0120
ADVA0121
ADVA0122
ADVA0123
ADVA0124
ADVA0125
ADVA0126
ADVA0127
ADVA0128
ADVA0129
ADVA0130
ADVA0131
ADVA0132
ADVA0133
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ADVA0161
ADVA0162
ADVA0163
ADVA0164
ADVA0165
ADVA0166
ADVA0167

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C      CSAVE=RRP+ZRP
      F=F+ATURP
      IF(ABS(ALPHA),GT,1,E-25) GO TO 501
      C      LINEAR RAYS
      RPNE=(1-ZRP)*C/P
      RPNE=(2)=1,E100
      GE TO 505
      C      PARABOLIC RAYS
      501  DISC=P*P=4,*ALPHA*C
      IF(DISC,LT,0,) GO TO 80
      DISC=SQR(DISC)
      S#1,
      CG 503 I=1,2
      F=F+S*DISC
      CHP=F/T
      IF(ABS(F),LT,1,005(F)) ERF=(ALPHA*((ALPHA+DRP==2+C)/P)==2+C)/P
      RPNE=(1)=EHP+LAP
      503  S#=S
      506  DE =1 I=1,2
      ZRNE=(1)=ZRP*(RPNE(1)+RRP)*(TGRP+ALPHA*(RPNEW(1)+RRP))
      51    ZRNE=(1)=CT*ZPNEW(1)+ST*RPNE(1)+ZS
      I#2
      C      SELECT CORRECT INTERSECTION
      IF(ABS(ZRNE(1)-ZR),LT,ABS(ZRNE(2)-ZR)) I#1
      TGRPA=TA*(RPNEW(1)+RRP)*TGRP
      TRAY=TRAY+DEL(TRPNEN(1)-RRP,TGRP,TGRPA)
      TGRPA=TANSUM(TGRPA,+TAKT)
      C      CHECK FOR TURNOVERS AND TURNADERS
      52    IF(TGR,LT,0,) GO TO 54
      IF(TGR,LT,0,) GO TO 53
      NOTREACH#1
      DE TO 54
      53    NOTREACH#1,I#2
      54    TGAM(|RAY)|TGR
      IF(INTERHLE,1) DE TO 545
      C      CHECK THAT RAY IS WITHIN THE PROPER LIMITS
      IF(ZRNE(1),LT,AL(NTRR-1)*BL(NTRR-1)+RMAX,,1) DE TO 80
      545  IF(ZRNE(1),GT,AL(NTRR)+BL(NTRR)+RMAX,,1) DE TO 80
      C      THROG IN VOLUME ATTENUATION
      IF(IATT,LT,0) SSR=SER+10,0001*ATT*(TRAY*TIME(|RAY))/SQRT(C/S))ADVA0207
      55    SS(|RAY)=SSR
      ZZ(|RAY)=ZNE(1)
      TIME(|RAY)|TRAY
      COUNT(|RAY)=NCTR
      PHASE(|RAY)=PHR
      GE TO 100
      60    IFISTE6U
      C      ADD SMALL ER ZERO HORIZONTAL GRADIENTS, EQUATION FOR SECTION
      C      DO IS SINGULAR, THIS IS AN ITERATIVE SOLUTION FOR SUCH A CASE ADVA0215
      C      GUESS VALUE FOR ITERATION ADVA0216
      71A=ZH+IGH*(RMAX*RR)
      66    DE 67 I#1,7
      RPNE=CT*(RMAX-RD)*ST*(ZNA+ZD)
      CHP=RPNA-RRP
      TGRPAV=IGRP+ALPHA*ERF
      LZP=CHP*TGRPAV
      ADVA0217
      ADVA0218
      ADVA0219
      ADVA0220
      ADVA0221
      ADVA0222
      ADVA0223

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ZPNH=ZRH+CZR
ZNH2=GT*ZPNH+ST*RPA++ZC
C*ABS(ZN-ZNH)
IF(I,EO,3) DC=0
ZNH=ZNH2
      C
      CHECK FOR CONVERGENCE
IF(D,LT,1,01) GE TG 6E
IF(D,LT,1,5*DC) GG TG 6E
IHIST=3
GE TG 80
      68
RPNEN=(1)=RPNEN(2)*RPNH
GE TG 505
      C
      PRINT! ERROR MESSAGE
      80
SGRF0,
PRINT B1,IRAY,IHIST,FR,ZR,TGR
PRINT B2, RMAX,ZNEK(1),TGR
      666
FORMAT(* RAY*,15*,* IN LAYER*,15*, Z**,F10,2,* R**,F10,2,* TGR**,FACVA0240
1 10,5,* VCTR*,*,616)
      81
FORMAT(* RAY *,15*,* TERMINATED*,5X,*IHIST*,12,5X,*STARTING RANGE*FACVA0241
1*,F12,2,5X,*RAY DEPTH*,F12,2,5X,*STARTING TANGENT*,F12,6) FACVA0242
      82
FORMAT(DX,*MAXIMUM RANGE*,F12,2,5X,*NEW RAY DEPTH*,F10,2,5X,*FIN*FACVA0243
1AL TANGENT*,F12,6)
GE TG 55
      100
CONTINUE
RETURN
END
      ADVAC0224
      ADVAC0225
      ADVAC0226
      ADVAC0227
      ADVAC0228
      ADVAC0229
      ADVAC0230
      ADVAC0231
      ADVAC0232
      ADVAC0233
      ADVAC0234
      ADVAC0235
      ADVAC0236
      ADVAC0237
      ADVAC0238
      ADVAC0239
      ADVAC0240
      ADVAC0241
      ADVAC0242
      ADVAC0243
      ADVAC0244
      ADVAC0245
      ADVAC0246
      ADVAC0247
      ADVAC0248
      ADVAC0249

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DS	ADVANCE		06/04/73	ED	0
PROGRAM LENGTH		IDENT	ADVANCE		
ENTRY POINTS	ADVANCE	01720			
BLOCK NAMES		00125			
	TRIANG	02261			
	RAYS	13561			
	INFE	00024			
	PIECE	00003			
	MIRRORS	00621			
	ABC	00026			
EXTERNAL SYMBOLS					
	THEAD,				
	03210140				
	03000040				
	01C10100				
	01203100				
	02007111				
	082EICT,				
	SORTF				
	MAXIF				
	STH,				
	ONSINGL,				

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```

SUBROUTINE CHANNEL(ZR,T,ZTE,ZTU)
COMMON /VELPRF/ N,Z(100),C(100)
CALL VELCALC
20  D6 25 I#2,N
IF(ZR,GT,0) GO TO 25
I#0|
F=(ZR-Z(I+1))/(Z(I)-Z(I+1))
CH=SOR((I+T0T)*(F+C(I)*(1,-F)*C(I+1)))
GO TO 30
25  CONTINUE
ZTU=ZT00*I,
RETURN
30  IN#1|Z#1
IF(C([N],GT,CH) GO TO 35
IN#1|N#1
IF([N],NE,0) GO TO 31
ZT040,
GO TO 40
35  F=(CH+C([N+1]))/(C([N])-C([N+1]))
ZT0=F*(Z([N])*(1,-F)+Z([N+1])
40  IN#1|Z
IF(C([N],GT,CH) GO TO 45
IN#1|N#1
IF([N],LE,N) GO TO 41
ZT0Z([N])
RETURN
45  F=(CH+C([N+1]))/(C([N])-C([N+1]))
ZT0=F*(Z([N])*(1,-F)+Z([N+1])
RETURN
ENTRY RCALC
IF(ZT0,GT,1,E) GO TO 50
RCYCLE=1,E300
RETURN
50  IN#1
RCYCLE=0,
TG2#0,
D6 60 I#1,N
IF(Z(I),GT,A#0,Z(I),LT,ZTU) GO TO 55
IF([N],EQ,1) GO TO 56
RCYCLE=RCYCLE+(ZTU-Z(I+1))/(1.5*TG1)
RETURN
55  TG1=SGR1((CH/C(I))**2-1)
IF([I],EQ,1) GO TO 59
IF([N],EQ,1) GO TO 56
DR=(Z(I)-Z(I+1))/(1.5*(TG1+TG2))
GO TO 57
56  DR=(Z(I)-ZT0)/(1.5*TG1)
57  RCYCLE=RCYCLE+DR
TG2#TG1
IN#2
60  CONTINUE
RETURN
ENTRY WDENS
IF(RCYCLE,GT,1,E100) GO TO 71
IN#1|Z
IF(Z([N],GT,ZR) GO TO 70

```

CHAN0000  
CHAN0001  
CHAN0002  
CHAN0003  
CHAN0004  
CHAN0005  
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CHAN0050  
CHAN0051  
CHAN0052  
CHAN0053  
CHAN0054  
CHAN0055

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```
IF(Z(|N+1|,GT,ZR) GO TO 75  
IN=|N+1|  
IF(|N,GE,N) GO TO 71  
GO TO 69  
70 IF(Z(|N+1|,LE,ZR) GO TO 74  
IN=|N+1|  
IF(|N,GE,1) GO TO 65  
71 T=0,  
RETURN  
74 IN=|N+1|  
VOC(IN)*(C(|N+1|)*C(|N|))*(ZR-Z(|N|))/(Z(|N+1|)-Z(|N|))  
T=1,/(SURT((CM/V)**2+1.)*RCYCLE)  
RETURN  
END
```

CHAN0056  
CHAN0057  
CHAN0058  
CHAN0059  
CHAN0060  
CHAN0061  
CHAN0062  
CHAN0063  
CHAN0064  
CHAN0065  
CHAN0066  
CHAN0067  
CHAN0068  
CHAN0069

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S CHANNEL

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ED 0

	IDENT	CHANNEL
PROGRAM LENGTH	00506	
ENTRY POINTS	00003	
CHANNEL		
RCALC	00151	
MSEAS	00257	
BLOCK NAMES		
VELPRF	00311	
EXTERNAL SYMBOLS		
OBSDICT,		
VELCALC		
SORTF		

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SUBROUTINE VELCALC
CEMMEN /INFO/ CDDLE,RMAX,DCDCSD(18)
CEMMGA /VELPRF/ N,Z(100),C(100)
CEMMGA /THIANG/ AP(100,2),BP(100,2),AL(100),BL(100),ZZER0(100),
1 RZER0(100),AA(100),BB(100),SS1(100),CCT(100),NTR
CEMMGA /ABG/PUNCHD8 (16),INCR,NBRS,NSRS,ALIM,IFT,IFT1
DATA (RBLUP=1,E3CU),(IFT2=0),(IBW=0)
IF ((IFT1,EU,IFT2) GE TG 10
IEH=0
IFT2=F11
13 IF ((IFT1,E3,0,GR,IEH,EC,1) GE TG 3
RELD=.1,E300
IBW=1
3 IF(ABS(HMAX-RELD),LT,1,) GE TG 20
RELD=RMAX
N=NTR+1
GE 10 :E1,V
IF(I,E2,I) GE TG 1
J=I+1
ZZ=AL(J)+BL(J)+RMAX
GE TG 2
1 J#1
ZZ=0,
2 ZF=CCT(J)*(ZZ-ZZEHG(,))+SS1(J)*(RMAX=RZER0(J))
C(I)=1./SQR(AA(J)*BB(,)*ZF)
10 Z(I)=ZZ
20 RETURN
END

```

VELC	1
VELC	2
VELC	3
VELC	4
VELC	5
VELC	6
VELC	7
VELC	8
VELC	9
VELC	10
VELC	11
VELC	12
VELC	13
VELC	14
VELC	15
VELC	16
VELC	17
VELC	18
VELC	19
VELC	20
VELC	21
VELC	22
VELC	23
VELC	24
VELC	25
VELC	26
VELC	27
VELC	28

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DS VELCALC

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ED 0

PROGRAM LENGTH	IDENT	VELCALC
ENTRY POINTS	VELCALC	00132
BLOCK NAMES		00006
INF6		00024
VELPRF		00311
TPIANG		02261
ABC		00026

EXTERNAL SYMBOLS  
Q8CDICT,  
SRTF

UNCLASSIFIED

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      SUBROUTINE INTENSTY
C JUNE 14, 1971 LLOYD'S MIRROR ADDED FOR ALL RECEIVERS AND TYPES   INTE  1
C UNUSED SWITCH IFIMS IS NOW LLMR, 0 FOR NO LLOYD'S MIRROR, AND   INTE  3
C NON-ZERO FOR LLOYD'S MIRROR. THIS SWITCH IS THE COLUMN AFTER   INTE  4
C IPER ON THE INPUT CARDS   INTE  5
C 6/15/71 RECEIVERS BELOW BOTTOM FIXED   INTE  6
COMMON /LOUDNESS/ LNHC,ACD(100),TYPEIIS(100),TYPEIP(100),    INTE  7
1 TYPEIII(100),TYPEISP(100)   INTE  8
COMMON /TLE/STILE(10)   INTE  9
COMMON /RAYS/ NRAY,(GAM(1000)*ZZ(1000)*SS(1000)*TIME(1000)*   INTE 10
1 NCOUNT(1000)*PHASE(1000)   INTE 11
COMMON /INFO/ RESTART,RMAX,OMEGA,ATT,IPRAY,ITN,ITN2,ITN3,IRIG,   INTE 12
1 ISC,P,IT1,IT2,IT3,IER,LLMR,LTTR,LTER,LTRP,(PIN,IATT   INTE 13
COMMON /FIDEF/ PI,DTR,TWOP
COMMON /VELPRF/MN,Z6(100),C(100)   INTE 14
COMMON /THPSTR/ DDG(102)   INTE 15
DIMENSION QUAD(100),IMP(100),SINT(100,4),SSL(100),QUS(100),TYP(101)   INTE 16
10
EQUIVALENCE (QUAD,DDG)
COMMON /ABC/PJNCMD(116),INCR,N2RS,NSRS,ALIM,IFT,IFT1   INTE 17
DATA (IENT=0),(IFT2=0),(I6H=0),(IHP=100(0))   INTE 18
SEC(T)=FVA*SOPT(1,+TCT)   INTE 19
IF (IFT1.EQ.IFT2) GO TO 2 $ IBH=0 $ IFT2=IFT1   INTE 20
2 IF (IFT1.EQ.0.OR.IEH.EQ.1) GO TO 3 $ IENT=0 $ IBH=1   INTE 21
3 FVA=1.
IF (IAIT.EQ.0.AND.ATT.NE.0.) FVA=10.**(-.0001*ATT*RMAX)   INTE 22
CALL VELCALC SWAVE,WTWOP,C(1)/OMEGA SAK=TWOP/WAVEL $ FLH=1.   INTE 23
DO 5 I=1,LNRC   INTE 24
5 TYPEISC(I)=TYPEISP(I)=TYPEIT(I)=TYPEIII(I)=QUAD(I)=0.
IF (IT1.EQ.0.AND.IT2.EQ.0) GO TO 60   INTE 25
SW=0
SDZ=0.
DO 10 I=2,NRAY   INTE 26
#AMINI(SS(I),SS(I-1))   INTE 27
SDZ=SDZ+ABS(ZZ(I)-ZZ(I-1))   INTE 28
10 SW=SW+1   INTE 29
UZBAR=SDZ/SW   INTE 30
IF(DZHAR.LT.WAVEL) DZDAR=WAVEL   INTE 31
CALL CHANNEL(1..1000.,ZS,ZD)   INTE 32
DZM=ZB/SQRT(FLOAT(NRAY))   INTE 33
IF(UZBAR.GT.DZM) UZBAR=UZM   INTE 34
IF(IT1.EQ.0) GO TO 45   INTE 35
DO 20 I=1,NRAY   INTE 36
#MCOUNT(I)
M=N/ITN   INTE 37
NTO=N-4*ITN   INTE 38
NSR=M-4*ITN   INTE 39
M=N/ITN   INTE 40
NTU=N-4*ITN   INTE 41
NBR=M
IF(I.EQ.1) GO TO 19   INTE 42
NTUO=IABS(NTO-NTUO)+IABS(NTU-NTUO)   INTE 43
NOSBR=IABS(NSR-NSR0)+IABS(NBR-NBR0)   INTE 44
IO=ND$3R   INTE 45
ID=ID+NDTUO   INTE 46

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IF(IU.GT.3) ID=3          INTE 57
W=AMIN1(SS(I),SS(I-1))   INTE 58
IF(W.LE.ALIM,OR,NBR,GT,NSRS,OH,NSR,GT,NSRS) ID=3   INTE 59
NCOUNT(I)=NCOUNT(I)+IU*IRIG   INTE 60
19 NSR0=NSR   INTE 61
N8R0=N3R   INTE 62
NTU0=NTU   INTE 63
NTO0=NTO   INTE 64
CONTINUE      S DO 21 I=1,LNRC   INTE 65
SSL(I)=0.0   INTE 66
QUS(I)=0.0   INTE 67
TYPS(I)=0.0   INTE 68
21 IHP(I)=0 S IPRM=0   INTE 69
INW=NCOUNT(2)/IBIG   INTE 70
DC 30 I=2*NRAV   INTE 71
NCOUNT(I)=NCOUNT(I)-IOW*IBIG   INTE 72
INXT=NCOUNT(I+1)/IBIG S IF(I+2.LE.NRAY) INXTT=NCOUNT(I+2)/IBIG   INTE 73
IF(INW.GE.2) GO TO 29   INTE 74
I01=0 S I02=0 S I03=0   INTE 75
Z1=ZZ(I-1)   INTE 76
S1=SEC(TGAM(I-1))*SS(I-1)   INTE 77
DS=SEC(TGAM(I))*SS(I)-S1   INTE 78
T1=TIME(I-1)   INTE 79
DT=TIME(I)-T1   INTE 80
TG1=TGAM(I-1)   INTE 81
DTG=TGAM(I)-TG1   INTE 82
DZ=ZZ(I)-Z1   S DO 26 J=1,LNRC S I01=0 S I02=0 S I03=0   INTE 83
ZR=RCD(J) S IF(ZR.GT.46) GO TO 25   INTE 84
F=(ZR-Z1)/DZ S DZ1=ZZ(I+1)-ZZ(I) S F1=(ZR-ZZ(I))/DZ1   INTE 85
IF(F.LT.-0.5.OR.F.GT.1.5) GO TO 25   INTE 86
IF (INW.EQ.0.AND.F.LE.1.0.AND.F.GE.0..AND.IHP(J).EQ.0) 23,24   INTE 87
23 I01=1   INTE 88
GO TO 26   INTE 89
24 IF (F.GT.1.0.AND.INW.EQ.0 ..AND.INXT.NE.INW.AND.IHP(J).EQ.0) 31,32   INTE 90
31 I02=1   INTE 91
GO TO 26   INTE 92
32 IF (F.LT.0.0.AND.IPR.NE.INW.AND.INW.EQ.0) 33,34   INTE 93
33 I03=1   INTE 94
GO TO 26   INTE 95
34 I01=0 S I02=0 S I03=0   INTE 96
GO TO 25   INTE 97
26 SL=(S1+FD*DS)/(RMAX*ABS(DZ))   INTE 98
IF (SL.LE.0.0) GO TO 45 S IF (ABSF(DZ).LT.0.001) GO TO 25   INTE 99
TG=TG1+FD*DTG   S IF (I01.EQ.1) IH(J)=1   INTE 100
TH=DTR*ATANF(TG) S IF (INW.GE.1.AND.INXT.GE.1) GO TO 25   INTE 101
IF (LLMR.NE.0) FLM=2.*SIM((ZR*AK*TG/SQRT(1.+TG**2))**2)   INTE 102
T=T1+FD*DT   INTE 103
IF (I01.EQ.1.AND.SINT(J,. ZQ,0,0) SINT(J,4)=FLM   INTE 104
IF (I01.EQ.1.AND.SINT(J,. EQ,0,0) SINT(J,1)=SL   INTE 105
IF (I02.EQ.1.AND.SINT(J,. EQ,0,0) SINT(J,2)=SL   INTE 106
13).EQ,0,0) SINT(J,4)=FLM   INTE 107
IF (I02.EQ.1.AND.SINT(J,1).EQ,0,0.AND.SINT(J,2).EQ,0,0.AND.SINT(J,4).EQ,0,0) SINT(J,1)=FLM   INTE 108
13).EQ,0,0) SINT(J,2)=SL   INTE 109
IF (I03.EQ.1.AND.SINT(J,1).EQ,0,0.AND.SINT(J,2).EQ,0,0.AND.SINT(J,4).EQ,0,0) SINT(J,2)=FLM   INTE 110
13).EQ,0,0) SINT(J,1)=FLM   INTE 111
IF (I03.EQ.1.AND.SINT(J,1).EQ,0,0.AND.SINT(J,2).EQ,0,0.AND.SINT(J,4).EQ,0,0) SINT(J,1)=FLM   INTE 112

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13).EQ.0.0) SINT(J,3)=SL
IF(IPER.EQ.0) GO TO 28
IF (IENT.EQ.0) WRITE(LTER,1899),STITLE
IF (IENT.EQ.0) WRITE(49,1879),STITLE
1879 FORMAT (10AB)
1899 FORMAT (1H1** EIGENRAY SET      *10AB)
IF(IENT.EQ.0) WRITE(LTER,899)
PR=10.* ALOG10(SL)
N=NCOUNT(I)
IENS=1
M=N/ITN
NTO=N-4*ITN
NSR=M-4*ITN
M=N/ITN
NTU=N-4*ITN
NBR=M
IF (IQ3.EQ.1) IQUAL=3
IF (IQ2.EQ.1) IQUAL=2
IF (IQ1.EQ.1) IQUAL=1
IREM=2
IF (IQ3.EQ.1.AND.SINT(J,3).NE.0.0) IREM=2H*
IF (SINT(J,3).NE.0.0.AND.IQ1.EQ.1) IREM=2H**
WRITE(LTER,900) I,NBR,NTU,NSR,NTO,RMAX,ZR,TH,T,PR,IQUAL,IREM
RMKM=RMAX/1000.0
WRITE(49,1878) I,NBR,NTU,NSR,NTO,RMKM,ZR,TH,T,PR
1878 FORMAT (5I5,F10.4,F10.4,F15.5,F10.1)
899 FORMAT (*UNRAY NBR NTU NSR NTO,10X,*RANGE DEPTH THETA
1 T14E*, 9X,*SL(DB)*,5X,*IQUAL*,4X,*REM*)
900 FORMAT (5I5,F15.0,F10.4,F10.4,F13.5,F10.1,6X,IS,5X,A2)
22 FLM=SINT(J,4)
IF (SINT(J,1).NE.0.) SL=SINT(J,1)
IF (SINT(J,2).NE.0.*A D*SINT(J,1).EQ.0.0) SL=SINT(J,2)
IF (SINT(J,3).NE.0.*A D*SINT(J,1).EQ.0.0) SL=SINT(J,3)
IF (SINT(J,3).EQ.0.0) GO TO 27
IF (IQ1.EQ.1.AND.SINT(J,1).NE.0.0) 71,72
71 TYPEIRP(J)=SSL(J)
IF (ISCP.EQ.0) GO TO 27
TYPEISC(J)=TYP5(J)
QUAD(J)=QUS(J)
GO TO 27
72 SSL(J)=TYPEIRP(J)
27 TYPEIRP(J)=TYPEIRP(J)+SL*FLM
IF (ISCP.EQ.0) GO TO 29
PR=SQRT(SL)
P=OMEGA*T*PHASE/I)
IF (IQ3.EQ.1.AND.IQ1.EQ.0) QUS(J)=QUAD(J)
QUAD(J)=QUAD(J)+PR*SIN(P)
IF (IQ3.EQ.1.AND.IQ1.EQ.0) TYP5(J)=TYPEISC(J)
TYPEISC(J)=TYPEISC(J)+PR*COS(P)
25 IF (INXT.GE.1.OR.IPR.NE.INW.AND.INW.NE.INAT) IHP(J)=0
29 IPR=INW
INW=INXT
IF (INW.EQ.0.OR.INW.LT.1.AND.INXTT.LT.1) GO TO 30
DO 28 L=1,LNRC
SINT(LL,1)=0.0
INTE 113
INTE 114
INTE 115
INTE 116
INTE 117
INTE 118
INTE 119
INTE 120
INTE 121
INTE 122
INTE 123
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INTE 126
INTE 127
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INTE 159
INTE 160
INTE 161
INTE 162
INTE 163
INTE 164
INTE 165
INTE 166
INTE 167
INTE 168

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SINT(LL,2)=0.0          INTE 169
SINT(LL,3)=0.0          INTE 170
SINT(LL,4)=0.0          INTE 171
28 CONTINJE             INTE 172
30 DO 37 I=1,LNRC        INTE 173
35 TYPEISC(I)=TYPEISC(I)*Z*QUAD(I)**2   INTE 174
37 QUAD(I)=EXP(-RCD(I)/DZBAR)           INTE 175
IF(IT2.EQ.0) GO TO 60                 INTE 176
F=2.*RMAX*DZBAR                  INTE 177
EB=EXP(-ZB/DZBAR)                INTE 178
DO 50 I=1,NRAY                  INTE 179
IF(ABS(SS(I)).LT.AL(M)) GO TO 50    INTE 180
EZ=EXP(-ZZ(I)/DZBAR)            INTE 181
SL=SEC(TGAM(I))*SS(I)/F          INTE 182
SGK=TGAM(I)*AK/SQRT(1.+TGAM(I)**2) INTE 183
SL=SL/(1.-.5*(EB/EZ+EZ))       INTE 184
DO 40 J=1,LNRC                  INTE 185
IF(RCD(J).GT.ZB) GO TO 50       INTE 186
IF(QUAD(J))                   INTE 187
IF(LLMR.NE.0) FLM=Z*SIN(RCD(J)*SGK)**2 INTE 188
IF(ER.GT.EZ) GO TO 29          INTE 189
S=SL*ER/EZ                     INTE 190
GO TO 40                      INTE 191
S=SL*EZ/ER                     INTE 192
40 TYPEIII(J)=TYPEIII(J)+S*FLM      INTE 193
CONTINJE                       INTE 194
50 IF(IT3.EQ.0) RETURN          INTE 195
60 DO 70 I=1,NRAY              INTE 196
CALL CHANNEL(ZZ(I)+TGAM(I),ZTO,ZTU) INTE 197
CALL H CALC                     INTE 198
IF(LLMR.NE.0) CALL MDENS(ZZ(I),CTR)  INTE 199
SL=FVA*SS(I)/RMAX              INTE 200
DO 65 J=1,LNRC                  INTE 201
IF(RCD(J).GT.ZTU) GO TO 70      INTE 202
IF(HC(J).LT.ZTO) GO TO 65      INTE 203
CALL H DENS(RCD(J),5)          INTE 204
IF(LLMR.EQ.0) GO TO 64          INTE 205
TG=TGAM(I)*CTR/S              INTE 206
FLM=Z*SIN(AK*RCD(J)*TG/SQRT(1.+TG**2))**2 INTE 207
S=S*FLM                         INTE 208
64 TYPEIII(J)=TYPEIII(J)+S*SL      INTE 209
65 CONTINJE                      INTE 210
70 RETURN                         INTE 211
END                            INTE 212
                                INTE 213
                                INTE 214

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5.40S INTENSTY

01/02/75

ED 0

	IDENT	INTENSTY
PROGRAM LENGTH	03451	
ENTRY POINTS	01540	
BLOCK NAMES		
LOUDNESS	00765	
TLE	00012	
RAYS	13561	
INFO	00024	
PIDEF	00003	
VELPRF	00311	
TMPSTR	00266	
ABC	00026	
EXTERNAL SYMBOLS		
Q2007111		
THEND.		
Q800DICT.		
VELCALC		
CHANNEL		
RCALC		
W2ENS		
ALUG10		
SQRTF		
SINF		
MINIF		
EXPF		
COSF		
ATANF		
STH.		
SLO.		
QNSINGL.		

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14A

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SUBROUTINE ITAPRINT (NINT)
CMMEN /INFO/ RSTART,RMAX,?MEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,
1  ISCP,IT1,IT2,IT3,IPER,IFTIMS,LTRT,LTER,LTRP,LPIN,IATT
CMMEN /THPCPA/ DLE(182)
CMMEN /LIM1..1/ R1 (10), CR (10), R2 (10)
CMMEN /ABC/PURCHO$ (16),INCR,NBRS,NSRS,ALIM,IFT,IFT1
CMMEN /TLE/STITLE (10)
DATA (14H#1)
DIMENSION LINE(90),CE(4),FMT(6),AAL(400),IS(4),ABDDD(182)
EQUIVALENCE (LINE,CDC)
CMMEN /LBUDNESS/ LNRC,RCD(100),AL:100,4)
EQUIVALENCE (AL,AAL)
DATA (HA6#3HA7,), (FE#5HF7,1,), (B=1H ), (IS=1HS,1HR,1H2,1H3)
DATA (FMT(1)=6H(F8,3,), (FMT(6)=8H6X,90A1))
DIMENSION ITT(4)
EQUIVALENCE (ISCP,ITT)
DATA (IERTED),(IFT2=0),(IBH=0)
IF (IFT1,EG,IFT2) GE TE 3 $ IBH#0 $ IFT2=IFT1
3 IF (IFT2,EG,0,ER,IEH,EG,1) GE TE 2 $ INCR=1 $ IENT#0 $ HA6#3HA7, ITNP 19
HF6#5HF7/,1, 3 B=1P $ IS(1)=1HS $ IS(2)=1HR $ IS(3)=1H2 $ IS(4)=1H3 ITNP 20
FMT(1)=6H(F8,3,) $ FMT(6)=8H6X,90A1) $ IBH=1 ITNP 21
2 IF (INT(IEU,1) GB TE 40 $ AM#0, G DB 10 I#1,400 ITNP 22
IF (AA,(1),GT,AM) AFAAAL(1)
10 CONTINUE $ DEM#10,*ALEG10(AM)) $ DBL=DBM#90, ITNP 24
RKA,001#RMAX ITNP 25
ISK#0 ITNP 26
IF (IEN1,EG,0) WRITE (39,1) STITLE ITNP 27
IF (LNRC,GE,35) ISK#1 ITNP 28
WHITE (39,907),ISK,RK,EBL,EBW ITNP 29
DE 30 I#1,LNRC ITNP 30
DE 15 J#1,90 ITNP 31
15 LINE(j)=1H ITNP 32
DE 25 J#1,4 ITNP 33
IF (AL(I,J),LT,ALIM) GE TE 20 ITNP 34
FMT(j+1)=HF6 ITNP 35
DB(j)=10,*ALEG10(AL(I,j)) ITNP 36
IL=(DB(j)*DBL)+1,P ITNP 37
IF (IL,LE,0,ER,IL,GT,90) GB TE 25 ITNP 38
LINE(IL)=IS(j) ITNP 39
DE 25 ITNP 40
20 FMT(j+1)=HA6 ITNP 41
DE(j)=H ITNP 42
CONTINUE ITNP 43
30 WRITE (39,FMT) RCD(1),EB,LINE $ IENT#1 ITNP 44
RETURN ITNP 45
40 IF (IEN1,NE,0) GB TE 41 ITNP 46
WHITE (39,920),STITLE,LNRC,ITT(1),ITT(2),ITT(3),ITT(4)
1 FORMAT (1H1,10A8) ITNP 48
IF (IEN1,EG,0) WRITE (35,941) STITLE,(RCD(J),J#1,19) ITNP 50
941 FORMAT (10A8,//,10F8,3) ITNP 51
IF (IEN1,EG,0,AND,ITT(1),GT,0) WRITE (45,912) ,STITLE ITNP 52
912 FORMAT (* COHERENT PHASE VALUES*,//,10A8) ITNP 53
IF (IEN1,EG,0,AND,ITT(2),GT,0) WRITE (46,913),STITLE ITNP 54
913 FORMAT (* RANDOM PHASE VALUES*,//,10A8) ITNP 55
IF (IEN1,EG,0,AND,ITT(3),GT,0) WRITE (47,914),STITLE ITNP 56

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914 FFORMAT (• TYPE 2 VALUES•,/,10AB)
  IF (IEN,I,EQ,0,AND,ITT(4),GT,0) WRITE (48,915) ,STITLE
915 FFORMAT (• TYPE 3 VALUES•,/,10AB)
  IENT=1
  WRITE (39,905) (HCU(I),I=1,LNRC)
  WRITE (39,908)
900  FFORMAT (11•INTENSITIES AT•,F10,3,• KM, •//0 DEPTH ISC  IP
  1  II  II  •,F6,1,B4X,F6,1)
903  FFORMAT (•RECEIVED INTENSITY VS RANGE•,15X,•AT DEPTHS•/
  1  •0  H(KM)  TYPE •,13F9,3,/,19X,13F9,3)
908  FFORMAT (1X)
41   RK=RMAX/1000.
  IP=0
  SE 50 I=1,4
  IF (ITT(I),EQ,0) GE TE 50
  GE 45 J=1,LNRC
  DLD(J)=
  PLUNCHC(INCR)=ABSF(DED(J))
  ABDDD(J)=PLUNCHC(INCR)
  INCR=INCR+1
  IF (INCR,LT,17) GE TE 45
  INCR=1
  WRITE (39,909) (PLUNCHC(I),II=1,16)
45  CONTINUE
  IF (I,EQ,1,AND,ITT(1),GT,0) WRITE (45,911) (ABDDD(J),J=1,19)
  IF (I,EQ,2,AND,ITT(2),GT,0) WRITE (46,911) (ABDDD(J),J=1,19)
  IF (I,EQ,3,AND,ITT(3),GT,0) WRITE (47,911) (ABDDD(J),J=1,19)
  IF (I,EQ,4,AND,ITT(4),GT,0) WRITE (48,911) (ABDDD(J),J=1,19)
  IF (IP,EQ,0) GE TE 46
  WRITE (39,905) IS(I),(DDE(J),J=1,LNRC)
905  FFORMAT (16X,A1,2X,13F9,1,/,19X,13F9,1)
  GE TE 50
46  IP=1
  WRITE (39,907) RK,IS(I),(DDE(J),J=1,LNRC)
907  FFORMAT (19,3,7X,A1,2X,13F9,1,/,19X,13F9,1)
50  CONTINUE
909  FFORMAT ( 10F5,1)
911  FFORMAT (10F8,3)
920  FFORMAT (10AB,/,5IB)
  RETURN
END

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ITNP 97  
ITNP 98  
ITNP 99  
ITNP 60  
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ITNP 96  
ITNP 97

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S ITNPRINT

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	IDENT	ITNPRINT
PROGRAM LENGTH	01560	
ENTRY POINTS	ITNPRINT	00511
BLOCK NAMES		
INFG	00024	
TMPSTR	00266	
LIMITS	00036	
ABC	00026	
TLE	00012	
LBUCKNESS	00765	

## EXTERNAL SYMBOLS

THEND,  
01010100  
08C0CT,  
AL2G10  
MAXIF  
STH,  
SLB,  
ONSINGL,

UNCLASSIFIED

## B. G. ROBERTS

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```

SUBROUTINE IVSPRL6T(ITE)
COMMON /INFO/ RSTART,RMAX,EDEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,
1  ISCPI,IT1,IT2,IT3,IPEI,IFTIMS,LTRT,LTER,LTRP,LPIN,IATT
COMMON /LBUDDRESS/ LARC,KCD(100),AL(100,4)
COMMON /THPSHT/ DUE(182)
COMMON /TLE/STITLE (10)
COMMON /ABC/PLRCHD8 (16),INCR,ABRS,NSRS,ALIM,IFT,IFT1
DATA (IENT0),(IFT2=0),(IBH=0)
DIMENSION LINE(100)
EQUIVALENCE (LINE),ODE
IF (IFT1,E0,IFT2) GE TE 13
IBH=0
IFT2=IFT1
13 IF (IFT1,E0,0,ER, IBH,E0,1) GE TE 3
IENT=0
IBH=1
3 IF (IEN1,NE,0) GE TE 10
WHITE (38,1 ),STITLE
1 FORMAT (1H1,10A8)
IEN1=1
IT=ITE+1
IF (IT,LE,5) IT=1
GE 2 I=1,11
2 LINE(I)=170+10*I
N=M*0(LNHC,9)
WRITE(38,900) (RCL(I),I,I=1,N)
WRITE (38,901) (LINE(I),I=1,11)
GE 25 I=1,11
25 LINE(I)=1H+
WRITE (38,903) (LINE(I),I=1,11)
FORMAT(10*,15A,*RECEIVFD INTENSITY VS RANGE/*RECEIVER AT DEPTH PIVSR 31
1 LETS AS//((F1E,3,19))
901 FORMAT(*0 R(KM)*,5X,11I10)
903 FORMAT (14X ,11(9X,A1))
10 IF (IT,LE,0,89,IT,GT,4) RETRN
GE 15 I=1,105
15 LINE(I)=48
GE 20 I=1,N
DB=10,*ALG10(AMAX1(1,E+25,AL(I,IT)))
IP=161,5*DB
IF (IP,LE,0,89,IP,GT,105) GE TE 20
LINE(IP)=1
20 CONTINUE
PK=RMAX/1000.
WRITE(38,902) PK,LINE
902 FORMAT(19,3,14X,105H1)
RETRN
END

```

## NRL REPORT 7827

; IVSRPL8T

06/04/73

ED 0

I5EAT IVSRPL8T

PROGRAM LENGTH	00432
ENTRY POINTS	IVSRPL8T
BLOCK NAMES	00064
INFE	00024
LBLOCKSS	0C765
THPSTR	0C266
TLE	00012
ABC	0C026

## EXTERNAL SYMBOLS

THEEND,  
\$1510100  
\$88C1CT:  
ALEG10  
XMINCF  
MAX1F  
STH,  
SLE,  
ONSINGL,

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SUBROUTINE RAY PLET(NP,ZMAX)
CMMEN /INFO/ RESTART,RMAX,EPEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,
1 ISCP,IT1,IT2,IT3,IPER,IFT1MS,LTRT,LTER,LTRPLPIN,IATT
CMMEN /RAYS/ NRAY,TGAM(1000),ZZ(1000),SS(1000),TIME(1000),
1 NCOUNT(1000),PHASE(1000)
CMMEN /TMPSTR/ DGE(102)
CMMEN /ABC/PLACEDB (16),INCR,NBRS,NSRS,ALIM,IFT,IFT1
DIMENSION R(25),ISYM(25),LINE(115),INUM(9)
CMMEN /THANG/ AP(100,2),BP(100,2),AL(100),BL(100),ZZER0(100),
1 RZER0(100),AA(100),BB(100),SST(100),CCT(100),NTR
EQUIVALENCE (LINE,CDC)
DATA (ISYM=1H,A,1H,C,1H,D,1H,E,1H,F,1H,G,1HH,1H,I,1H,J,1H,K,1HL,1HM,1HN,1H0)RAYP 1
1 ,1HP,1H0,1H9,1HT,1HL,1HV,1HW,1HX,1HY,1HZ,1H*)RAYP 2
1 CMMEN /TLE/STITLE (10)RAYP 3
DATA (IENT#0),(IBLAK#1F ),(IB8#1HB),(IS#1HS),(IFT2#0),(IBH#0)RAYP 4
DATA (INUM#1H2,1H3,1H4,1H5,1H6,1H7,1H8,1H9,1H9)RAYP 5
IF (IFT1,0,0,IFT2) GE TE 2RAYP 6
IBH#0RAYP 7
IFT2#1RAYP 8
2 IF ((IFT1,0,0,SR,IEH,EC,1) GE TE 3RAYP 9
IENT#0 3 IBH#1RAYP 10
3 IF((IENT,0,0) GE TE 10RAYP 11
WRITE (LTRP,1),STITLERAYP 12
IENT#1RAYP 13
ANP=FLOAT(NRAY)/FLOAT(NP)RAYP 14
DE 5 (1,1,1)RAYP 15
A=ANP*(FLOAT(1)-,5)+1,RAYP 16
IR(1)=ARAYP 17
IF(IR(1),GT,1RAYP 18
CONTINUERAYP 19
SZ=ZMAX/114,RAYP 20
WRITE (LTRP,900) SZRAYP 21
10 ZB=AL(NIR)+BL(NTR)*RMAXRAYP 22
RKH#,001/ZMAXRAYP 23
IB=(ZMAX-ZB)/SZ+1,5RAYP 24
IB1#1RAYP 25
IF((IB,LE,0) GE TE 12RAYP 26
IF((IB,GT,115) ID#115RAYP 27
DE 11 IB1,IBRAYP 28
11 LINE(1)=IBRAYP 29
IB1#IB+1RAYP 30
12 DE 15 IB#IB1,114RAYP 31
15 LINE(1)=IBLNKRAYP 32
LINE(115)=ISRAYP 33
DE 20 IB#1,1PRAYP 34
K=IR(1)RAYP 35
IF (NSRS,0,2500,AND,NSRS,EC,2500) GE TE 17RAYP 36
NN=NCOUNT(K) SH=MN/ITN SNM=M/ITN SNSR=M>NN=ITN SHENN/ITN SNBR=HRAYP 37
17 IF(ABS(SS(K)),LT,ALIM,ER,NSR,GT,NSRS,OR,NSR,GT,NSRS) GE TE 20RAYP 38
ZR=ZZ(K)RAYP 39
IB=(ZMAX-ZR)/SZ+1,5RAYP 40
IF((IP,GT,115) IP#115RAYP 41
IF((IP,LE,0) GE TE 20RAYP 42
IF(LINE(IP),EQ,IBLAK,GR,LINE(IP),EQ,IS,OR,LINE(IP),EQ,1HR) GOT 19RAYP 43
DE 16 J#1,8RAYP 44
IF(LINE(IP),NE,INUM,) GE TE 16RAYP 45

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```
LINE({P})={NUM(J+1)
66 TO 20
16 CONTINUE
LINE({P})={NUM(1)
66 TO 20
19 LINE({P})={SYM(1)
20 CONTINUE
WRITE (LTHP,901) RKP,LINE
1 FORMAT (1H1,10A8)
900 FORMAT(27HOPLET OF RAY PATHS      SCALE,F8.2,2X,10HM/POSITION/
1   10HORANGE(XM),3X,114(1HX),1HS)
901 FORMAT(11,3,2X,115A1)
RETURN
END
```

RAYP	57
RAYP	58
RAYP	59
RAYP	60
RAYP	61
RAYP	62
RAYP	63
RAYP	64
RAYP	65
RAYP	66
RAYP	67
RAYP	68
RAYP	69
RAYP	70

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S RAYPLAT

06/04/73

ED 0

	IDENT	RAYPLAT
PROGRAM LENGTH	00605	
ENTRY POINTS	00145	
PLTCK NAMES		
LVE	00024	
HAYS	13561	
TMPSTR	00266	
ABC	00026	
THIANG	02261	
TLE	00012	

## EXTERNAL SYMBOLS

THEAD,  
0110100  
DICT,  
STA,  
SLG,  
2NSINGL,

## NRL REPORT 7827

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SUBROUTINE RAYQUIST (NP)
COMMON /RAYS/ ARAY,TGAM(1000),ZZ(1000),SS(1000),TIME(1000),
1 NCOUNT(1000),PHASE(1000)
COMMON /INFO/ RSTART,RMAX,EDEGA,ATT,IPRAY,ITN,ITN2,ITN3,IBIG,
1 ISCP,IT1,IT2,IT3,IPER,IFTIMS,LTRT,LTER,LTRP,LPIN,IATT
COMMON /THPSTR/ DDC(102)
COMMON /TLE/ STITLE(10)
DIMENSION LINE(71)
DIMENSION ISYM(25),IR(25)
COMMON /PIDEF/ PI,CTF,THEPI
EQUivalence (LINE,CDI)
COMMON /ARG/ PLACHD8(16),INCR,NBRS,NSRS,ALIM,IFT,IFT1
DATA (IENT=0),(IFT2=0),(IB4=0)
DATA (ISYM=1H,1HC,1HD,1HF,1HG,1HH,1HI,1HJ,1HK,1HL,1HM,1HN,1HZ)
1 ,1HP,1HQ,1HR,1HT,1HL,1HV,1H*,1HX,1HY,1HZ,1H*) GO TO 7
IF (IFT1,EU,IFT2) GO TO 7
IBH=0
IFT2=IFT1
7 IF (IFT1,EO,0,ER,IEH,EC,1) GO TO 6
IENT=0
IBH=1
6 IF (IENT,EO,1) GO TO 3
LTD=37
NP=FLOAT(NRAY)/FLOAT(NP)
DE 4 I=1,NP
AR=NP*(FLOAT(I)+1),
IR(I)=RA
IF (IR(I),GT,NRAY) IR(I)=RAY
CONTINUE
IENT=1
3 WRITE (LTD,2),STITLE
INC#1
1 CALL CHANNEL(1,,1000,,ZS,ZB)
DE 5 I=1,71
LINE()=1HX
RK=RMAX/1000,
SCALE=ZB/71,0
WRITE(LTD,900) RK,ZE,SCALE,LINE
DE 8 I=1,71
8 LINE()=1H
DE 40 I=1,NRAY
SS=SS()
IF (NBRS,EO,2500,AND,NERE,EC,250C) GO TO 35
N=NCOUNT()
N=N/ITN
N=M/ITN
N=H/ITN
N=V/ITN
NBR=M
35 IF (S,GT,ALIM,AND,NER,LE,NBRS,AND,NSR,LE,NSHS) GO TO 12
IF (I,EU, IR(INC))>10,15
10 WRITE (LTD,1901,ISYM(INC),I
INC=INC+1
DE TO 40
15 WRITE(LTD,901) I
500 FORMAT(26HCRAY DEPTH DISTRIBUTION AT,F10,4,4H KM,,10X,*BOTTM DEPTRAYZ 56

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1H*,F10,3,*,M*,1UX,SCALE=*,F10,3,* M/POSITION*,//,29H6LD NRAY RAYZ 57
2NBR NTU NSR NT6,3X,5HCEPHT,5X,5HTHETA,6X,4HTIME,1X,6HLPSES,1X,RAYZ 58
371A1)
901 FERMAT(4X,14,1CX,11HTEMINATED,)
1901 FERMAT(2X,A1,1X,14,10X,11HTERMINATED,)
GE TG 4U
12 FE=10,*ALOGIC(S)
T=TIME()
Z=ZZ()
N=ACELN(I())
M=N/ITN
NTG=N*M/ITN
N=M/ITN
NSH=M*N/ITN
P=N/ITN
NTU=N*M/ITN
NBR*M
LINE(1)=1HE
LINE(71)=1HS
CALL CHANNEL(Z,TGAM(I),ZT0,ZTL)
IZP=70,-(1,-ZTL/ZB)+1,5
IF (IZP,GT,71,ER,IZP,LT,1) GE TG 45
LINE([ZP]=1H*
45 IZM=70,-(1,-ZT0/ZB)+1,5
IF (IZM,GT,71,ER,IZM,LT,1) GE TG 55
LINE([ZM]=1H*
55 IZR=70,-(1,-ZTB/ZB)+1,5
IF (IZR,GT,71,ER,IZR,LT,1) GE TG 60
LINE([ZR]=1H*
60 TH=CTR=ATAN(TGAM(I))
IF (I,EG, IR(INC))20,25
20 WRITE (LTBD,902) ISYR(INC), I,NBR,NTU,NSR,NTB,Z,TH,T,DB,LINE
INC=INC+1
GE TG 3U
902 FERMAT(2X,A1,1X,515, FE,2,F10,5,F10,3,F7,1,1X,71A1)
25 WRITE (LTBD,1902) I,NBR,NTL,NSR,NTB,Z,TH,T,DB,LINE
RAYZ 91
1902 FERMAT(4X,515, FE,2,F10,5,F10,3,F7,1,1X,71A1)
30 IF (IZP,LE,71,AND,IZP,GE,1) LINE([ZP]=1H
IF (IZM,LE,71,AND,IZM,GE,1) LINE([ZM]=1H
IF (IZR,LE,71,AND,IZR,GE,1) LINE([ZR]=1H
40 CONTINUE
2 FERMAT (1H1,10AB,/)
RETURN
END

```

NRL REPORT 7827

DS RAYZDIST

06/04/73

ED 0

	IDENT	RAYZDIST
PROGRAM LENGTH	01'54	
ENTRY POINTS	RAYZDIST	00234
BLOCK NAMES		
PAYS	13561	
INFG	0CC24	
TMFSTR	0C266	
TLE	0CC12	
PICEF	0C003	
ABC	0CC26	

EXTERNAL SYMBOLS

C1C1010U  
THEAD,  
GCCICL,  
CHANNEL  
ALEG10  
ATANF  
STH,  
SLE,  
ONSINGL,

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06/04/73

SUBROUTINE BYEBYE  
DIMENSION LEAVE(1)  
J=1  
LEAVE(J)=6300000003000000  
END

BYBY	1
BYBY	2
BYBY	3
BYBY	4
BYBY	5

## NRL REPORT 7827

S BYEBYE

06/04/73

ED 0

PROGRAM LENGTH		00017
ENTRY POINTS	BYEBYE	00004
EXTERNAL SYMBOLS		
28C1CT,		

ICENT BYEBYE

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## IDS RECOVERY

PROGRAM LENGTH ENTRY POINTS	EVENT	RECOVERY	08/02/72	EN	O	PAGE NO.	I
DUMP RESTART	00125 00009 00051					00001	
	ASTATUS ST	MACHU STATUS	PI ((P1))				
	NDUP	0+47:ST				00002	
	NDUP	0+40:ST				00003	
	EDUM					00004	
						00005	
						00006	
						0000A	

TITLE -- DUMP AND RESTART FACILITY  
 IDENT NAME -- GENHNL-RECOVERY  
 IDENT NUMBER -- 00001400  
 LANGUAGE -- COMPASS 5.0  
 COMPUTER -- CDC 3800  
 C-L-TAT-AUTH -- ANNA HYUN MAYSS, CODE 7817.1  
 DOUGLAS P. SHANNON, CODE 7817.3  
 RESEARCH COMPUTATION CENTER  
 MATH, AND INFO. SCIENCES DIVISION  
 DATE -- JUNE 1970  
 PURPOSE -- ALLOWS PROGRAMS WITH A LONG RUN-TIME TO  
 HAVE A RESTART CAPABILITY

00008	
00009	
00010	
00011	
00012	
00013	
00014	
00015	
00016	
00017	
00018	
00019	
00020	
00021	
00022	
00023	
00024	
00025	
00026	
00027	

			DUMP/RESTART	
00017	WT1	E+07	15	ALWAYS INPUT TAPE, FIRST OUTPUT TAPE
00004	THRES	E+01	5+1	PARITY RE-TRY COUNTER
50000	LOCUME	E+01	500008	OCTAL NUMBER ON DEMAND CARU
00152	PARITY	E+01	47	PARITY STATUS BIT
00100	UNLCAUNT	E+01	*	1 IF UNLOAD TAPE AFTER USE. LAN SMITH
00000	F=1	E+01		

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DS	RECOVERY				08/02/72	EN	O	PAGE NO.	
00000	63 0 00000	DUMP	UJUP	ee					2
	00 0 77117								
00001	77 2 04000		UJTA	(0)SAVEAU	SAVE REGISTERS TO DUMP ON TAPE			00029	
	20 0 P00110								
00002	00 7 40053		HAT	DATA				00030	
	20 0 P00117		SIA	SAVED				00031	
00003	56 1 P00113		SIU	SAVE12,1				00032	
	57 2 P00113		SIL	SAVE12,2				00033	
00004	56 3 P00114		SIU	SAVE34,3				00034	
	57 4 P00114		SIL	SAVE34,4				00035	
00005	56 5 P00115		SIU	SAVE56,5				00036	
	57 6 P00115		SIL	SAVE56,6				00037	
00006	50 1 00017		ENI	MT1=1				00038	
	50 0 00000							00039	
00007		MOUT	FJDE	((0,1),0,BIN,L0)	MODE TAPE 200 BPI				
00008	50 6 00004		ENI	TRAILS,0	SET ME=THY COUNTER			00040	
	50 0 00000							00041	
00013		MEW=1	MEWNU	((0,1),0)					
00016		WHITE		((0,1),0,CWA=0)				00042	
00021		ASTATUS		((0,1),0)				00043	
00024	63 0 30052		ZHUP	Q,PARITY,CONT,1	JUMP IF NO PARITY ERNUN			00044	
	64 0 P00050							00045	
00026		MEWNU		((0,1),0)					
00032		HEAD		((0,1),0,SK[PCH,0])	MAKE SURF OF PARITY ERROR			00046	
00035		ASTATUS		((0,1),0)				00047	
00040	63 0 30052		ZHUP	Q,PARITY,CONT,1	JUMP IF NO PARITY ERNOK			00048	
	64 0 P00050							00049	
00041	55 6 P00013		IJP	REW+1,R					
	51 1 00001		ENI	1,1				00050	
00042		RELEASE		((=1,1),0)				00051	
00044	62 0 00022		MOUPINE	H1=M1=0,MODE	BAD TAPE --- THY ANOTHER UNIT			00052	
	30 1 P00007				JUMP IF NOT OVER TAPE UNIT LIMIT			00053	
00045	12 1 P00102		LUA	ERHOP=-T1=1+1	ABORT MESSAGE			00054	
	20 0 P00047		SIA	++1,1					
00046		ABORT		++	KILL JOH			00055	
00047		IPL		UNLOAD+T1,2				00056	
00048	62 0 00017	CONT,1	MOUPINE	81+H1=0,3	JUMP IF NOT FIRST TAPE			00057	
	30 1 P00045							00058	
00051		MEWNU		((0,1),0)	PERFORM FREQ REWIND			00059	
00054	52 1 P00113		ENI	UNLOADHT				00061	
	53 6 P00115		L1U	SAVE12,1	HELOAD USED INDEX REG.			00062	
00055	77 2 00000		L1L	SAVE56,6				00073	
	12 0 P00110		L1DA	SAVEAO	RESTORE A AND O			00074	
00056	75 0 PG0000		UJUP	DUMP	EXIT!			00075	
	50 0 00000							00076	

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605 -RECOVERY							04/02/72	EN	O	PAGE NO.	3
00047	00	V	00000	RESTART	UCT	0				0007A	
00048	00	0	00000							00079	
00049	77	1	00000		EIO	*				00080	
							TRIERS=0	REGISTERS NEED NOT BE SAVED		00081	
00051	50	0	00000		ENI		MJUE	SET ME-MV COUNTER		00082	
00052							MLOJNU	(M1,100,LO,WIN) SET MODE TO 200 BPI		00083	
00053							MTI=0			00084	
00054							MTI,RC=4,0	HEINCAHNAE CCNF		00085	
00055							MTI			00086	
00056							0,PARITY=CONT=2			00087	
00057	55	0	P00006		IUP		HEF=Z,M			00088	
00102	12	0	P00112	CONT=2	AD0H1		BAU HEAD	KILL JOB IF TAPE UNREADABLE		00089	
00103	00	7	00555		L0A		SAVED	REVITALIZE MACHINE REGISTERS		00090	
00104	77	2	00000		WAT		AU			00091	
00105	12	0	P00110		ULDA		SAVLAQ			00092	
00106	52	1	P00113		L1U		SAVE12,1			00093	
00107	52	2	P00113		L1L		SAVE12,2			00094	
00108	52	3	P00114		L1U		SAVE34,J			00095	
00109	52	4	P00114		L1L		SAVE34,S			00096	
00110	52	5	P00115		L1U		SAVE56,S			00097	
00111	52	6	P00115		L1L		SAVE56,B			00098	
00112	76	0	P00157	*	IPK		UNLOAD47,I			00099	
	50	0	00000		UJP		RESTART			00101	

## NRL REPORT 7827

S - RECOVERY

					DATE	EN	O	PAGE NO.	
00110		SAVEAU	025						4
00112		SAVEDU	025						
00113	00	V CUDOD	SAVE12	ULT	2				00103
00114	00	V 00000	SAVE12	ULT	1				00104
00115	00	V 00000	SAVE50	ULT	0				00105
00116	00	V 00000	SAVE50	ULT	0				00104
00117	00	V 00000	SAVE50	ULT	0				00107
00118	50	0 77777	MC-A	IUTW+C	(1)00000+77777H	ALL OF BANK ONE			
00119	00	1 00000		IUTW+C	MANK ZERO FROM LOAD HOUND TO RECOVERY = 1				00109
00120	10	0 00000		IUTW	77776H+LOAD HOUND,F=4-77776H+LOAD HOUND=1				00110
00121	00	C P00110		IUTW	(1)SAVEAU,A	SPACE FOR INDEX REGISTERS			00111
00122	20	0 77777	MC-A	EJU	EJU				00112
00123	00	0 77777	MC-A	IUSH	00,00				00113
00124	22	2 12466	EHWCW	ECU	1,04CWW 15				00114
00125	51	0 00107		ECU	1,04CWW 16				00115
00126	51	0 00108		ECU	1,04CWW 17				00116
00127	22	2 12466		IEN	UNLOADWT,I				00117
00128	51	0 00107		EVD					00118
00129									00121

## B. G. ROBERTS

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04/05/72

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PROGRAM THPLT          TPLT  1
C THIS VERSION IS COMPATIBLE WITH 4-5-72 VERSION OF TRIMAIN      TPLT  2
C   DISK VERSION OF THPLT                                         TPLT  3
C   IF INFO WILL FIT IN CORE DISK IS NOT OPENED                  TPLT  4
C   THIS DETERMINED BY NRMAX AND THE NUMBER OF RAYS TO PLOT       TPLT  5
C                                                               TPLT  6
C COMMON /INFO/ ID,NR,PRMAX,ZMAX,RSCALE,AL,RR(2000),ZB0T(2000),IKNM  TPLT  7
C DIMENSION TITLE(10),RUF(254),NRPL0T(512),ZR(1000),TR(1000),SS(1000)TPLT  8
1),NCAUNTS(1000)                                              TPLT  9
COMMON /1/ LSTER(16384)                                         TPLT 10
C6449N /2/ TSFER(16384)                                         TPLT 11
900 FORMAT(1CAR)                                                 TPLT 12
901 FFORMAT(28H1CALC8MM PL,DT FROM RAY TAPE ,10AB)             TPLT 13
902 FFORMAT(2F8.3,I4,6I5,F10.3)                                TPLT 14
903 FFORMAT(8HOLENGTH,F10.2,3X,1CHMAX DEPTH,F12.1,3X,14HN0, OF RECORD)TPLT 15
15,110,5X,=IFMC=,13,5X,=IFMC=,13,5X,=NFSK=,13,5X,=ITTR=,13,/,  TPLT 16
21X,=DB LIMIT=,F8.3,5X,=MAXIMUM NUMBER OF SURFACE REFLECTIONS=,  TPLT 17
31D,5X,=MAXIMUM NUMBER OF BOTTOM REFLECTIONS=,15)            TPLT 18
904 FFORMAT(20I4)                                                 TPLT 19
905 FFORMAT(5HUNRAY,20I5)                                         TPLT 20
906 FFORMAT(11HONG OF RAYS,10,3X,1DLENGTH OF BLOCK,10,3X,12HN0 OF BLOC)TPLT 21
1KS(16)                                                       TPLT 22
9039 FFORMAT(24HCPARITY ERROR IN RECORD ,16)                   TPLT 23
1LF9=U $ ICEEQ SREAD 4,ITNC SREWIND 1                         TPLT 24
4 FORMAT (12)
CALL PLOTS(BLK,254,10)                                         TPLT 25
2 READ Y02, AL,ZMAX,NRMAX,IKNM,IFMC,NFSK,ITTR,NSR1,NBR1,ALIM1
IF (EOF,60)2,
7 IL0=100+1
8 D0 3 J=1,NFSK
3 CALL SKIPFILE (1)
READ (1),TITLE,ALIM,NBRS,NSHS,ITNSIF(ITTR,LT,C)READ 900,TITLE
IF (ALIM1,NE.0.0,AND,ALIM1,GT,ALIM) ALIM=PWRF(10,0,(=4LIM1/10.0))TPLT 33
IF (ALIM1,EQ.0.0) ALIM1=-10.0*AL0G10(ALIM) $ PRINT 901,TITLE
IF (NSR1,NE.,0,AND,NSR1,LT,NSRS) NSHS=NSR1
IF (NBR1,NE.,0,AND,NBR1,LT,NBRS) NBRS=NBR1
PRINT 903,AL,ZMAX,NRMAX,IKNM,IFMC,NFSK,ITTR,ALIM1,NSRS,NBRS
IF (AL,LE.0.,OR,AL,GT,120.) STOP $ IF (ZMAX,LE.0.) STOP $ IL=1
IF (NRMAX,LE.,0,OR,PRMAX,GT,2000) STOP
5 IH=IL+19
IF (IH,GT,511) STOP
READ Y04,(NRPL0T(I),I=IL,IH)
PRINT 905,(NRPL0T(I),I=IL,IH)
IF (EOF,60) 10,15
10 IH=IL-1
11 GO TO 25
12 IF (NRPL0T(IH),EQ,0) GO TO 20
13 IL=IL+20
14 GO TO 5
15 IH=IH-1
16 IF (NRPL0T(IH),NE,0) GO TO 25
17 IF (IH,GT,0) GO TO 20
18 NCPLT=14
19 IF (IH,LE,0) STOP
20 LBK=32*(512/TPLT)
21 BLK=(NRMAX-1)/LBK+1

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PRINT 906,NTPLT,LBLK,MBLK
NDISK=MBLK+LBLK+NTPLT+2
IF(NDISK.GT,2+20) STOP
IF(MBLK.EQ.1,6R,1DF0.E0.1) GA T0 30
1DF0#1
CALL UKOPEN(2,3HAN,0)
    PLOT TITLE AND Z-AXIS
C   CALL SYMBOL(1.,0.,.14,TITLE,90.,,80)
30  CALL SYMBOL(2,8,9,93,.14,1MC,0,,1)
Z=0,
D6 31 I=1,10
CALL PLOT(3.,11,-1,3)
CALL PLOT(3.,10,-1,2)
CALL PLOT(3,05,10,-1,2)
CALL PLOT(2,95,10,-1,2)
Z=Z+ZMAX/10,
CALL NUMBER(2,32,9,93-I,.14,Z,0.,4HF5,F)
IF (I,EQ.5,AND,IFMC,GE.0) CALL SYMBOL (2.,4.5,.14,9HDEPTH (M),90.,,TPLT 74
19)
IF (I,EQ.5,AND,IFMC,LT.0) CALL SYMBOL (2.,4.5,.14,10HDEPTH (FT),,TPLT 76
190.,10)
31  CONTINUE
IF (IFMC,LT,0) ZMAX= ZMAX+0,3048
NR=NRMAX
M=1
IREC=0
32  D0 50 IR=1,LBLK
IREC=IREC+1 $ IFEF#0
READ(1) NRAY,RR(IREC),ZU3T(IREC),(TR(I)),I=1,NRAY),(ZR(I)),I=1,NRAY)TPLT 85
1,(SS(I),I=1,NRAY),(NCOUNT(I),I=1,NRAY)
IF(EOP,1) 36,38
30  IFEF#1
IF (NRMAX,LT,IREC-1) GA T0 52
NRMAX=IREC-1
NR=NRMAX
G6 T0 52
38  IF(10CHECK,1) 39,40
39  PRINT 9039,IREC
40  D6 45 I=1,NTPLT $ K=NRPLT(I) SJ=LBLK*(I-1)+IR $ ZSTOR(J)=ZR(K) TPLT 95
IF (NSRS.EQ,2200,AND,NSRS.EQ,2500) GA T6 41
NR=NCOUNT (K)$MM=MN/ITNSNSR=MM-NR+ITN $MM=MN/ITNENBR=MM TPLT 97
41  IF (ES(K),LE,ALIM,PH,NR,GE,NSRS,GR,NR,GE,NSRS) ZSTOR(J)=ZR(K) TPLT 98
IF (ZH(K).LT.0.0) ZSTOR(J)=ZR(K)
42  TSTOR(J)=ZR(K)
43  CONTINUE
50
51  IF(MBLK.EQ,1) G6 T0 60 $ IDEL=MBLK+LBLK
MBISK=(M-1)*LBLK
D6 55 I=1,NTPLT
CALL UKLOCATE("MDISK")
J=(I-1)*LBLK+1
K=J+LBLK-1
CALL UKWRITE(ZSTOR(J),TSTOR(K))
MDISK=MDISK+IDEL
CALL UKLOCATE("MDISK")
CALL UKWRITE(TSTOR(J),TSTOR(K))
52  MDISK=MDISK+IDEL

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60      IF(M,GR,NOLY,GR,1,IREF,LD,1) GO TO 65          TPLT 113
       M=M+1
       GO TO 35
65      NREC=J2*(I'RMAX-E3/32+1)                      TPLT 114
       RX=XR*(1.0)
       RSCALE=XAL/RMAX
       CALL PLGTRST
       IF(M'RMAX,EG,1) GO TO PU
       IL=1
       MLISK=0
       DO 70 I=1,NTPLT
       CALL DLKLOCATE(MLISK)
       CALL LKREAD(ZSTUR(1),ZSTUR(NREC))
       MLISK=MLISK+1
       CALL DLKLOCATE(MLISK)
       CALL LKREAD(TSTGR(1),TSTGR(NREC))
       MLISK=MLISK+1
       CALL KAYPLST(ZSTUR,TS1PR)
70      IL=IL
       GO TO 90
80      IL=1
       DO 85 I=1,NTPLT
       L=(I-1)*LBLK+1
       CALL KAYPLST(ZSTUR(L),TSTGR(L))
85      IL=IL
80      CALL PLST(AL+10.,0.,-3)
       IF(IREF,EG,1) GO TO 91  S  IREC=0
90      IREC=IPEC+1
       READ(1) XRAY,XR(IREC),ZB01(IPEC),(TR(I),I=1,NRAY),(ZR(I),I=1,NRAY)
       1,(RS(I),I=1,NRAY),(VC01NT(I),I=1,NRAY)
       IF(EUF,1) 91,92
91      IF(ILC.LT.ITAC) GO TO 2
       CALL STEPFLET
       STOP
       END

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TRIPLET

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ED 0

PROGRAM LENGTH	IDENT
ENTRY POINTS	TRIPLET
BLOCK NAMES	12/71
INFO	11432
1	47000
2	47000

IDENT TRIPLET

EXTERNAL SYMBOLS

CBCENTRY  
THEAD,  
CBCSTEPS  
C2C0700C  
C120310C  
CBCDICT,  
PLGTS  
SKIPFILE  
CKOPEN  
SYMBOL  
PLGT  
NUMBER  
CKLOCATE  
CKWHITE  
PLSTROT  
CKREAD  
RAYPLAT  
STEPPLAT  
ALRGIC  
PGWHF  
CBCIFEOF  
CBCIFIOC  
PE.,  
TSH.,  
TSE.,  
STH.,  
SLG.,  
SLT.,  
CNSINGL,

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SUBROUTINE PLOTBRT
C 449: /INFO/ ID,NR,RMAX,ZMAX,RSCALE,AL,PR(2000),ZBRT(2000),IKNM
      N14=AMINI(AL+1.,40.5)
      RI=1.
      RMA=RMAX
      IF (IKNM.LT.0) RMAN=RMAX/1.052
  50   N1=RMAX/RT
      IF (IT,LE,N1M) GO TO 51
      RI=2,0RT
      N1=RMAX/RT
      IF (NT,LT,N1M) GO TO 51
      RI=2,0RT
      N1=RMAX/RT
      IF (NT,LE,N1M) GO TO 51
      RI=2,0RT
      GO TO 56
C       PLOT SURFACE AXIS
  51   CALL PLGT(3.,10.,3)
      X=3.
      RSCALE1=PSCALE
      IF (IKNM.LT.0) RSCALE1=1.052*RSCALE
      DX=RT*RSCALE1
      RE=0.
      IR=0
  52   CALL PLGT(X,10.,2)
      CALL PLGT(X,9.95,2)
      RK=R/1000.
      CALL NUMBER(X-.24,10.05,1.4E-1,RK,0,,4WF4,0)
      IF (R,LT,RMAN/2.) GO TO 59
      IF (IF,EG,1) GO TO 59
      IF (IKNM.LT.0) CALL SYMBOL(X-.30,10.25,,14,10HRANGE (NM),0,,10)
      IF (IKNM.GE.0) CALL SYMBOL(X-.30,10.25,,14,10HRANGE (KM),0,,10)
      IF =1
  53   CALL PLGT(X,10.,3)
      IF (R,GE,RMAN) GO TO 60
      X=X+DX
      RE=RT
      GO TO 58
C       PLOT BOTTOMOUM CONTOUR
  54   DO 63 I=1,NR
      K=R+1-I
      Y=10.*((1,-ZBRT(K))/ZMAX)
      X=RP(K)*RSCALE+3.
      IP=2
      IF (I,EG,1) IP=3
      IF (Y,GE,0.) GO TO 63
      IP=3
      Y=0.
  55   CALL PLGT(X,Y,IP)
      RETURN
      END

```

TPLT 148  
TPLT 149  
TPLT 150  
TPLT 151  
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TPLT 197  
TPLT 198

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S PLETBET

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ED 0

	IDENT	PLOTBET
PROGRAM LENGTH	U0302	
ENTRY POINTS	PLETBET	U0010
BLOCK NAMES		
INFO	U7647	
EXTERNAL SYMBOLS		
C1010100		
CGCDICT,		
PLOT		
NUMBER		
SYMSL		
HIFIF		

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SUBROUTINE RAYPLAT(ZSIOM,ISTAR)
DIMENSION ZSTBR(2000),TSTBR(2000)
DIMENSION Z(25),R(25)
COMMON /INFB/ ID,NR,PRMAX,ZMAX,RSCALE,AL,RH(2000),ZB0*(2000),IKNM
NR=1 $ IBHEU $ IPHEU $ IHTEU $ TRIE0 $ ISTE0 $ IJ1*0
IF (ID,LT,0) NR=NR + 1F (NID,NE,1) IPR=1
ZG=AHSF(ZSTBR(1))
IF (ZSTBR(1).LT,0.0) RETURN
TG=TSTBR(NID)
RR=RR(NID)
ZB0=ZB0(NID)
X=R0*RSCALE + IF (ZB,GT,1.0) ZB=ZB0
Y=10.0*(1.-ZB/ZMAX)
IF (Y,LT,0.) Y=0.
CALL PLAT(X,Y,Z)
D9 99 LL=2,NR
IF (ID,GT,0) GO TO 75
L=N+R+LL+1
GO TO 74
74 L=LL
ZM=AHSF(ZSTBR(L)), TN=TSTBR(L), SRN=RR(L), SZBN=ZB0(L),RN=RR-R0
IF (ZM,GT,ZBN) ZM=ZBN + IF (ZSTBR(L),LT,0.0) AND.IPR,EO-1) 91,93
93 IF (NID,NE,1) AND.IRH,EO,0) 94,95
94 X=R0*RSCALE Y=10.0*(1.-ZB/ZMAX) $ IF (Y,LT,0.) Y=0.0
CALL PLAT(X,Y,Z) + IBHE1$[PR=0$IPR=1$[IF (ZSTBR(L+1),GE,0.)]IST=1]TPLT 222
95 ZN=ZL+DF-TV
ZG=ZG+DF+TG
IF (ZN,GE,0.) GO TO 75
IF (ZB,GE,0.) GO TO 75
ZB=-ZB
ZG=-ZG
TG=+TG
T9=(ZB-ZG)/DR
IF (ZB,LE,ZG) GO TO 79
IF (ZB,LE,ZBN) GO TO 79
IF (TG,EO,0.) GO TO 76
D9=ZB-ZG
ZG=ZG+DF+TG
TG=+TG
T9=(TG-TG)/(1.+TG+TG)
TG=(TG-TG)/(1.+TG+TG)
GO TO 77
76 ZG=2.0*TB3-ZB
TG=+TG
77 DR=RN-R0
ZG=ZG+DF+TG
ZB=ZB+DR+TN
78 DX=AHS(D+RSCALE)
Y=DX,02*2.
C     INTERPOLATION TO FIFTIETHS WILL BE DONE
IF (N,LT,25) N=25
I=1
DR=1./(N-1)
F=0.
C     SPLINE FIT BY CONTINUOUS LINEAR INTERPOLATION
DZ=ZB-ZB
DZ=DZ-N/6
TPLT 199
TPLT 200
TPLT 201
TPLT 202
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TPLT 254

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74      D7=ZB-ZNB          TPLT 255
      Z1=ZB+F+BI          TPLT 256
      ZB=ZB+F+DZB          TPLT 257
      ZD=ZNB+F+DZN          TPLT 258
      G=1,-F              TPLT 259
      Z4=G+Z2+F+Z1          TPLT 260
      Z2=G+Z1+F+Z3          TPLT 261
      Z(I)=G+Z4+F+Z5          TPLT 262
      R(I)=H0+F+DR          TPLT 263
      I1=I1+1              TPLT 264
      F=F+DF              TPLT 265
      IF(I1,LE,N) GO TO 79          TPLT 266
      DE 89 I1=1,N          TPLT 267
      IN=0                  TPLT 268
      IF(Z(I),LT,0.) IN=1          TPLT 269
      IF(Z(I),GT,ZBN+(R(I))-RN)+TB) I1=-1          TPLT 270
      IF(I1,EQ,-1) GO TO 82          TPLT 271
      IF(I1,NE,0) GO TO 82          TPLT 272
      IF(I1,NE,1,AND,IF,NE,1) GO TO 80          TPLT 273
      RHIT=,D*(R(I))+R(I-1)*(R(I)-R(I-1))*(Z(I)+Z(I-1))/(Z(I-1)-Z(I))          TPLT 274
      TPLT 275
      1II))
      X=RHIT*RSCALE$IF#3$IF (IBT,EG,1,SH,NID,EG,1,ER,IST,EG,1)IP=2$IRT=1TPLT 276
      CALL PLOT(X*3.,+16.,IP)$ IF (ZSTOP(L),GE,0,0) GO TO 82 $ IPR#1          TPLT 277
      GO TO 91              TPLT 278
      36      D=(Z(I)-Z(I-1))/(R(I)-R(I-1))-TB          TPLT 279
      RHIT=(Z(I)-ZB-(R(I)-RN)+TB)/D+R(I-1)          TPLT 280
      F=(RHIT-R(I-1))/R(I)-R(I-1)          TPLT 281
      IF(F,GT,1,) GO TO 82          TPLT 282
      IF(F,LT,0,) GO TO 82          TPLT 283
      X=RHIT*RSCALE$IP=3$IF(IBM,EG,1,ER,NID,EG,1,ER,IST,EG,1)IP=2          TPLT 284
      IBT=1                  TPLT 285
      Y=10.*{1.-(ZBN+(RHIT-RN)+TB)/ZMAX}$IF(ZSTOP(L),LT,0,0) IPR=1          TPLT 286
      IF(Y,GT,0,) GO TO 81          TPLT 287
      Y=C.                  TPLT 288
      IP=3                  TPLT 289
      81      CALL PLOT(X*3.,Y,IP)          TPLT 290
      82      IF(Z(I),GT,0.) GO TO 83          TPLT 291
      Y=10.*{1.+Z(I)/ZMAX}          TPLT 292
      X=R(I)*RSCALE$IF (Z(I),EG,0,0,AND,IP1,EG,1) IJT=1          TPLT 293
      IF (Z(I),EG,0,0,AND,ZSTOP(L),LT,0,0) IPR#1 $ GO TO 85          TPLT 294
      IF (Z(I),GT,ZB+(R(I)-RN)+TB) GO TO 84          TPLT 295
      Y=10.*{1.-Z(I)/ZMAX}$IF(Z(I),EG,ZBN+(R(I)-RN)+TB,AND,ZSTOP(L),LT)          TPLT 296
      1T,a,b) IPR#1          TPLT 297
      X=R(I)*RSCALE$IF (Z(I),EG,ZBN+(R(I)-RN)+TB,AND,IP1,EG,1) IJT=1          TPLT 298
      GO TO 86              TPLT 299
      84      DZ=Z(I)-(ZBN+(R(I)-RN)+TB)          TPLT 300
      ZP=Z(I)-Z.+DZ/(1.+TB**2) $ R'=R(I)          TPLT 301
      IF(TB,NE,0,) RP=RP+2.*DZ/(TB+1./TB) $ Y=10.*{1.-ZP/ZMAX}          TPLT 302
      IF(ZP,EG,ZBN+(RP-RN)+IP,AND,ZSTOP(L),LT,0,0)IPR#1          TPLT 303
      IF(ZP,EG,ZBN+(RP-RN)+IP,AND,IH1,EG,1) IJT=1 $ X=RP*RSCALE          TPLT 304
      IF(IBM,EG,1,AND,NID,NE,1,SH,IST,EG,1) GO TO 86          TPLT 305
      IF(NID,NE,1) GO TO 187          TPLT 306
      IF(IPR,EG,1,ER,ZSTOP(L),GE,0,0) GO TO 86          TPLT 307
      187 IF (I,EG,4) GO TO 186          TPLT 308
      DZS=Z(I+1)-(ZB+(R(I+1)-RN)+TB)          TPLT 309
      ZPS=Z(I+1)-2.*DZS/(1.+TB**2)          TPLT 310

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IF (ZP,GE,ZPS,AND,NID,FQ,1,0R,DZS,LE,0,0,AND,NID,EQ,1) IPR#1      TPLT 311
IF (ZP,GE,ZPS,AND,NID,NE,1,0R,DZS,LE,0,0,AND,NID,NE,1) IJT#1      TPLT 312
G0 T0 86
186 IF (IPR,EQ,0,AND,LSTEP(L),LT,0,0) IPR#1      TPLT 313
IF (IBT,EQ,0,AND,LSTEP(L+1),LT,0,0,AND,NID,NE,1) IJT#1      TPLT 314
89 IP#2
IF (Y,LT,10.,AND,Y,GT,0.) G0 T0 87      TPLT 315
IP#3
Y=A MINI(10.,AMAX1(Y,0.))      TPLT 316
87 IF (X,LT,AL+1.,AND,X,GE,-.01) G0 T0 88      TPLT 317
IP#3
X=A MINI(AL+1.,AMAX1(X,0.))      TPLT 318
88 IF (IBT,EG,0,AND,IRI,EQ,1,AND,IST,EQ,0)IP#3 S CALL PLOT(X+3.,Y,IP)TPLT 323
18=IN S IF(IJT,EQ,1) IBT#1 S IF (!IPR,EQ,1) G0 T0 91      TPLT 324
CONTINUE      TPLT 325
91 ZB3=ZBN S Z0=ZN      TPLT 326
T0=TN
80 R0=RN
RETURN
END
TPLT 327
TPLT 328
TPLT 329
TPLT 330
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S RAYPLOT

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IDENT RAYPLOT

PROGRAM LENGTH	01371
ENTRY POINTS	RAYPLOT
BLOCK NAMES	00062
INFO	07641

## EXTERNAL SYMBOLS

C1C10100
20001CT,
PLST
MINF
MAXIF

## Appendix B

### COMPARISON OF CALCULATED AND EXPERIMENTAL RESULTS

A comparison was made between the calculated results from TRIMAIN and some experimental data which was furnished by Cdr. P.R. Tatro of the Maury Center for Ocean Science. The input parameters for TRIMAIN were: a frequency of 100 hertz and no volume attenuation, a fan of rays between  $\pm 60^\circ$  in  $1^\circ$  steps, a bottom loss of MGS class IV for the entire track, type II intensity calculations, a source depth of 152.4 meters and a receiver depth of 762.0 meters. Figs. B1a, B1b, and B1c are print plots of input sound-speed profiles, Fig. B2 is a Calcomp plot of profiles and the bottom track, Fig. B3a is a list of calculated intensity values, Fig. B3b is a list of experimental intensity values, Fig. B4 is a Calcomp plot of selected rays which were traced (one ray every  $15^\circ$ ), and Fig. B5 is a Calcomp comparison of experimental and calculated intensity values. Good agreement exists between the two sets of values.

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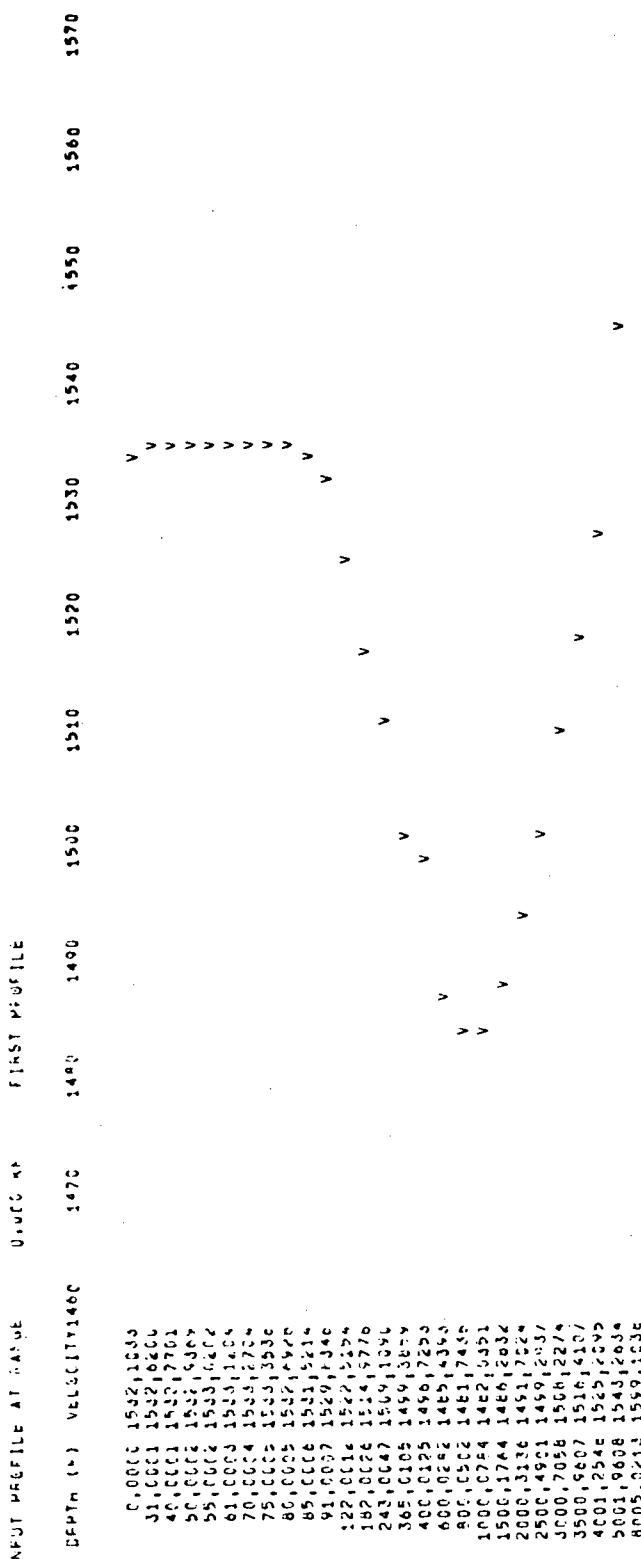


Fig. B1a — Input profile at 0 km

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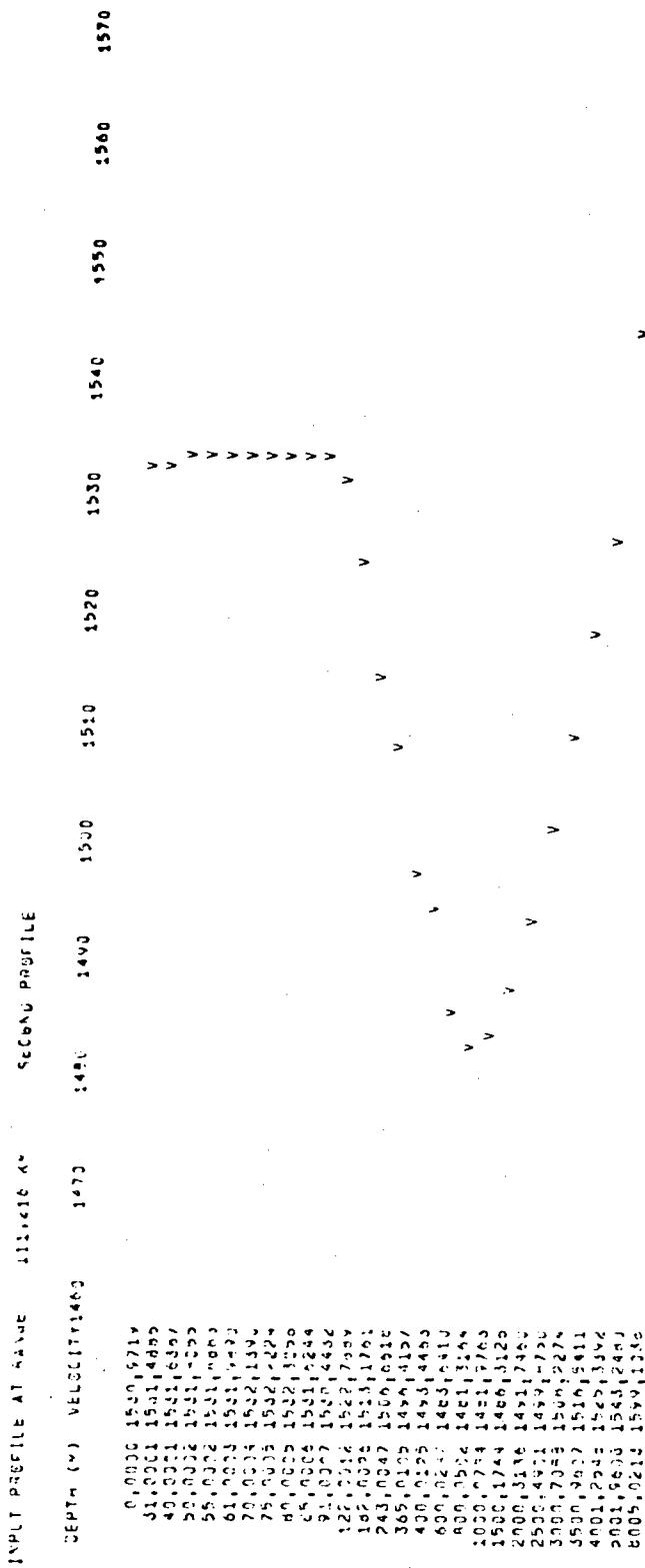


Fig. B1b — Input profile at 111.216 km

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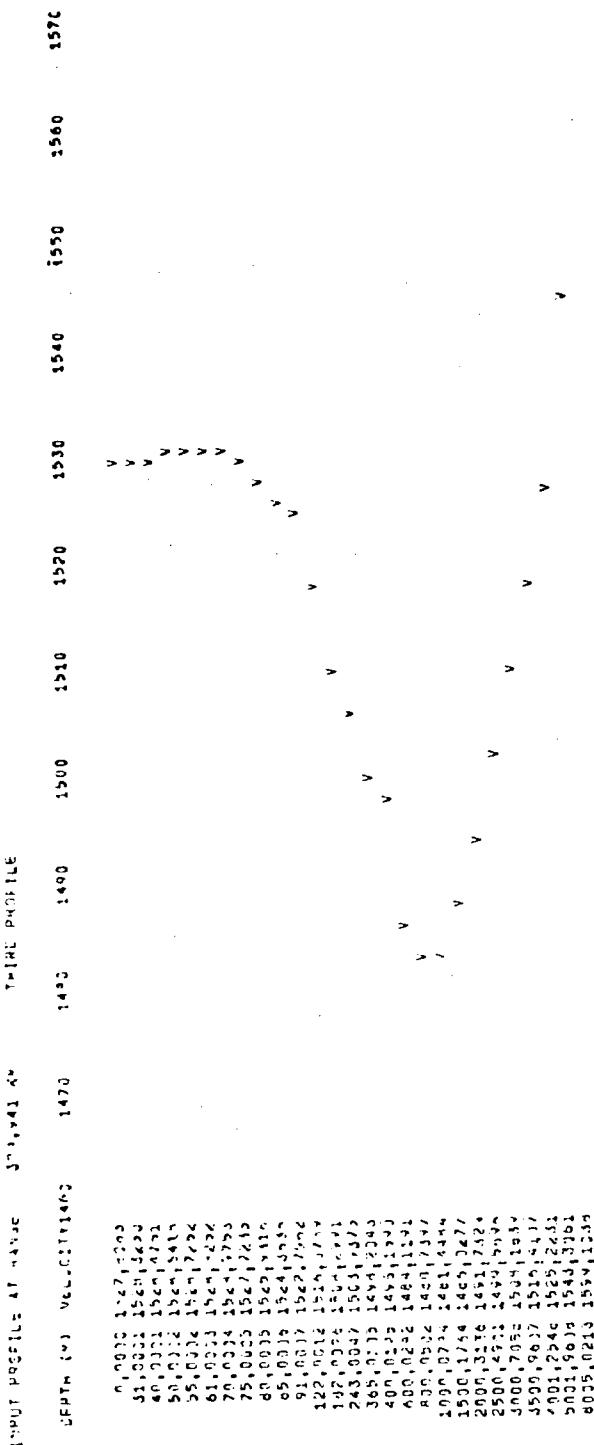


Fig. E1c—Input Profile at 329.941 km

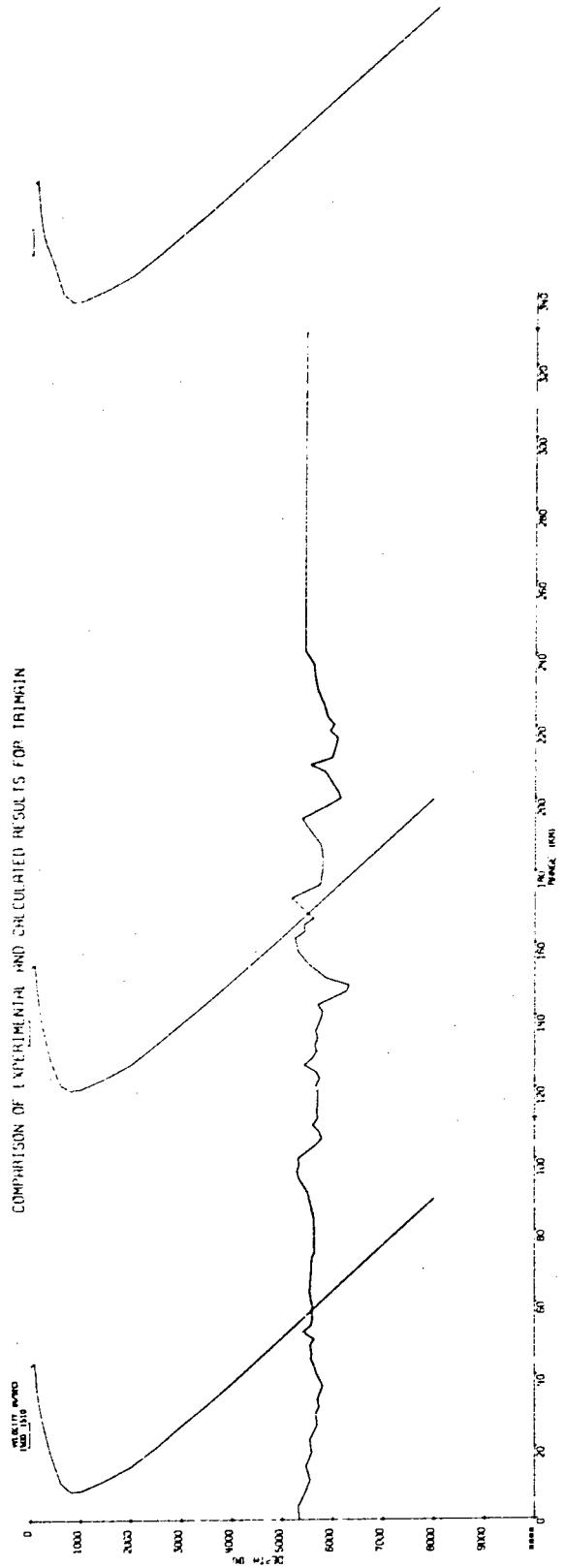


Fig. B2 — Profiles and Bottom Track

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RANGE CALCULATED RESULTS	LINES	61,700		62,400		126,700		91,100		192,000		94,700		258,400		144,700	
		61,700	62,400	62,400	62,400	126,700	126,700	91,100	91,100	192,000	192,000	94,700	94,700	258,400	258,400	144,700	144,700
1,700	68,400	67,700	69,000	132,000	99,300	63,400	127,700	92,300	193,000	160,300	102,400	102,400	260,000	260,000	145,100	145,100	
2,000	67,400	68,700	69,000	134,000	99,300	64,400	128,700	93,300	194,000	161,300	103,400	103,400	261,000	261,000	144,500	144,500	
2,300	66,400	65,700	62,000	135,000	99,300	65,400	129,700	94,300	195,000	162,300	104,400	104,400	262,000	262,000	143,300	143,300	
2,600	65,500	70,400	92,000	134,000	99,300	66,400	130,700	95,300	196,000	163,300	105,400	105,400	263,000	263,000	142,300	142,300	
2,900	69,700	71,400	62,400	137,000	99,300	67,400	131,700	96,300	197,000	164,300	106,400	106,400	264,000	264,000	141,300	141,300	
3,200	70,400	72,700	92,000	138,000	99,300	68,400	132,700	97,300	198,000	165,300	107,400	107,400	265,000	265,000	140,500	140,500	
3,500	67,200	73,700	92,000	135,000	99,300	69,400	133,700	98,300	199,000	166,300	108,400	108,400	266,000	266,000	139,500	139,500	
3,800	65,500	74,400	62,400	140,000	99,300	70,400	134,700	99,300	200,000	167,300	109,400	109,400	267,000	267,000	138,500	138,500	
4,100	63,400	68,700	94,000	141,000	99,300	71,400	135,700	100,300	201,000	168,300	110,400	110,400	268,000	268,000	137,500	137,500	
4,400	67,100	72,700	93,500	142,000	99,300	72,400	136,700	101,300	202,000	169,300	111,400	111,400	269,000	269,000	136,500	136,500	
4,700	67,100	73,700	94,000	143,000	99,300	73,400	137,700	102,300	203,000	170,300	112,400	112,400	270,000	270,000	135,500	135,500	
5,000	67,400	75,400	93,500	145,000	99,300	74,400	138,700	103,300	204,000	171,300	113,400	113,400	271,000	271,000	134,500	134,500	
5,300	67,200	80,700	65,100	144,000	99,300	75,400	139,700	104,300	205,000	172,300	114,400	114,400	272,000	272,000	133,500	133,500	
5,600	67,400	81,700	95,000	147,000	99,300	76,400	140,700	105,300	206,000	173,300	115,400	115,400	273,000	273,000	132,500	132,500	
5,900	67,500	82,700	94,500	148,000	99,300	77,400	141,700	106,300	207,000	174,300	116,400	116,400	274,000	274,000	131,500	131,500	
6,200	67,700	83,700	95,000	149,000	99,300	78,400	142,700	107,300	208,000	175,300	117,400	117,400	275,000	275,000	130,500	130,500	
6,500	67,400	85,400	95,500	150,000	99,300	79,400	143,700	108,300	209,000	176,300	118,400	118,400	276,000	276,000	129,500	129,500	
6,800	67,700	86,700	96,000	151,000	99,300	80,400	144,700	109,300	210,000	177,300	119,400	119,400	277,000	277,000	128,500	128,500	
7,100	66,100	87,700	103,000	152,000	99,300	81,400	145,700	110,300	211,000	178,300	120,400	120,400	278,000	278,000	127,500	127,500	
7,400	66,200	88,700	103,500	153,000	99,300	82,400	146,700	111,300	212,000	179,300	121,400	121,400	279,000	279,000	126,500	126,500	
7,700	66,400	89,700	104,000	154,000	99,300	83,400	147,700	112,300	213,000	180,300	122,400	122,400	280,000	280,000	125,500	125,500	
8,000	66,700	90,700	104,500	155,000	99,300	84,400	148,700	113,300	214,000	181,300	123,400	123,400	281,000	281,000	124,500	124,500	
8,300	67,100	91,700	105,000	156,000	99,300	85,400	149,700	114,300	215,000	182,000	124,400	124,400	282,000	282,000	123,500	123,500	
8,600	66,500	92,400	105,500	157,000	99,300	86,400	150,700	115,300	216,000	183,000	125,400	125,400	283,000	283,000	122,500	122,500	
8,900	67,500	93,700	106,000	158,000	99,300	87,400	151,700	116,300	217,000	184,000	126,400	126,400	284,000	284,000	121,500	121,500	
9,200	66,700	94,700	106,500	159,000	99,300	88,400	152,700	117,300	218,000	185,000	127,400	127,400	285,000	285,000	120,500	120,500	
9,500	67,100	95,700	107,000	160,000	99,300	89,400	153,700	118,300	219,000	186,000	128,400	128,400	286,000	286,000	119,500	119,500	
9,800	66,400	96,400	107,500	161,000	99,300	90,400	154,700	119,300	220,000	187,000	129,400	129,400	287,000	287,000	118,500	118,500	
10,100	66,200	97,100	108,000	162,000	99,300	91,400	155,700	120,300	221,000	188,000	130,400	130,400	288,000	288,000	117,500	117,500	
10,400	66,700	97,700	108,500	163,000	99,300	92,400	156,700	121,300	222,000	189,000	131,400	131,400	289,000	289,000	116,500	116,500	
10,700	66,400	98,400	109,000	164,000	99,300	93,400	157,700	122,300	223,000	190,000	132,400	132,400	290,000	290,000	115,500	115,500	
11,000	66,700	99,100	109,500	165,000	99,300	94,400	158,700	123,300	224,000	191,000	133,400	133,400	291,000	291,000	114,500	114,500	
11,300	67,200	100,700	110,000	166,000	99,300	95,400	159,700	124,300	225,000	192,000	134,400	134,400	292,000	292,000	113,500	113,500	
11,600	67,500	101,400	110,500	167,000	99,300	96,400	160,700	125,300	226,000	193,000	135,400	135,400	293,000	293,000	112,500	112,500	
11,900	68,100	102,100	101,000	168,000	99,300	97,400	161,700	126,300	227,000	194,000	136,400	136,400	294,000	294,000	111,500	111,500	
12,200	67,700	102,700	101,500	169,000	99,300	98,400	162,700	127,300	228,000	195,000	137,400	137,400	295,000	295,000	110,500	110,500	
12,500	68,400	103,400	102,000	170,000	99,300	99,400	163,700	128,300	229,000	196,000	138,400	138,400	296,000	296,000	109,500	109,500	
12,800	67,100	104,100	102,500	171,000	99,300	100,400	164,700	129,300	230,000	197,000	139,400	139,400	297,000	297,000	108,500	108,500	
13,100	66,400	104,700	103,000	172,000	99,300	101,400	165,700	130,300	231,000	198,000	140,400	140,400	298,000	298,000	107,500	107,500	
13,400	67,100	105,400	103,500	173,000	99,300	102,400	166,700	131,300	232,000	199,000	141,400	141,400	299,000	299,000	106,500	106,500	
13,700	66,700	106,100	104,000	174,000	99,300	103,400	167,700	132,300	233,000	200,000	142,400	142,400	300,000	300,000	105,500	105,500	
14,000	67,400	106,700	104,500	175,000	99,300	104,400	168,700	133,300	234,000	201,000	143,400	143,400	301,000	301,000	104,500	104,500	
14,300	67,100	107,300	105,000	176,000	99,300	105,400	169,700	134,300	235,000	202,000	144,400	144,400	302,000	302,000	103,500	103,500	
14,600	66,400	107,900	105,500	177,000	99,300	106,400	170,700	135,300	236,000	203,000	145,400	145,400	303,000	303,000	102,500	102,500	
14,900	67,100	108,500	106,000	178,000	99,300	107,400	171,700	136,300	237,000	204,000	146,400	146,400	304,000	304,000	101,500	101,500	
15,200	66,700	109,100	106,500	179,000	99,300	108,400	172,700	137,300	238,000	205,000	147,400	147,400	305,000	305,000	100,500	100,500	
15,500	67,400	109,700	107,000	180,000	99,300	109,400	173,700	138,300	239,000	206,000	148,400	148,400	306,000	306,000	99,500	99,500	
15,800	67,100	110,300	107,500	181,000	99,300	110,400	174,700	139,300	240,000	207,000	149,400	149,400	307,000	307,000	98,500	98,500	
16,100	66,400	110,900	108,000	182,000	99,300	111,400	175,700	140,300	241,000	208,000	150,400	150,400	308,000	308,000	97,500	97,500	
16,400	67,100	111,500	108,500	183,000	99,300	112,400	176,700	141,300	242,000	209,000	151,400	151,400	309,000	309,000	96,500	96,500	
16,700	66,700	112,100	109,000	184,000	99,300	113,400	177,700	14									

EXPERIMENTAL RESULTS RANGE	LOSSES	98.527	99.750	100.979	95.370
2.515	±7.630	109.429	97.500	223.114	94.620
3.765	±2.250	110.871	93.620	224.485	94.750
5.252	±2.120	112.243	92.000	225.827	94.500
6.429	±3.130	113.514	91.200	227.228	94.500
8.761	±2.630	114.926	91.120	230.240	100.120
9.773	±1.580	116.357	99.500	231.572	94.120
10.744	±3.770	117.899	97.120	232.943	94.370
12.115	±6.000	119.210	95.000	234.315	97.000
12.427	±5.720	120.562	92.270	235.467	94.620
14.859	±2.420	121.754	93.870	237.128	97.750
16.721	±5.500	122.725	93.370	238.430	102.250
19.461	±6.750	124.497	94.260	239.261	102.370
21.731	±4.970	126.268	106.120	241.173	104.500
22.463	±7.750	127.440	108.370	242.545	99.360
23.774	±8.220	128.912	111.120	243.916	97.720
25.146	±7.500	130.123	113.120	246.568	103.250
26.613	±8.200	131.555	112.620	249.431	104.750
27.369	±9.500	132.500	114.370	251.103	104.250
29.261	±1.120	136.246	110.751	252.374	103.370
30.432	±8.870	137.417	110.500	253.746	101.620
32.704	±8.200	138.929	109.620	255.118	102.000
33.774	±7.750	140.360	112.250	256.469	102.250
36.575	±4.420	141.732	111.500	257.261	101.220
37.248	±8.370	142.104	112.120	259.232	99.120
39.712	±1.980	144.475	111.750	260.404	97.370
40.451	±9.750	145.847	111.500	262.480	97.300
42.762	±1.500	147.212	110.370	264.262	98.370
43.434	±2.250	149.276	107.500	265.533	98.500
46.177	±2.500	150.547	105.750	267.005	99.250
47.544	±1.750	152.219	101.370	268.376	99.500
48.720	±7.620	153.391	99.750	269.748	99.360
53.721	±1.120	154.762	96.120	271.120	98.130
55.493	±7.000	157.515	93.370	272.491	97.120
56.464	±2.000	158.977	96.000	273.963	97.000
57.355	±3.500	160.249	93.130	275.234	99.370
62.746	±8.750	161.420	93.250	276.406	100.250
64.118	±4.350	162.092	93.500	283.117	96.750
65.429	±3.420	166.378	95.120	284.468	96.120
66.270	±6.700	168.750	96.120	285.861	99.380
68.233	±4.120	170.293	93.250	287.231	99.500
69.723	±5.370	172.164	92.500	288.612	98.620
71.755	±7.370	173.735	92.420	289.975	101.370
72.466	±7.370	175.108	94.120	291.346	103.500
75.209	±5.370	176.479	97.870	292.718	101.720
77.581	±5.370	177.351	93.500	294.769	99.500
77.933	±5.120	179.222	95.120	295.461	97.750
79.324	±6.820	180.594	97.360	296.769	102.120
80.456	±8.000	183.794	98.130	300.152	106.120
82.267	±7.870	185.165	93.130	301.523	102.870
83.439	±2.130	186.538	93.500	302.895	98.250
86.122	±2.000	198.535	103.500	304.267	96.250
87.554	±6.980	199.206	102.420	305.639	99.470
88.745	±6.500	201.274	102.420	307.010	100.420
90.257	±2.130	202.449	101.620		
91.469	±3.500	204.221	102.500		
92.240	±2.500	205.393	93.370		
92.412	±8.420	206.764	96.350		
95.753	±3.700	208.136	95.870		
97.155	±2.750	209.507	95.500		

Fig. B3b — Experimental intensity values

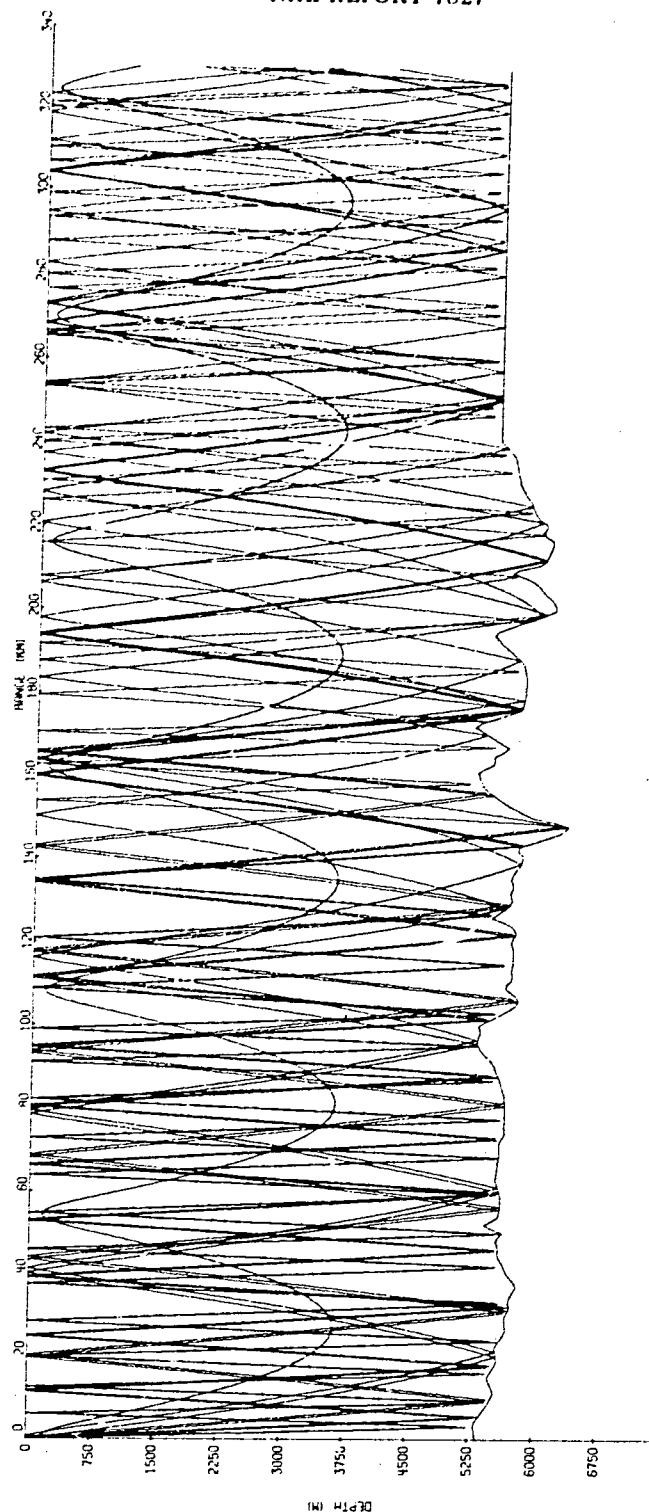


Fig. B4 — Selected rays which were traced (one ray every  $15^\circ$ )

COMPARISON OF EXPERIMENTAL AND CALCULATED RESULTS FOR THERMINI

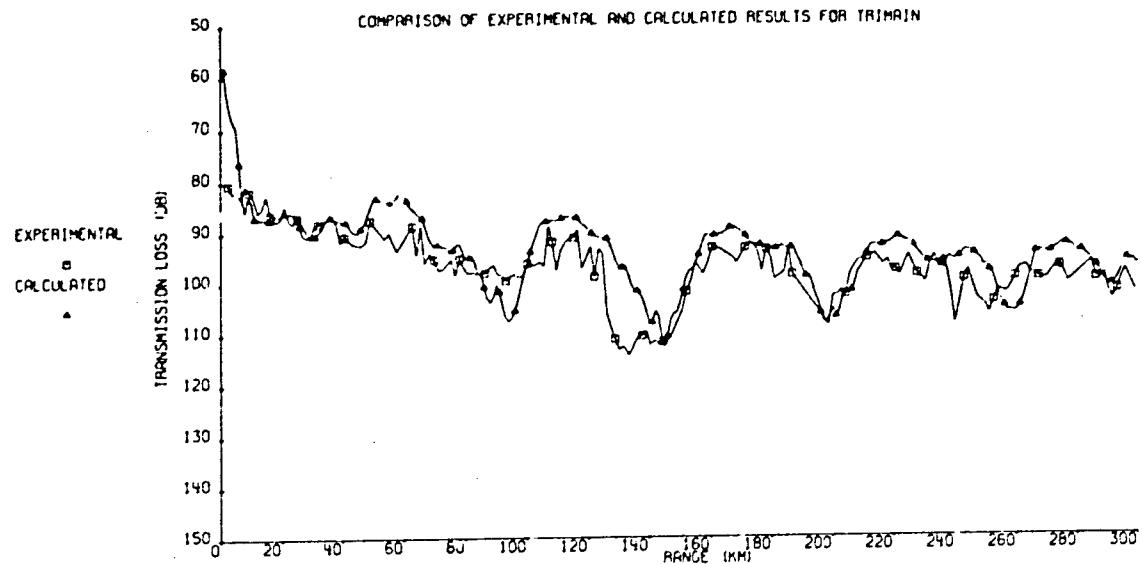


Fig. B5 — Comparison of experimental and calculated intensity values